New Monks Farm

Interpretative Hydrogeological Report on Groundwater Levels and Influencing Factors For New Monks Farm Developments Ltd April 2014





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Executive Summary

The Site	The proposed development site, which is of approximately 28 hectares, is located off Marsh Barn Lane at New Monks Farm, Lancing, West Sussex. The site comprises part open fields and part a golf course in construction.
	Overall the site slopes in a north easterly direction, with ground levels ranging between 2.0 m and 5.0m AOD. The site contains numerous watercourses.
Report objectives	To test the validity of preliminary mapping by the Environment Agency, which classifies the site as being at high risk from groundwater flooding, additional intrusive investigations and detailed water level logging in multiple geological horizons has been undertaken. The results have been compiled and assessed by experienced hydrogeologists to derive a comprehensive understanding of the hydrogeology and hydrogeological processes operating at the site (refer last box for conclusions).
Investigation carried out	 The drilling work, which occurred mainly over the period 23/1/2014 to 5/2/2014 (during which time the weather was generally very wet), included: 10 No Cable percussion boreholes to a depth of between 10m and 15 m bgl and dual 50 mm diameter monitoring wells (one borehole was redrilled); 2 No falling head tests; 20 No automatic water level data recorders were installed in ten borehole wells on the 7/2/2014 and these were set to record water levels at 2 minute intervals. The divers were withdrawn and the data information downloaded on the 4/3/2014, so as to allow this interim report to be produced. The loggers were then reset the same day with the aim to continue through to the week commencing 5th May 2014; and 10 No divers were installed at ten surface water localities utilising a mix of hanging lines off culverts and bridge decks and from wooden gantry type structures. The loggers were installed at the same time as the well loggers and recorded at the same intervals. They were downloaded on the same date and re-set in the same manner as the wells.
Geology findings	The ground conditions encountered by the boreholes were in accordance with the published geology for the site with made ground over clay superficial (Alluvium or Head deposits) with chalk beneath. It is noted that granular beach deposits were absent (a porous geological units found elsewhere in the Worthing area). The clay cover is complete over the whole site.
	The nature of the clay superficial is divided into two types; namely

	soft highly compressible alluvial silty clays and lower compressibility soft or soft firm (locally firm) slightly gravelly silty clay head deposits.
	Of the superficial deposits, the clay head dominates in terms of footprint coverage and the stratum is typically 3 to 4m thick. The alluvial clay is present as finger shaped deposit which runs in an east- west alignment in the northern fifth of the site. The clay alluvium is either of similar thickness to the clay head or in the case of a northern-central area considerable thicker (8.6m).
Groundwater findings	The site is not located within a groundwater source protection zone (ie a zone of land where groundwater resource is protected by the regulatory authorities).
	The pattern of response from the water level versus time graphs for shallow and deep geological units confirms that the Head Deposits and the alluvial clays are acting as an aquiclude or aquitard; with nominal hydraulic interconnectivity between the units. This separation of water units applies both during periods when the Chalk piezometric surface (equivalent to the water pressure) in a unit is artesian, with a pressure head above the elevation of the perched water table level in the clay above; and when the piezometric surface in the Chalk is lower than this perched water table.
	In a single location (central northern sub area) the chalk piezometric level rises less than a metre above the land surface.
	The most southerly borehole on the site has a lower piezometric surface in the Chalk aquifer than the near surface perched water table. Moreover, the observed water level in the Chalk in this peripheral location shows a clear tidal influence, with a diurnal water level range of up to approximately 3cm. The periodicity of the diurnal variability in Chalk groundwater head confirms a direct tidal influence and therefore hydraulic connectivity with the sea or estuarine water at this sector of the site.
Surface water findings	The closest major water feature is the River Adur located approximately 1.5 km east of Marsh Barn Lane. Surface water movements at the site are influenced by a series of ditches that eventually combine and discharge via a control structure adjacent to the south-east corner of the site boundary with Shoreham airfield which then drains into the tidal River Adur.
	The hydrographs (water height in the channel versus time graphs) for all the functioning surface water stations show there is a response to rainfall, with a fairly rapid response with an increase in water level during and following rainfall, with a tail off back to a base level. The hydrographs for those monitoring points placed on the most northerly water courses show higher amplitude peaks with quite marked tails offs. This pattern is attributed to surface water runoff, in part via the A27 drainage and in part from the hills to the north of the A27.
	The surface water level data also displays a longer trend with the

	surface water height data reducing over the course of the monitoring period notably from a peak level on the 14 February 2014 through the 03 March 2014. This longer term trend in declining surface water levels over this period is identifiable in all of the surface water monitoring locations across the site; although is less pronounced in the water course located in the north-eastern corner of the site.
	Furthermore, the surface water monitoring locations to the south and east of the study site all show evidence of diurnal fluctuation in water level related to the tidal cycle. This tidal influence on the surface water levels over much of the site is interpreted to most likely be a result of retardation where flow within the channels backs up due to the rising and high tide in the Adur estuary and sea.
Conclusions/ groundwater model	The Newhaven Chalk forms the bedrock geology to the site. The Chalk aquifer is recharged at its outcrop to the north of the A27, and is confined by superficial deposits over the entirety of the site, with semi-confinement just beyond the northern boundary of the site.
	Towards the southeast of the study site, there is a tidal signal in the Chalk piezometry, inferring hydraulic connectivity between the Chalk aquifer and the marine or estuarine environment. This is not identified elsewhere across the deep monitoring boreholes at the site.
	Furthermore, the water levels in the shallow boreholes towards the eastern boundary of the study site also display a diurnal cycle that can be attributed to tidal fluctuation influence.
	The superficial Head and Alluvium deposits overlay the Chalk bedrock and form an aquiclude or aquitard, substantially limiting vertical groundwater movement between the Chalk and the near surface deposits. As a result, during the period of groundwater level monitoring, the Chalk aquifer beneath the site is confined with the piezometric surface above the base of the superficial deposits.
	The superficial deposits act as an aquitard or aquiclude, with some evidence for low to very low vertical permeability, related to clays and silts within specific lateral continuous horizons within the Head and Alluvium deposits. This provides protection to the Chalk aquifer at depth and results in both a perched aquifer in the superficial deposits; and confinement of the Chalk aquifer.
	The intense and substantially above average rainfall prior to and during the field monitoring has led to elevated water table levels in the superficial deposits, forming localised groundwater mounds. The excess groundwater storage is released via flows and seepages into the surface water drainage system. During the high rainfall event, the water level within the surface water drainage was observed to be lower than the perched groundwater mounds. Therefore, there is a component of perched groundwater contribution to the base flow within the surface water drainage at the site.
	There is no evidence to indicate that there is direct contribution to

	surface water flows from the Chalk aquifer at depth beneath the site.
	It is noted that during the study period, excess groundwater storage was released from the unconfined Chalk aquifer to the north of the A27 via ephemeral springs and streams, resulting in localised groundwater flows and flooding in parts of Lancing close to the A27 in February and March 2014. The groundwater flooding event in Lancing did not lead to groundwater flooding of the study site. It may have contributed to additional flows within the surface water drainage across the site, as the excess groundwater flowed (and was also pumped) from the affected areas through the surface water drainage towards the River Adur, estuary and sea.
Overall conclusions and implications to the surface water management system.	The observations made during the very high rainfall and groundwater conditions experienced in early 2014 show that the study site is not susceptible to groundwater flooding, provided the geological units remain intact during any development.
	The EA mapping of a 'high risk' of flood emergence' would appear over cautious for this site.
Relevance to surface water management	A key component of the development proposals is to mitigate against flood risk by raising ground levels to a height commensurate with the 1 in 200 year coastal flood level (to 2115) plus a 300mm freeboard to account for varying wave heights and uncertainty. To mitigate against potential overland flows entrance thresholds to buildings will be raised a further 150mm. The investigations have encountered a degree of baseflow (at least during wet weather periods) between the shallow superficial geology and the water courses but this is restricted by the clay geology (hence low permeability). In this setting it is not considered that the capacity of the existing channels will be compromised by baseflow. Any filling of the site will increase the capacity of the channel and act to improve flow capacities.
Recommendations	It is recommended that the planned additional monitoring of the various measuring points is continued into May when the response of the surface water and groundwater to drier weather can be seen.



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Appendices

Appendix A Harrisons Factual Site Investigation Report Appendix B Groundwater levels (compensated logger data) Appendix C Groundwater levels (manual water dips) Appendix D Water Quality data (laboratory certificates and in situ index testing)

1. Introduction

- 1.1 Capita Property and Infrastructure Ltd were commissioned by New Monks Farm Development Ltd to undertake a hydrogeological study at New Monks Farm, North Lancing focused on assessing groundwater water levels and factors which influence these, including rainfall and seasonal affects and to make an assessment of this data to interpret the risk level of groundwater flooding at the site. A mixed use development is planned for the site comprising commercial, housing and a school.
- 1.2 Our approach to the above was outlined in a letter to the Capita Project Manager dated 2nd December 2013, which comprised the following tasks:
 - 1. Preparation of a Hydrogeological Desk Study report to include:
 - a) Site walkover;
 - b) Review of published available geological and hydrogeological mapping; and
 - c) Review of published hydrogeological records (including borehole records).
 - 2. Design and supervision of a ground investigation to assess relationship between groundwater and surface water levels;
 - Collection of two rounds of groundwater samples for chemical analysis (one undertaken at time of issue);
 - 4. Installation of groundwater level dataloggers; and
 - 5. Production of an interpretative hydrogeological report to assess seasonal impacts¹ and impact of recharge from rainfall intensity on groundwater levels.
- 1.3 The preparation of this report, which is an interim issue, has involved the examination of information from the following sources:
 - 1. Digital mapping supplied by Landmark Information Group, including:
 - a) British Geological Survey 1:10,000 Superficial and Bedrock Geology maps;
 - b) British Geological Survey Geological Indicators of Flooding Map;
 - c) British Geological Survey Groundwater Flooding Susceptibility Map; and
 - d) Environment Agency Historic Flood Events Record.
 - 2. British Geological Survey Solid and Drift Geological Mapping Sheet 318: Brighton (1:50,000)
 - 3. British Geological Survey Memoir for Geological Sheet 318 entitled *Geology of the country around Brighton and Worthing*;

¹ It was appreciated from the outset that seasonal impacts would take a time period more extensive than the 3 months length of the monitoring exercise but it was acknowledged that the period of highest rainfall (ie winter) would be covered which was the 'worst cakey b se' month in terms of groundwater flooding (should it occur).

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- 4. Electronic records of historical boreholes accessed using http://mapapps.bgs.ac.uk/geologyofbritain/home.html;
- Harrison Group Environmental Ltd Factual *Letter-style* Report on Ground Investigation at New Monks Farm, Lancing dated February 2014;
- Brassington, F.C. and Younger, P.L., 2010. A proposed framework for hydrogeological conceptual modelling. *Water and Environment Journal* Volume 24, Issue 4, pages 261–273, December 2010.
- Shepley, M. G, Whiteman, M. I., Hulme, P. J. and Grout, M.J., 2012. *Introduction:* groundwater resources modelling: a case study from the UK. In: Shepley, M. G., Whiteman, M. I., Hulme, P. J. and Grout, M. W. (eds) Groundwater Resources Modelling: A Case Study from the UK. Geological Society, London, Special Publications, 364, 1–5.
- Rushton, K. R. and Skinner, A.C., 2012. A national approach to groundwater modelling: developing a programme and establish technical standards. In: Shepley, M. G., Whiteman, M. I., Hulme, P. J. and Grout, M. W. (eds) *Groundwater Resources Modelling: A Case Study from the UK*. Geological Society, London, Special Publications, 364, 8–17.
- Whiteman, M. I., Seymour, K. J., van Wonderen, J. J., Maginness, C. H., Hulme, P. J., Grout, M. W. and Farrell, R. P. 2012. *Start, development, and status of the regulator-led national groundwater resources modelling programme in England and Wales*. In: Shepley, M. G., Whiteman, M. I., Hulme, P. J. and Grout, M. W. (eds) *Groundwater Resources Modelling: A Case Study from the UK*. Geological Society, London, Special Publications, 364, 19–37.
- 10. Met Office Rainfall data for Shoreham Airport February 2014 to March 2014;
- 11. Environment Agency groundwater level monitoring data;
- 12. Environment Agency monthly water situation report for South East Region, Solent and South Downs, February 2014.
- 13. Tidal data for Shoreham Harbour; and
- 14. Groundwater level data Brighton and Hove Albion Training Ground.

Disclaimer

- 1.4 This report is for the use of New Monks Farm Developments Ltd only and should not be used by any other party unless specifically advised in writing by Capita Property and Infrastructure Ltd.
- 1.5 This report has been prepared by Capita Property and Infrastructure Ltd on the basis of the available information received during the assessment period. Although every reasonable effort has been made to obtain all relevant information, all potential environmental constraints or liabilities associated with the site may not necessarily have been revealed.



2. Background

Site Location and Immediate Environs

- 2.1 The proposed development site is located off Marsh Barn Lane at New Monks Farm, Lancing, West Sussex (approximate NGR 519575 105380). The development boundary covers approximately 28 hectares. A site plan is shown on Figure 1.
- 2.2 The site currently exists as undeveloped greenfield land in the west and a golf course (under construction) located on eastern portion. The A27 dual carriageway bounds the site to the north; a residential development to the west; Shoreham airport bounds the site to the east; and the Brighton and Hove Albion Football Club Training Ground (under construction) forms the southern boundary.

Site Description

- 2.3 A site visit was conducted by an environmental consultant on the 7th January 2013, which confirmed the land uses described above. Site access off the A27 via the VOSA weighbridge lay-by.
- 2.4 Two stacked portacabins are located to the immediate west of the site entrance and a vehicle wheel wash is located approximately 50 m to the south of the entrance. A surfaced haul road extends past the site entrance following the boundary to the east and south, providing access to the Brighton and Hove Albion Football Club development on the southern boundary. A site security office managed by the football club developers is located on the haul road approximately 600 m south of the site entrance.
- 2.5 Numerous drainage ditches and balancing ponds are located throughout the site; Figure 2 illustrates the main surface water features.
- 2.6 A topographic survey was carried out by M.J Zara Associates on behalf of Michael Cox Associates in April 1999. Overall the site slopes in a north easterly direction, with the following observations noted:
 - i. The area of highest elevation can be found in the south western corner where ground levels are approximately 5.0 m AOD;
 - ii. Ground levels in the north western corner are 2.0m AOD; and
 - iii. Ground levels in the centre of the site are typically 2-2.5m AOD.

Development Proposal

- 2.7 An indicative development proposal is included as Figure 9 for a mixed used development and includes the following:
 - iv. Residential;
 - v. Business and Commercial; and



vi. Primary School

Previous Reports

2.8 A summary of reports specific to groundwater flooding at New Monks Farm, Lancing are provided below.

Strategic Flood Risk Assessment - Capita Symonds Ltd January 2008 - 2010

- 2.9 Groundwater flooding is caused by the emergence of water originating from sub-surface permeable strata (Jacobs 2006). An increase groundwater level sufficient for the water table to rise above the ground surface and inundate land downstream from the outflow may result in a groundwater flood event. Groundwater floods can emerge from either point or diffuse locations; and may be via substantial flows via ephemeral springs or numerous smaller springs and seepage at the ground surface. Groundwater flood events tend to be long in duration developing over weeks or months and prevailing for days or weeks.
- 2.10 Groundwater flood events have been recorded in various aquifer units (including Cretaceous Chalk, Limestones, river terrace gravels). However most accounts of groundwater flooding are confined to the Chalk outcrop, which includes the Chalk of Southern England (Jacobs 2006).
- 2.11 The primary control on the distribution and timing of groundwater flooding from the Chalk are:
 - Spatial and temporal distribution of rainfall.
 - Spatial distribution of aquifer properties.
 - Recharge mechanisms, duration and spatial distribution.
 - Spatial and lateral distribution of geological structures (drift deposits, stratigraphy).
 - Efficiency of the surface runoff and drainage network.
- 2.12 Compared to other aquifer units, the Chalk can be more vulnerable to groundwater flooding because of its geological formation. Characteristically, groundwater movement and storage in the Chalk is predominantly via transmissive fractures and fissures which can result in rapid rises in groundwater levels, which may take a substantial time to recede. The propensity for groundwater flooding is higher where the Chalk is exposed with minimal drift cover. The vulnerability of an aquifer to groundwater flooding can largely be determined by an analysis of the meteorological situation and geological knowledge.
- 2.13 Map G of the strategic flood risk assessment titled 'Areas Prone to Groundwater Flooding' highlights that the proposed development is located in an area classified as a 'High Potential for Groundwater Flooding' and land that borders the site to the immediate north is classified as a 'Groundwater Emergence Zone Area' and also a contains a 'Recorded Groundwater Flooding Event'.



Strategic Flood Risk Assessment – JBA Consulting January 2012

- 2.14 A "Core Strategy" summary sheet is provided for New Monks Farm² which states with respect to Groundwater Flood Risk 'The site is underlain by the Newhaven Chalk Formation, and is within the EA's major aquifer high vulnerability zone. Consequently the area may be susceptible to groundwater emergence. According to the EA groundwater flood susceptibility map, the majority of the site resides in a 1km square where the proportion of the 1 km square that is susceptible to groundwater flood emergence is more than 75%.'
- 2.15 And recommends that 'The site is also at risk of groundwater and surface water flooding, therefore steps should be taken to reduce the consequence of flooding. Any future development should ensure that it would not increase the surface water flood risk elsewhere, to achieve this any existing flow paths would need to be maintained. The site is greenfield so surface water drainage techniques should be built into any new design to ensure the runoff rate does not increase.'

Meeting of Capita, Planners and Environment Agency on 14 January 2014

- 2.16 Dr Rob Hares of Capita property and Infrastructure produced a memo to inform the meeting at the EA offices in Worthing. This provided a plan of intrusive investigation to assess the potential for groundwater flooding and this involved the following measures:
 - i. Strike and resting groundwater levels across the site (determined by groundwater strikes during Cable Percussion Boreholes);
 - ii. Assessment of permeability of Head Deposits; Alluvium and Beach Deposits;
 - iii. Continual measurement of groundwater water levels (using Schlumberger data loggers) within Newhaven Chalk; Gravel; and Beach Deposits; and
 - iv. Continual measurement of water levels within notable surface water features (using Schaumberg data loggers)
- 2.17 To facilitate the above it is intended to excavate ten boreholes to a maximum depth of 15 m bgl. The groundwater monitoring will be undertaken over a 3 month period and will assess changes in groundwater levels in response to rainfall intensity and tidal variance. The data will also be used to assess groundwater/surface water interactions and will be used to provide conceptualism of the site with hydrographs. This scoping/methodology was generally agreed.

² <u>http://www.adur-worthing.gov.uk/media/media,87208,en.pdf</u> accessed 17/03/14



3. Ground Conditions

Geology

- 3.1 A review of published geological information was carried out, including information from the British Geological Survey (BGS) 'GeoIndex' online database (which includes 1:50000 scale geological mapping), Lexicon and borehole information.
- 3.2 The site is underlain by bedrock of the Newhaven Chalk Formation, superficial deposits are found across the site comprising Head Deposits at the near surface to the west of Marsh Barn Lane, with borehole logs confirming Head Deposits underlie the whole study site; and Alluvium at the near surface above the Head Deposits, to the east of Marsh Barn Lane; with an area of Alluvium to the west of Marsh Barn Lane immediately south of the A27.
- 3.3 The British Geological Survey (BGS) have records of several historical boreholes on site and within the surrounding area. A summary of the published and encountered geological sequence is provided in Table 3.1 below.
- 3.4 The geology beneath the land to west of New Monks Farm and to east of Shadwells Road comprises of superficial Head Deposits, comprising Clay Silt Sand and Gravel. This is above a bedrock of formed by the Newhaven Chalk Formation. The Newhaven Chalk is underlain by the Seaford Chalk which forms the bedrock outcrops to the east and northeast from the site; and is overlain by the Tarrant Chalk Member of the Culver Chalk Formation which outcrops to the west and northwest from the site. The Seaford Chalk, Newhaven Chalk and Tarrant Chalk form a continuous Principal Aquifer that underlies the site; and has a recharge area to the north of the A27, along the South Downs dip and scarpe slope.
- 3.5 Two borehole logs are identified in the area west of New Monks Farm and east of Shadwells Road.
 - TQ10NE86 Topsoil to 0.2 m over; CLAY 1.5 m over; clay gravel 0.2 m; over CHALK 4.1 m Standing water level at 0.4 m bgl (moderate seepage at depths > 3.8 m bgl);
 - TQ10SE193 Brown silty CLAY with Gravel 2.92 m over; putty chalk 1.64 m water strike approx. 3.81 m rose to approx. 2.92 m.
- 3.6 The land to the west of North Barn Farm and to east of Barfield Park Road is underlain by superficial Raised Beach Deposits, comprising Sand and Gravel. Beneath the Raise Beach Deposits, the bedrock comprises of the Newhaven Chalk Formation. This geology is confirmed from the following borehole logs in this area:
 - TQ10SE38 Drift overlying Upper Chalk (thicknesses not given) to max depth 8.84 m; with rest water level at 0.76 m bgl;
 - TQ10SE23/A Drift (Gravel) 3.05 m over; Chalk 15.2 m;
 - TQ10SE23/B Drift (Beach deposits) 3.05 m over; Chalk 27.4 m. Water level about 3.05 m (top of the Chalk).



- 3.7 The geology underlying the land to the east of Marsh Barn Lane consists of superficial Alluvium deposits comprising Clay, Silts, Peat and Sands. The bedrock is Newhaven Chalk Formation. This is confirmed by the following borehole logs:
 - TQ10SE192 Topsoil 0.3 m over; soft-firm silty CLAY 1.3m over; firm brown grey silty CLAY 1.0m over; Putty Chalk 1.5 m; water strike at top of the Chalk (3.048 m) rising to 1.5 m;
 - TQ10NE108 Dark Clay 9 m over; Chalk 18 m; water struck at 11 m.

Geological Unit		Description	Thicknesses
Made Ground		Not known – in location of new Golf Course	Not known
Quaternary	Alluvium	Clay, Silty, Peaty, Sandy. Superficial Deposits formed up to 2 million years ago in the Quaternary Period. Local environment previously dominated by rivers.	
		TQ10SE192 soft to firm brown and grey silty CLAY and fine	
		grey SAND with flint and putty CHALK	4.57 m
		TQ10N108 Dark CLAY	9.00 m
	Head	Clay, Silt, Sand And Gravel. Superficial Deposits formed up to 3 million years ago in the Quaternary Period. Local environment previously dominated by sub-aerial slopes	
		TQ10NE86 soft to firm grey mottled brown silty CLAY fine	1.00
		gravel with soft brown CLAT at the base.	1.90 m
		TQ10SE193 Firm brown silty CLAY with gravel	2.92 m
Cretaceous	Newhaven Chalk Formation	Chalk. Sedimentary Bedrock formed approximately 71 to 86 million years ago in the Cretaceous Period. Local environment previously dominated by warm chalk seas.	
		TQ10NE86 describes extremely soft structureless putty chalk becoming firm structureless CHALK with lumps of intact CHALK and a few flints. (Grade V)	Base not recorded on historic borehole logs. Published records report 204 m

Table 3.1 Description of Geology

Hydrogeology

3.8 Hydrogeological information has been obtained from the Environment Agency's (EA's) website page 'What's in Your Backyard'. The bedrock geology (Newhaven Chalk Formation) is classified as a Principal Aquifer, which is described by the EA as "layers of rock or drift deposits that have high intergranular and/or fracture permeability - meaning they usually provide a high level of water storage. They may support water supply and/or river base flow on a strategic scale."



- 3.9 The superficial deposits (Head and Alluvium) are described by the EA as "Secondary Undifferentiated where it has not been possible to attribute either category A or B to a rock type. In most cases, this means that the layer in question has previously been designated as both minor and non-aquifer in different locations due to the variable characteristics of the rock type."
- 3.10 The site is not located within a groundwater source protection zone. The groundwater vulnerability for the majority of the site is classed as Major Aquifer High. However, a section of land to the west of Marsh Barn Lane is classified as Major Aquifer Intermediate. The groundwater vulnerability maps are a "*broad appraisal of where groundwater resources may be vulnerable from surface land use activities.*" A high classification assumes that the soils can readily transmit liquid discharges because they are either shallow or susceptible to rapid flow directly to rock, gravel or groundwater.
- 3.11 The Environment Agency monitors groundwater levels at a number of observation boreholes in the Lancing area. Historic water level data for five observation boreholes in the Lancing area has been reviewed as part of this study. Three of the data sets from boreholes referred to as Sussex Pad Hotel, Old Salts Farm and New Salts Farm have historic data but not continuous over recent years. However, the boreholes referred to as Sussex Pad No.1, north of the A27 close to the north-eastern corner of the study site and the surface water monitoring location SW10; and the Daniels Barn borehole, south of the A27 and north of the study site, close to BH10, has a long term water level monitoring record.

Hydrology

- 3.12 The closest major water feature is the River Adur located approximately 1.5 km east of Marsh Barn Lane. However, surface water which runs off the developable part of the site is collected by a series of ditches that eventually combine and discharge via a control structure adjacent to the south-east corner of the site boundary with Shoreham airfield. These ultimately discharge to the River Adur. The surface water ditches are illustrated on Figure 2.
- 3.13 The estuarine reach of the River Adur has been classed as good and moderate potential with respect to current chemical and ecological potential, respectively.
- 3.14 A freshwater spring known as Honeyman's Hole is located offsite, approximately 450 m to the east of the site entrance.



4. Site Works

Scope of Investigations

- 4.1 A site investigation specification and tender package was prepared by Capita in January 2014 and Harrison Environment Group Ltd were duly commissioned to undertake the drilling work. The drilling occurred mainly over the period 23/1/2014 to 5/2/2014 during which time the weather was generally very wet. A further borehole (BH4S) was drilled after a hiatus on 19/3/2014 and on the same date the seal was rectified in 6S and BH5 decommissioned by grouting. The objectives of the site investigation were as described in para 2.16.
- 4.2 The site investigation Contractor carried out the following exploratory works:
 - CAT scan to screen for buried services;
 - 10 No Cable percussion bored excavations to a depth of between 10m and 15 m bgl and dual 50 mm diameter monitoring wells (designated BH1 to BH10)
 - A re-drill designated BH4AS with a 1.5m long 50mm diameter monitoring well;
 - 2 No falling head tests at locations specified by the Project Manager;
 - The recovery of small disturbed samples and bulks samples and U100 samples for soil classification purposes;
 - Grouting sections of boreholes;
 - Preparation of Factual Reports (to include x,y,z co-ordinates and levels of boreholes and pits); and
 - Provision of digital data in AGS and AutoCAD format.
- 4.3 Ten locations were proposed for exploratory boreholes. The final locations, determined from access considerations and with respect to any buried services were to be agreed on site with the Project Manager, and are shown in Figure 4. Those wells selected for water level installations were as follows: BH1S and D, BH2 S and D, BH4D, BH6D, BH7 S and D, BH10 S and D.
- 4.4 Capita engineers installed automatic water level data recorders (called divers) in ten borehole wells on the 7/2/2014 and these were set to record water levels at 2 minute intervals. The divers were withdrawn and the data information downloaded on the 4/3/2014, so as to allow an interim report to be produced. The loggers were then reset the same day with the aim to continue through to the week commencing 5th May 2014. A barometric data logger was installed to record atmospheric pressure over the same data collection intervals.
- 4.5 Capita engineers installed automatic water level data recorders (called divers) at ten surface water localities utilising a mix of hanging lines of coverts and bridge decks and from wooden gantry type structures. The loggers were installed at the same time as the well loggers and recorded at the same intervals. They were downloaded on the same date and re-set in the same matter as the wells.



- 4.6 Manual dips were collected on the 5/6 of March and the 4/5 of April 2014 of all functioning loggers, both wells and surface waters.
- 4.7 Capita engineers collected water samples from each borehole and surface water location over the period 4 to 6/3/2014. Low flow pump techniques (with stabilised water quality parameters using a multiparameter troll) were used to collect groundwater samples and simple jar immersion techniques were used to collect surface water samples. These were despatched in cool boxes under ice packs to I2 Laboratories.

Findings of Site Works: Ground Conditions

- 4.8 The ground conditions encountered by the boreholes were in accordance with the published geology for the site with made ground over clay superficial (Alluvium or Head deposits) with chalk beneath. It is noted that granular beech deposits were absent.
- 4.9 A summary of the geology is shown in Figure 2. This illustrates that there is cover of clay over the Chalk bedrock over the whole of the site. The nature of the clay superficial is divided into types namely soft highly compressible alluvial silty clays and lower compressibility soft or soft firm (locally firm) slightly gravelly silty Clay head deposits.
- 4.10 Of the superficial deposits, the clay head dominates in terms of footprint coverage and the stratum is typically 3 to 4m thick. Where it is thinner this is because its upper layers have been replaced with made ground. The alluvial clay is present as finger shaped deposit which appear to follow the larger current water coarse which runs in an east- west alignment in the northern fifth of the site (within 200m of the Old Shoreham Road (A27). The clay alluvium is either of similar thickness to the cay head or in the case of BH1 considerable thicker (8.6m).
- 4.11 The chalk subcrop proved difficult to sample and log its various weathering grades despite an attempt to collect 'undisturbed' U100 samples of the material. However, there often appears to be a 1.5m thick upper unit of structureless gravelly Silt over a layer of structureless chalk cobbles and gravel.
- 4.12 When drilling, most boreholes made two separate water strikes, an upper one in the shallow perched water table (ie within the superficial deposits an second one within the Chalk. Both strikes had a significant head rise after 20 minutes. Refer Borehole logs in Appendix A for detail. None of the borehole strikes gave rise to water flowing out of the casing top.



5. Hydrogeological Assessment

Groundwater Levels Analysis

- 5.1 As detailed in Section 4, water levels within the upper superficial and Lower Chalk aquifer units have been measured using pressure transducers logging the piezometric head. This data is presented in Figures 8 a to f for the period from 07 February to the 03 March 2014.
- 5.2 Distinct water levels are observed between water level within the upper superficial aquifer and the Lower Chalk aquifer at depth. This is noted in BH01, BH02, BH07 and BH10 as presented in Figures a, b, e and f, respectively. In plan the flow directions in the units are shown in the surfer plots in Figures 6a and 6b (superficial deposits) and Figures 7a and 7b (Chalk -2 dates).
- 5.3 The water level in the shallow borehole BH02S (Head deposits) shows a relatively flat trend between 2.65 m AOD and 2.78 m AOD over the period 07 February to the 03 March 2014 which contrasts with the deeper piezometer at this location which is more variable. For example, for the same period the Chalk has a piezometric head greater than that of the perched water table at the start of the data period with a maximum of 3.096 m AOD; which drops to lower than the water level in the Head from 22 February 2014, reaching a minimum water level of 2.527 m AOD. The shallow and deep water level time series confirms that the Head Deposits are acting as an aquiclude or aquitard; with nominal hydraulic interconnectivity, both during periods when the Chalk piezometry is artesian with a pressure head above the elevation of the perched water table level above; and when the piezometric surface in the Chalk is lower than this perched water table.
- 5.4 Borehole BH01 is positioned towards the north of the site, drilled through Alluvium deposits. The water level data in the shallow well shows a relatively flat trend between 2.82 and 2.86 m AOD; whereas the deeper Chalk piezometry commences at a higher head, approximately 9cm above the shallow water level in mid-February, with a gradual decline to be essentially coincident with the shallow water level by early March 2014. The initial difference in the piezometric head should be considered in the context of the position of BH01 towards the north of the site, closer to the Chalk outcrop than the other boreholes drilled through the Head Deposits at the site. The elevated piezometric surface is interpreted to be in response to the intense rainfall falling up to mid-February; and as the excess groundwater storage in the Chalk aquifer drained from the aquifer via perennial and ephemeral springs to the north of the A27, and then the pressure in the Chalk aquifer slowly diminished. As the water table in the Chalk aquifer reduced, the difference in the piezometric level in the Chalk relative to the Alluvium and Head deposits also reduced.



- 5.5 The difference in superficial/Chalk heads during the elevated piezometry and the lag before the two piezometric levels reached equilibrium, indicates that there is a delay in the hydraulic interconnection between the two aquifer systems. It is unclear solely from the groundwater level data whether the hydraulic interconnection occurs via a predominantly vertical pathway or via a lateral interaction due to the thinning of the Head Deposits and proximity of the Chalk outcrop to the north. This thinning may be further exacerbated by underground services and the depth and constituent make-up of the A27 base in relation to the thickness of the Head Deposits.
- 5.6 Borehole BH10 is located to the northeast of the site, immediately to the south of the A27 and caravan park and in a similar geological setting as BH01. The shallow piezometer BH10S is drilled into the Alluvium deposits, with the water level essentially flat, rising from 2.90 m AOD at the start of February to approximately 3.05 m AOD by mid-February before declining to 2.77 m AOD by the end of February 2014. This is the same situation as found in the shallow well in BH01S. It is noted that the shallow groundwater level is approximately 2.9m above the level of the nearest water level monitoring points at SW08. This is a result of intense and prolonged rainfall-recharge to the alluvium aquifer building up groundwater levels without sufficient time for these to drain down to reach equilibrium with the level of the adjacent surface water. The drain down being slowed buy the low permeability of the alluvial clay.
- 5.7 This contrasts with the piezometric surface measurements in the Chalk aquifer beneath the Alluvium at this location, whereby the piezometric surface in BH10D rises steadily from approximately 2.17 m AOD on 07 February 2014 to approximately 2.63 m AOD by the beginning of March 2014. Although the Chalk piezometer rising and the Alluvium falls over the same period, there is no evidence to indicate that these converge and therefore the Chalk groundwater and the perched groundwater in the Alluvium deposits act locally as separate hydrogeological units; with layers in the Alluvium deposits retarding vertical groundwater movement sufficiently to act as an aquitard.
- 5.8 The most southerly borehole on the site BH07 has a lower piezometric surface in the deeper Chalk aquifer than the near surface perched water table. The water table in the superficial deposits over the period from 07 February to 03 March 2014 ranges from 3.67 m AOD to 4.01 m AOD, varying in response to rainfall and surface water levels. In contrast, the piezometric surface in the Chalk aquifer beneath the Alluvium in BH07D ranges from 2.233 m AOD to 2.735 m AOD. Moreover, the observed water level in the Chalk borehole BH07D shows a clear tidal influence, with a diurnal water level range of up to approximately 3cm. The periodicity of the diurnal variability in Chalk groundwater head confirms a direct tidal influence and therefore hydraulic connectivity with the sea or estuarine water at this sector of the site.



- 5.9 The water levels in the upper and lower aquifer units in BH4 shows identical values throughout the time series, strongly indicating that there is direct hydraulic connectivity between the units at this location. Investigations determined that the borehole was poorly grouted, and allowed water flow between the units via borehole BH04. This was addressed through the re-drilling of the shallow piezometer referred to as BH04A to a depth of 1.5m below ground level into the Head Deposits on the 20 March 2014. The shallow borehole BH04S was grouted to ensure that the water level measured in BH04D was only that of the Chalk aquifer at depth. There was no water strike during the drilling BH04A. Future monitoring at BH04D and BH04AS will allow clarification of the true head differences.
- 5.10 The water level time series for the shallow and deep aquifers monitored at BH06 show a parallel water level between the shallow level water level and the deeper piezometric head of approximately 8 cm throughout. The near-constant difference between these two piezometric measurements indicates that there is a strong interconnectivity between the upper and lower aquifers at this location. It is understood that the bentonite plug dropped during the construction of BH06 which may explain the difference between the water levels whilst representing a fairly rapid pathway via the borehole. Other possible explanation, such an error in the water level measurement, reading error in the pressure transducer or adjustment to atmospheric pressure have been checked and shown not to be the case.

Chalk Aquifer Groundwater Levels

- 5.11 As described previously the Environment Agency monitors groundwater levels at two key wells in the environs of the site namely Sussex Pad No.1, north of the A27 close to the north-eastern corner of the study site and the surface water monitoring location SW10; and the Daniels Barn borehole, south of the A27 and north of the study site, close to BH10, has a long term water level monitoring record. Refer to Figure 1 for locations of these wells.
- 5.12 These two long term Chalk groundwater monitoring boreholes are well placed to determine the seasonal and long term range in Chalk groundwater conditions beneath the study site.
- 5.13 The historic water level at Sussex Pad Borehole No.1 has a range from -0.31 m AOD to +3.43 m AOD over the period 1977 to 2013; and the Daniels Barn Borehole has a range from -1.26 m AOD to +2.12 m AOD over the period 1976 to 2010.
- 5.14 The higher end of these ranges compare well with those found in the Chalk during the march monitoring period. This is to be expected given that the weather followed one of the wettest period in the UK for tens of years. Capita has a data request logged with the EA for the Sussex Pad well to seek availability of levels for the same period as water level monitoring for this study. However, we would expect the similarity to be maintained.

Surface Flows

5.15 The level of the surface water monitoring was monitored at nine locations across the site, as identified in Figure 4. The time series of the surface water levels recorded using Diver pressure transducer loggers and adjusted for atmospheric pressure, are presented in Figure 8g.



- 5.16 A number of similar trends can be identified from the time series for the nine surface water level monitoring points. There is a response to rainfall, with a fairly rapid response with an increase in water level during and following rainfall, with a tail off back to a base level.
- 5.17 The magnitude of the hydrograph peak and the duration of the tail vary between the monitoring points. There is evidence of individual rainfall events in the hydrographs, notably present in SW01 and SW02 to the north of the study area, adjacent to Marsh Barn Lane. Surface runoff, in part via the A27 drainage, from the hills to the north of the A27 can explain the short term rainfall response within these hydrographs.
- 5.18 The surface water level data also displays a longer trend or hydrograph. The water level within the surface water monitoring points has a trend reducing over the course of the monitoring period notably from a peak level on the 14 February 2014 through the 03 March 2014, as presented in Figure 8g. This longer term trend in declining surface water levels over this period is identifiable in all of the surface water monitoring locations across the site; although is less pronounced in SW10 on the north-eastern corner of the site.
- 5.19 Furthermore, the surface water monitoring locations to the south and east of the study site namely SW03, SW04, SW05, SW06, SW07, SW08 and SW10 all show evidence of diurnal fluctuation in water level related to the tidal cycle. This is particularly pronounced at SW07 and SW10 to the south east and north east of the study area, respectively. This tidal influence on the surface water levels over much of the site is an important consideration in terms understanding the drainage. The tidal water level response may be either a result of marine or estuary water flowing back into the channels within the study area; however, it is more likely that the flow within the channels backs up due to the rising and high tide in the Adur estuary and sea, resulting in the hydraulic response at the monitoring locations.

Water Quality

- 5.20 Analysis of the water samples taken from the deep and shallow boreholes on 04 and 05 March 2014 and surface water monitoring locations on 05 and 06 March 2014 (monitoring locations as identified in Figure 4). A significant range of parameters were tested for comprising general inorganics, total phenols, heavy metals and metalloids, monoaromatics, total and speciated PAHs and aliphatic (C5 C35) and aromatic (C5 C35) petroleum hydrocarbons. The analytical results are provided in Appendix D.
- 5.21 The groundwater quality results from samples taken from the deep boreholes drilled into the Chalk aquifer are generally good. The metals are within EQS with the exception of dissolved manganese in BH07D, BH08D, BH09 and BH10D located towards the eastern side of the study site. All the other parameters, as listed above, analysed within the samples taken from the Chalk groundwater are within EQS and DWS.



- 5.22 The water quality of the groundwater samples from the shallow boreholes shows a significant number of parameters are within EQS and DWS. However, notably manganese is elevated across the study site; boron is elevated above DWS and nickel above DWS and EQS in BH07S and BH08S. Dissolved sodium is found at elevated concentrations in BH06S, BH08S, BH09S and BH10S. Total PAH is identified in BH08S at 0.7 μg/l; although not identified in the speciated hydrocarbon analysis results for this borehole. All other parameters are within DWS and EQS limits.
- 5.23 The water quality analysis finds that the surface water samples are mostly within EQS and DWS, with the exception of arsenic and boron above DWS whilst within EQS in SW01; and dissolved manganese above DWS and EQS in SW10.
- 5.24 Sodium and chloride are elevated only in BH07D in the deeper boreholes and in BH07S, BH08S and BH09S for the shallow boreholes; and only in SW06 for the surface water samples.



6. Hydrogeological Conceptual Site Model

Conceptual Model Framework

- 6.1 Conceptual models provide a framework to enable interpretation of the available information to provide validate and justifiable set of simplifying assumptions to describe the groundwater system (Brassington and Younger, 2010; Whiteman *et al*, 2012).
- 6.2 A phased approach based on the data availability is regarded as best practice when developing conceptual model. This phased approach is outlined in Rushton and Skinner (2012). Such that a Phase 1 Conceptual Model is built on the scoping stage data and understanding and on the Phase 1 field data collection, collation and analysis. Subsequent Phases of conceptual model development are based on testing the Phase 1 conceptual model with further data collation and interpretation to refine the conceptual understanding.
- 6.3 The conceptual model of the groundwater system and potential surface water interaction sets out to define the extent of the study area and lateral and vertical subdivisions based on the geology, hydrogeology, topography and drainage.
- 6.4 The conceptual model includes a description of the hydrogeological conditions and flows across the site and at its boundary based on observed groundwater levels in specific horizons and geologies and surface water flows, together with an understanding of the groundwater movement, the inflows and outflows with respect to the study area.
- 6.5 Furthermore, the conceptual model considers a plausible range of aquifer parameters and their variability across the site and within the specific geological lithologies encountered
- 6.6 The Phase 1 conceptual model, as described by Rushton and Skinner (2012), considers the limitations of the data, the inherent assumptions and the applicability of the conceptual model in the context of the data analysed. The level of confidence associated with the numerical model and the a view as to whether there limitations within the Phase 1 conceptual model could lead to model refinement with further targeted data collection and interpretation. The cyclic process of conceptual model development and testing is presented by the Environment Agency (2002) as referred to in Whiteman, *et al.* (2012), such that the initial conceptual model is developed, then tested prior to further model development and testing.



Initial Conceptual Understanding

- 6.7 From the information presented in Section 3 Ground Conditions and 4 Site Investigation Findings, the generalised conceptual understanding of the site and surrounding area has a number of primary features. The Newhaven Chalk forms the bedrock beneath the site and is underlain by the Seaford Chalk which forms the bedrock outcrops to the east and northeast from the site; and overlain by the Tarrant Chalk Member of the Culver Chalk Formation which outcrops to the west and northwest from the site. The Seaford Chalk, Newhaven Chalk and Tarrant Chalk form a continuous Principal Aquifer that underlies the site; and has an recharge area to the north of the A27, along the South Downs dip and scarpe slope.
- 6.8 The Chalk bedrock and aquifer beneath the site is entirely overlain by superficial deposits. The superficial deposits overlying the Chalk across the site broadly divided into the Head Deposits to centre and south; and Alluvium deposits to the north possibly extending to the central- east of the site. This sub –division is however, a little meaningless as both the Head and the Alluvium provide a confinement of the Chalk aquifer across the site.
- 6.9 The superficial Head Deposits are also found to the north of the A27, up to between approximately 75 metres to the north of the north-eastern site boundary corner to approximately 300 metres to north of the north-western site boundary corner. Beyond the Head Deposits to the north, the Chalk is unconfined. The conceptual understanding developed in this assessment asserts that the recharge for the Chalk aquifer occurs at the unconfined Chalk to the north of the Head Deposits where there is no confinement by the superficial deposits, therefore, beyond between 75 and 300 metres north of the A27 (ie 100m to 325m from the site).
- 6.10 There is a general understanding that effective rainfall-recharge of the Chalk aquifer occurs predominantly throughout the winter, and ceases with increasing temperature, soil moisture deficit and evapo-transpiration by plants during the later spring, summer and early autumn.
- 6.11 The elevation of the Chalk and the effective recharge means that the groundwater table is at higher elevation above sea level in the aquifer outcrop to the north of the A27 than to the south. The regional groundwater movement is from the outcrop southwards towards the sea and eastwards towards the River Adur. At the site, the surfer plots suggest that the eastwards flow towards the River Adur is dominant. Where the Adur has hydraulic interconnectivity with the Chalk, the Adur forms a hydraulic fixed head boundary to the Chalk groundwater system. The sea forms a fixed head boundary to the south; with either direct or indirect chalk groundwater-seawater interaction. In terms of the conceptual understanding, there is a presumption of west to east groundwater flow within the Chalk beneath the site.



- 6.12 The site is not within published groundwater protection zones of public or private water supply abstractions; and therefore understood not to be within the catchment of such abstractions. There are major public water supply abstractions from boreholes in the Chalk to the west of the site in the Northbrook and Broadwater areas of Worthing which are not expected to have an hydraulic impact on the site. The water flow is away from these locations. Furthermore, there is abstraction for public water supply in Shoreham however, because the Adur is understood to act as a hydraulic boundary, confirmed by the Source Protection Zones indicating their catchment is to the east of the Adur, this abstraction is understood not to affect groundwater movement in the Chalk beneath the site.
- 6.13 Topographically, the site is set on the coastal plain. The superficial Head and Alluvium deposits confine the Chalk aquifer. As such, the piezometric (or pressure) head within the confined Chalk aquifer is expected to be above the base of the superficial deposits. It is noted that with the site lying in a built environment that the 'high risk' of groundwater flooding classification for the site will more than likely have been predicted on the assumption that cohesive covers soils at the site were absent or could not be relied upon to provide an aquiclude.
- 6.14 Furthermore, whilst the Alluvium and Head deposits are variable gravelly clays, clays and silts the presence of fine sands and medium grained sands cannot be ruled out locally. Groundwater will pass through these superficial deposits via the sand matrix, along channel deposits and specific horizons. Nonetheless, both the Head Deposits and the Alluvium are shown to form an aquitard (with limited groundwater movement) or aquiclude (an effective barrier to a groundwater flow). This is likely to be more pronounced with the vertical direction than the lateral one. Therefore, the conceptual understanding asserts that a perched water table in the Alluvium and Head deposits will be found and that movement between the surface water and near surface perched groundwater and the Chalk aquifer beneath will be limited.

Conceptual Site Model Development

- 6.15 The data collected within this study tests the initial conceptual understanding.
- 6.16 Broadly, the piezometric data from the deeper boreholes confirms that the Chalk is semiconfined to the north the site and confined across the majority of the site. The Head Deposits confine the Chalk to the main body of the site; and the Alluvium deposits confine the Chalk to the northeast, north and part of the northwest of the study site.
- 6.17 To the southeast of the study area, the Chalk groundwater piezometry has a clear tidal signal, confirmed by water quality sampling in this area. The extent of tidal influence and interaction is discussed later in this section.
- 6.18 There is a distinct perched groundwater table within the Superficial Head and Alluvium deposits. The extent of the interaction with the surface water and Chalk groundwater at depth and at outcrop to the north is discussed in this section.



6.19 Furthermore, the period of study covered the period of above average monthly rainfall, a sequence of intense rainfall events and a rapid rise in groundwater levels within the Chalk which led to localised impacts of ephemeral springs and streams flowing from the Chalk on the Lancing area. These conditions were excellent in testing the conceptual understanding in terms of risks from groundwater flooding within the study site.

Surface Water - Groundwater Interaction

- 6.20 As discussed in Section 5, some of the observation borehole data shows evidence of interaction between the groundwater and surface water, whereas some of the other groundwater level data does not display direct correlation with longer and short term surface water data tends.
- 6.21 The degree to which water level in the shallow piezometers is affected by the surface water is a function of the proximity to the surface water and the elevation of the perched water table in the superficial deposits. As the site investigation and monitoring took place over a period of significantly above average monthly rainfall, the water table in the superficial deposits are interpreted to have established local mounds, with the elevation of the water table above the elevation of the nearby surface water features. Therefore, the surface water features were gaining water and not contributing significantly to the groundwater system over this period.
- 6.22 In contrast the monitored surface water levels appear to respond to changes in groundwater levels in the superficial Head and Alluvium deposits. This indicates that these features are gaining water from the perched groundwater in the superficial deposits.
- 6.23 The period over which the data was collected, was a period of above average monthly rainfall with a number of intense heavy rain storms occurring. The drainage system across the site responded to these events with elevated water levels within all the surface water level monitoring points. These levels reduced following cessation of the respective rain events, inferring a notable contribution from surface water drainage within their hydrographs.
- 6.24 However, there is also evidence of a notable baseflow component within these hydrographs; and a relationship between the water levels within the superficial deposits and the surface water levels. As the water levels in the superficial deposits are greater than the surface water levels, this relationship may relate to the rainfall response, such that the rainfall event adds to the groundwater storage and therefore imposes an increased driving head releasing this storage to the surface water drainage, whilst the rainfall response is also observed in the surface water system. To assess fully the degree of baseflow contribution from the perched groundwater in the superficial deposits, monitoring over a period of low or no rainfall would be required.

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Tidal Influence

- 6.25 As discussed above, a significant number of the surface water monitoring locations have a diurnal pattern within the logger data parallel with the tidal cycle. This is particularly with respect to the surface water monitoring locations to the south and east of the study site namely SW03, SW04, SW05, SW06, SW07, SW08 and SW10. This is notably pronounced at SW07 and SW10 to the southeast and northeast of the study area, respectively. The drainage pattern indicates that this hydraulic response is related to direct surface water interaction with the tidal estuary or marine environment; and is not considered directly or indirectly related to the groundwater hydraulics.
- 6.26 This is confirmed by the shallow observation boreholes which do not display a diurnal pattern attributable to the tidal cycle. Although there is evidence from some of the shallow observation borehole to indicate surface water groundwater interaction, the responsiveness in groundwater level is insufficient to show a tidal response. This may be a result of groundwater levels in the Alluvium are observed to be higher than that of the surface water, therefore the extent of groundwater to surface water interaction is one of aquifer drainage from the Alluvium to the drainage channels, rather than the other direction during the high water table conditions. Therefore the hydraulic response does not directly reflect changes in the surface water drainage depth.
- 6.27 Data from the deeper Chalk boreholes shows the piezometric surface is generally unaffected by the tidal cycle; with the one exception of BH07D which is located on the eastern end of the southern boundary of the study site. BH07D displays a clear tidal response, indicating direct hydraulic interaction with the marine or estuarine environment. This tidal response is not observed at BH06D drilled into the Chalk beneath Head deposits towards the southwest corner of the site. In terms of hydraulics, it therefore indicates rapid groundwater movement between the sea or estuarine water and the Chalk occurs at depth in the area of BH07D. The tidal hydraulic response identified in BH07D is not mirrored in the groundwater in the Alluvium above (ie in BH07S).
- 6.28 Sodium and chloride are elevated only in BH07D out of the deeper borehole monitoring set indicating confirmation of the marine or estuarine influence within the Chalk aquifer towards the southeast of the study area. The elevated sodium and chloride concentrations in BH07S, BH08S and BH09S towards the eastern boundary of the study site may be indicative of the tidal influence within the surface drainage, though as described above water quality measurement in low flow conditions would be required to add evidence for this observation.



6.29 Sodium and chloride concentrations within the surface water samples from the single sampling round identified elevated chloride and sodium concentrations only in SW06 – towards the southeast corner of the site. This may be reflected the position of the tide at the time of the sampling – such that the surface water samples were taken between 11:55 and 12:17 on 5 March 2014 and between 10:30 and 14:51 on 6 March 2014; and the high tide at Shoreham-by-Sea was at 13:57 on 5 March and 14:59 on 6 March 2014, therefore all samples were taken during a rising tide and do not necessarily reflect the surface water quality at or immediately following high tide. The quality may also reflect the predominance of surface water flows following the intense rainfall preceding the sampling round.

Above long term average rainfall events

- 6.30 The period of study coincided with an extremely high rainfall sequence which included a series of intense rainfall events. The Environment Agency (2014) reported that the area experienced three consecutive months with more than double the long term average rainfall during December 2013, January and February 2014.
- 6.31 The monitoring data needs to be considered within the context of this period of extreme rainfall. The data shows a response to this particularly in terms of the water levels in the surface water drainage across the study site and the water levels within the shallow boreholes. The piezometric surface within the Chalk aquifer is also understood to be have been significantly affected by the elevated groundwater levels within Chalk aquifer as a whole.
- 6.32 The conceptual understanding of the surface water, perched groundwater and deeper Chalk piezometric head above the level base of the superficial deposits across the site has been confirmed from the observation data and developed in the context of this extreme event.
- 6.33 Some of these effects are shown to have a relatively short duration, such that the piezometric levels in some of the deep boreholes notably BH02D were greater than the water level in the superficial deposits above BH02S at the start of February, with a notable decline in the Chalk piezometry to less than the piezometric head above by mid to late February 2014. The rainfall sequence at the end of January and beginning of February included a series of very intense, high rainfall events; with an initial response in piezometric level which drained with gravity via ephemeral springs and streams in the Chalk outcrop to the north of the A27, reducing the driving head over February as the excess groundwater storage was release from the Chalk aquifer.
- 6.34 The perched aquifer within the superficial deposits also responded to this rainfall sequence through localised groundwater mounds and notably higher water table than the surrounding surface water drainage system. The conceptual model would indicate that with prolonged low rainfall, the water level within the superficial deposits would deplete further and approach the water levels associated with the surface water drainage.



- 6.35 The water levels within the surface water drainage system were also high in response to these rainfall events, although drained quicker than the superficial perched aquifer and the Chalk aquifer beneath. The surface water drainage levels measured during the study period were strongly affected by the rainfall response, with tidal affects less prominent, and only towards the east of the study site.
- 6.36 The extreme above long term average rainfall events of the winter 2013/14 has enabled a robust assessment of risk from groundwater flooding. The site was not flooded in response to the elevated groundwater levels. However, the volume of ponded water, notably to the northwest of the study area, adjacent to Marsh Barn Lane immediately to the south of the A27 is a response to the intense rainfall and demonstrates the importance of the surface drainage channels in allowing this water to drain from this area.
- 6.37 There may be a contribution from the raised perched groundwater in the superficial deposits in response to the extreme rainfall sequence, and the associated release from perched groundwater storage of this excess groundwater. This too will drain into the surface water drainage system and therefore also demonstrates the importance of maintaining effective drainage of the site. Nonetheless, there were no observed effects of ground surface flooding within or surrounding the study site from the superficial deposits apart from an additional contribution to the flow and level surface water drainage system as the excess storage within the localised perched groundwater drained.
- 6.38 The superficial deposits are generally shown not to have direct hydraulic continuity with the Chalk aquifer beneath, and therefore act as an aquiclude or aquitard. This was confirmed with the Chalk piezometric surface was observed to rise above the level of the base of superficial deposits without direct hydraulic interaction.
- 6.39 Therefore, the study shows that the superficial deposits provide a substantive cover to the aquifer and groundwater from the Chalk would flow into the superficial deposits and potentially result in localised groundwater flooding and exacerbated surface water drainage if this natural cover provided by the superficial deposits was breached. There are building solutions available to stop such a breach occurring (e.g. use of raft foundations) but the detailed solutions are not part of this report.



7. Conclusions and Recommendations

Conclusions

- 7.1 This hydrogeological study has established an understanding of the groundwater hydraulics and interactions associated with the study site at New Monks Farm, North Lancing.
- 7.2 From the desk and field study, a conceptual model of the groundwater system associated with the study site has been developed and refined.
- 7.3 Furthermore, the period of the site investigation and monitoring coincided with the end of a period of three consecutive months with more than double the long term average rainfall; with localised surface and groundwater flooding occurring within the area and region (but not at the site). The data and observations made during this period have enabled a robust assessment of the risk of groundwater flooding from high water table levels at the site.
- 7.4 The Newhaven Chalk forms the bedrock geology to the site. The Chalk aquifer is recharged at its outcrop to the north of the A27, and is confined by superficial deposits over the entirety of the site, with semi-confinement just beyond the northern boundary of the site.
- 7.5 Towards the southeast of the study site, there is a tidal signal in the Chalk piezometry, inferring hydraulic connectivity between the Chalk aquifer and the marine or estuarine environment. This is not identified elsewhere across the deep monitoring borehole at the site.
- 7.6 However, the water levels in the shallow boreholes towards the eastern boundary of the study site also display a diurnal cycle that can be attributed to tidal fluctuation influence.
- 7.7 The superficial Head and Alluvium deposits overly the Chalk bedrock and form an aquiclude or aquitard, substantially limiting vertical groundwater movement between the Chalk and the near surface deposits. As a result, during the period of groundwater level monitoring, the Chalk aquifer beneath the site is confined with the piezometric surface above the base of the superficial deposits.
- 7.8 The superficial deposits act as an aquitard or aquiclude, with some evidence for low to very low vertical permeability, related to clays and silts within specific lateral continuous horizons within the Head and Alluvium deposits. This provides protection to the Chalk aquifer at depth and results in both a perched aquifer in the superficial deposits; and confinement of the Chalk aquifer.
- 7.9 The intense and substantially above average rainfall prior to and during the field monitoring has led to elevated water table levels in the superficial deposits, forming localised groundwater mounds. The excess groundwater storage is released via flows and seepages into the surface water drainage system. During the high rainfall event, the water level within the surface water drainage was observed to be lower than the perched groundwater mounds. Therefore, there is a component of perched groundwater contribution to the base flow .within the surface water drainage at the site.



- 7.10 There is no evidence to indicate that there is direct contribution to surface water flows from the Chalk aquifer at depth beneath the site.
- 7.11 It is noted that during the study period, excess groundwater storage was released from the unconfined Chalk aquifer to the north of the A27 via ephemeral springs and streams, resulting on localised groundwater flows and flooding in parts of the Lancing close to the A27 in February and March 2014. The groundwater flooding event in Lancing did not lead to groundwater flooding of the study site; although it may have contributed to additional flows within the surface water drainage across the site as the excess groundwater flowed (and was also pumped) from the affected areas, through the surface water drainage towards the River Adur, estuary and sea.
- 7.12 The observations made during the very high rainfall and groundwater conditions experienced in early 2014 show that the study site is not directly susceptible to groundwater flooding.
- 7.13 However, this is on the proviso that the surface drainage system is maintained to ensure its capacity to drain the site in terms of rainfall-runoff; tidal increase and movement; perched groundwater storage release and additional flows through the site from ephemeral groundwater springs and streams, including drainage from groundwater flooding events in the sites near environs.
- 7.14 Furthermore, this is on the second proviso that the superficial deposits maintain the confinement of the Chalk aquifer and are not breached. This is because groundwater monitoring during the study period indicates that the piezometric surface within the Chalk can be above the base of the superficial deposits, and a breach of these superficial deposits could result in a groundwater flow into the near surface perched aquifer, increased flow into the surface drainage system and the potential for localised ponding or flooding of the land surface.
- 7.15 During low groundwater conditions, such breaches if allowed to occur, may also lead to drainage of the perched water table into the Chalk aquifer beneath. This may have implication in terms of groundwater quality, particularly with respect to the elevated concentrations of parameters identified within the shallow boreholes and surface water drainage during the monitoring period which may enter the Chalk aquifer beneath.
- 7.16 The baseline water quality of the site has been established and may be of use to monitor future construction affects.

Recommendations

7.17 The field monitoring and associated desk study interpretation is based on a limited period during early 2014. Principally, this period included intense and prolonged above long term average rainfall and episode of groundwater flooding in the Lancing area to the north of the site. To fully evaluate the impact of groundwater on the baseflow within the surface drainage system, to further understanding the extent of vertical interconnectivity during periods of low water table and the tidal influence, there is value to continuing the monitoring to include a period of low rainfall and low groundwater levels. However, we consider that this will only refine the hydrogeology model rather than substantially change it.



- 7.18 It will be helpful to obtain further water level information from the EA historically monitored Sussex Pad well in order to have coincident information between that well and the site wells.
- 7.19 Any construction at this site should fully consider and have measures in place to avoid breaching the confinement of the Chalk by the overlying Head and Alluvium deposits. Building solutions to achieve this are available.



Figures

Figure 1 Site Location Plan (and EA monitoring wells) Figure 2 Site Geology Figure 3 EA Mapped Groundwater Risk Status Figure 4 Site Investiation Layout Figure 5 Geological Sections Figures 6a and 6b Groundwater piezometric surface for Superficials Figures 7a and 7b Groundwater piezometric surface for Chalk Figures 8a to 8f Borehole hydrographs Figure 8g Surface water hydrographs Figure 9 Development Proposals



LAYOUT FILENAME: F:/ZENV/!Projects/CS056361_ New_Monks_Farm/B.Work_Tasks/5.GIS/ARC/Mxds: CS056361_Fig1.mxd






LAYOUT FILENAME: F:/ZENV/!Projects/CS056361_ New_Monks_Farm/B.Work_Tasks/5.GIS/ARC/Mxds: CS056361_Fig5.mxd

















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Figure 8e: BH07 Hydrograph

700 10.0 650 5.0 600 0.0 550 500 **Groundwater Level (cm AOD)** 400 320 -5.0 Rainfall (mm/hr) -10.0 -15.0 300 ~~~~ www ~~~ 250 -20.0 \sim 200 -25.0 150 100 - -30.0 02/02/2014 07/02/2014 12/02/2014 17/02/2014 22/02/2014 27/02/2014 04/03/2014 Date – – – Groundlevel —— BH07S —— BH07D ------ Rainfall

We | Listen Create Deliver

CAPITA







NOTED PLAN EXTRACTED FROM NEW HONKS FARM MASTERPLAN FOR REFERENCE











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AWN BY	CHECKED BY	PASSED BY	DATE	SCALES @ A3 SIZE	IS
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New Monks Farm CS/05631 April 2014 Commercial in Confidence Appendix A

Appendix A

Harrison's Site Report

	2	ha	rrisor	ngrou	up	Percu	Issic	on Bo	reh	ole Re	cord		BH1	
						Project: Hy	ydroge	eological	Grou	nd Investig	ation, N	ew Mo	nks Farm, Wes	t Sussex
Project	ID · GI	18017				Coordinate	es: 51	9129.3E				Grour	nd Level: 2.47r	nAOD
Tiojeet		10017					10	5630.2N					Sheet 1 o	f 2
		Deceri	ation			Logond	Dept	1 O.D.	Sam	ples/ Test	Casing		Remarks	
		Descri	JUON			Legend	(m)	Level (m)	Туре	Depth (m)	Depth (m)	ר	and Fest Results	Installations
MADE GI slightly sa subangul tile.	ROUND andy CL lar fine t	. Light brow AY. Gravel o coarse fli	n slightly is angular nt, brick ar	gravelly to nd					B1	0.50	()			0.20
Firm orar CLAY. Gr fine to co matter.	ngish bro avel is s arse ch	own slightly subangular alk. Occas	r gravelly s to subrour ional organ	silty nded nic			- 0.90 	1.57	D1 U1	1.00 1.50-1.95		8 blc	ws: NR recovery	
Soft dark	grey sil	ty CLAY.					2.00	0.47	B2 D2	2.00 2.00				
									D3	3.00				3.00
									U2	4.00-4.45		10 blc	ws: 75% recovery	
									D4	5.00				
									D5	6.00				
									D6 D7	7.00 7.00				
									B3	8.00				
From 9.3	0m to 9	50m: Band	of fine to	coarse				7.02	De	0.50				
∖flint.					/		9.50	-7.03	00	9.50				
Continu	ued ne	ext sheet				p p a p p	0.00	7.40	1	Water Level	Observat	ions		
Hole Diameter	Diamete Depth	Details Casing	Ch	iselling De	etails Time	Date		Water		Standing	Stan	ding	Casing	Depth
200 150	9.50 15.00	<u>Depth (m)</u> 6.00 15.00	(m)	(m)	(hhmm)	23/01/14 23/01/14		Strike (r 5.50 9.00	n) -	Time (mins) 20 20	Leve 1.50 5.10	l (m) D D	Depth (m) 4.20 9.50	Sealed (m) 6.00
Client: Engine Contrac Dates: Plant: Drilled Loggeo Checke	er: (ctor: 2 By: By: By: ed By: \	Capita Capita Harrison Gr 23/01/2014 Dando 2000 D. Bowman P. Price J. Keay	oup Enviro	rcussive F	Ltd Rig	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instal from 15.00 from 5.00n tap/bung, 5. Backfill dei 5.00mbgl, and concre	I pit excav ter was e ntal seal lation def mbgl to 6 end cap tails: Grav tails: Grav gravel filt ete from 0	vated from G ncountered placed betw ails: 50mm (12.00mbgl, p L. Slotted fro and top hat d vel filter pack ver packs fro 0.20mbgl to	L to 1.20 at 5.50m een from diameter lain from m 5.00m cover. cs from 1 m 5.00m GL.	Imbgl. bgl and 9.50ml 5.00 to 6.00m HDPE standpij n 12.00mbgl to nbgl to 3.00mb 5.00mbgl to 12 bgl to 3.00mbg	J bgl. bgl. bgl. 50mm c GL. 50mm c gl, plain fron c.00mbgl, be l, bentonite	irom 15.00 liameter H n 3.00mbç ntonite pe pellets fro	Dmbgl to GL. Slotted IDPE standpipe instal It GL. Finished with ellets from12.00mbgl to m 3.00mbgl to 0.20m	led .gas o bgl
+M-Hn-R-308	80			Print Date:	04/04/2014			Harrison Gro	up Enviro	nmental Ltd, Ur	nit A11, Popla	ar Busines	s Park, 10 Prestons Ro	ad, London E14 9RL

harrisongroup	Percu	issio	n Bo	reho	ole Re	cord		BH1	
	Project: Hy	ydroge	ological	Groun	id Investig	jation, N	ew Moi	nks Farm, Wes	t Sussex
Project ID.: GL18017	Coordinat	es: 519	9129.3E				Groun	nd Level: 2.47r	nAOD
		105	5630.2N					Sheet 2 o	12
Description	Legend	Depth (m)	O.D. Level (m)	Samp Type	Depth (m)	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
9.50m - 9.90m : Structureless CHALK composed of slightly gravelly SILT. Clasts are very weak to weak low and medium density white. Matrix is light brown. 9.90m - 15.00m : Structureless CHALK composed of silty GRAVEL and COBBLES. Clasts are very weak to weak low and medium density white. Occasional subangular to				B4 U3 D9	10.00 11.00-11.45 11.00		25 blo	ows: NR recovery	
subrounded fine to coarse flint.	<u>, , , , , , , , , , , , , , , , , , , </u>			D10	12.00				12.00
	• p p p • • p p p			B5	13.00				
	<u>1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 </u>			D11	14.00				
Borehole Complete at 15.00 m	<u>•', r', r', r', r', r'</u> , r	15.00	-12.53	D12 U4	15.00 15.00-15.45		50 blo	ows: NR recovery	15.00
		E		<u>ا</u>	Vater I evel	Observet	ions		
Hole Diameter Details Chiselling Details			Water		Standing	Stan	dina	Casing	Depth
Diameter (mm)Depth (m)Casing Depth (m)From (m)To (m)Time (hhmm)2009.506.0015.0015.0015.00	Date 23/01/14 23/01/14		Strike (r 5.50 9.00	n) T	ime (mins) 20 20	Leve 1.50 5.10	<u>9</u> l (m))	Depth (m) 4.20 9.50	Sealed (m) 6.00
Client: Capita Engineer: Capita Contractor: Harrison Group Environmental Ltd Dates: 23/01/2014 Plant: Dando 2000 Cable Percussive Rig Drilled By: D. Bowman Logged By: P. Price Checked By: J. Keay	Remarks:								

	2	ha	rrisor	ngroi	up	Percu	issio	n Bo	reho	ole Re	cord		BH2	
						Project: H	ydroge	ological	Groun	nd Investig	ation, N	ew Mor	nks Farm, Wes	t Sussex
Project	ID · GI	18017				Coordinate	es: 519	9022.5E				Groun	d Level: 3.53	nAOD
riojoot	18 GE	10017					105	5454.6N					Sheet 1 c	f 1
		Descri	ption			Legend	Depth (m)	O.D. Level (m)	Samp Type	Depth	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
Brown sli Gravel is ∖and med	ghtly gra subang ium flint.	avelly silty o ular to subi	CLAY TOP rounded fir	SOIL. ne	/		0.40	3.13	D1	0.20				0.20
Soft to fir gravelly subround	m orang CLAY. G led fine	ish brown ravel is sul and mediu	slightly bangular to m flint.	D					B1 D2	1.00 1.00				
Firm orar slightly g subangul flint and o	ngish gre ravelly (lar to sul chalk.	ey mottled CLAY. Grav prounded f	off white vel is ine and mo	edium			2.70	0.83						2.00
Firm grey gravelly subround	/ mottlec CLAY. G led fine	l off white s ravel is sul to coarse fl	slightly bangular to lint and ch	o alk.	/		3.20	0.33	D3	3.30				3.00
Structure gravelly S low and r occasion staining.	less CH, SILT. Cla nedium al black	ALK compo sts are ver density wh specks an	osed of a v y weak to ite with d orange	rery weak			5.10	-1 57						
Structure GRAVEL weak low occasion	less CH and CO and me al yellow	ALK compo BBLES. Cla dium dens v staining.	osed of silt asts are ve ity white w	y ry weak ⁻ ⁄ith	to		- 5.10 	-1.57						
Structure GRAVEL weak low is very lig	less CH and CO and me ht brown	ALK compo BBLES. Cla dium dens n.	osed of silt asts are ve ity white. N	y ry weak : Matrix	to			-2.47		Water Level	Observat	ions		7.00
Hole	Diameter	Details	Ch	iselling D	etails			Water	`	Standing	Stan	dina	Casing	Denth
Diameter (mm) 200 150	Depth (m) 4.20 10.00	Casing Depth (m) 4.20 10.00	From (m)	To (m)	Time (hhmm)	Date 30/01/14		Strike (r 4.20	n) T	ime (mins) 20	2.00	9 l (m))	Depth (m) 4.00	Sealed (m) 5.00
Client: Engine Contrac Dates: Plant: Drilled Logged Checke	Cer: C Stor: F By: E By: F By: F d By: J	Capita Capita Iarrison Gr 0/01/2014 Oando 2000 D. Bowman D. Bowman D. Price . Keay	oup Envirc 31/01/201) Cable Per	onmental 4 cussive F Print Date:	Ltd Rig 04/04/2014	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instal 10.00mbgl 3.00mbgl 1 tap/bung, 5. Backfill de 3.00mbgl, and concre	I pit excava ter was en ntal seal p lation deta to 7.00m to GL. Slot end cap a tails: Grav gravel fil ete from C	ated from G countered a blaced betw isls: 50mm o bgl, plain fr ted from 3.0 nd top hat o el filter pack from 3.0 arrison Grou arrison Grou	L to 1.20r at 4.20mb diameter H diameter H oom 7.00m D0mbgl to sover. (s from 10 oom 3.00m GL. up Enviror	nbgl. gl. 3.20mbgl to 4 HDPE standpij nbgl to GL. 50 o 2.00mbgl, pla 0.00mbgl to 7. nbgl to 2.00mbg nmental Ltd, Ur	.20mbg. pe installed f mm diamete ain from 1.50 00mbgl, ben igl, bentonite	irom 10.00 or HDPE si Imbgl to G tonite pell pellets fro ar Business	Imbgl to GL. Slotted tandpipe installed fro iL. Finished with gas ets from 7.00mbgl to om 2.00mbgl to 0.20 s Park, <u>1</u> 0 Prestons Ro	rom m nbgl iad, London E14 9RL

	2	ha	rrisor	Igroi	up	Percu	issio	n Bo	reho	ole Re	cord		BH3	
				_		Project: H	ydroge	ological	Grour	id Investig	ation, N	ew Moi	nks Farm, Wes	st Sussex
Project	ID · GI	18017				Coordinate	es: 518	3960.4E				Grour	nd Level: 4.37	mAOD
Појесі		10017					105	5345.7N					Sheet 1 c	of 2
		Descri	otion			Legend	Depth (m)	O.D. Level (m)	Samı Type	Depth	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
MADE GI CLAY. Gr fine to co plastic fra Soft to fir	ROUND. avel is s arse me agments m orang	Brown slig ubangular dium flint, a	htly grave to subrour asphalt an	lly sandy nded d velly	, /		0.40	3.97	D1 B1	0.20				0.20
CLAY. Gr fine to co	avel is s arse flint	ubangular t.	to subrour	nded					D2	2 00				
From 2.0 gravelly o	0m to 2. clay. Gra	4m: Thin b vel is of ch	ands of off alk.	white			2.40	1.97	DE	2.00				-
Soft light sandy gra to subrou chalk. O	brown n avelly C unded fir ccasiona	nottled off LAY. Grave ne and mec al light grey	white sligh el is suban lium flint a v silty clay	tly gular nd					U1 D3	3.00-3.45 3.00		30 blo 30 b	ows: NR recovery blows: recovery	
Structure sandy grato to weak I	less CH avelly SI ow and i	ALK compo LT. Clasts a medium de	osed of slig are very we ensity, whit	ghtly eak e with	/		- 3.40	0.97	D4	3.60				
occasion brown.	al black	specs. Mat	trix is light						U2	5.00-5.45		100 bl	ows: NR recovery	
At 6.00m Structure GRAVEL weak low occasion	: Occasi less CH, and CO v and me al yellow	onal flint. ALK compo BBLES. Cla dium dens / staining.	osed of silt asts are ve ity white w	y ry weak t ith	to		7.00	-2.63	D5	8.00				
							-							
Continu	ued ne	xt sheet		in allies a D	ataila				\ 	Nater Level	Observat	ions		
Hole Diameter	Diameter Depth	Details Casing Depth (m)	Ch From (m)	To	etalls Time (hhmm)	Date		Water Strike (r	n) Т	Standing ime (mins)	Stan Leve	ding I (m)	Casing Depth (m)	Depth Sealed (m)
200 150	4.00 15.00	4.00 15.00				29/01/14 30/01/14		3.00 5.40		20 20	1.00))	2.80 5.00	4.00
Client: Engine Contrac Dates: Plant: Drilled Logged Checke	Cer: C Ctor: F 2 By: E d By: F ed By: J 30	Capita Capita Harrison Gru 19/01/2014- Dando 2000 D. Bowman D. Bowman D. Price	oup Enviro 30/01/201 Cable Per	onmental 4 cussive F Print Date:	Ltd Rig	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instail 15.00mbg 2.00mbgl and top ha 5. Backfil de 2.00mbgl, and concre	рit excava ter was en intal seal p llation deta to 12.00r to GL. Slot tt cover. tails: Grave gravel filte tete from 0.	ted from G countered a laced betw ils: 50mm c nbgl, plain 1 ted from 2.0 el filter pack r packs fro 20mbgl to 0	L to 1.20r at 3.00mk een from Jiameter I from 12.0 00mbgl to 00mbgl to xs from 15 m 2.00ml GL.	nbgl. ygl and 5.40ml 3.00mbgl to 4 HDPE standpi 0mbgl to GL. 1.00mbgl, pla 5.00mbgl to 12 bgl to 1.00mbgl to 1.00mbgl to 1.00mbgl to 1.00mbgl	bgl. .00mbg. pe installed 1 50mm diam ain from 1.00 2.00mbgl, be gl, bentonite	from 15.00 eter HDPB Imbgl to v Intonite pe pellets fro ar Business	Dmbgl to GL. Slotted E standpipe installed with gas tap/bung, er ellets from 12.00mbgl om 1.00mbgl to 0.20r	from from nd cap to nbgl vad. London F14 981

harrisongroup	Percu	ssio	n Bo	reho	ole Re	cord		BH3	
	Project: Hy	/drogec	logical	Grour	nd Investig	ation, N	ew Mor	nks Farm, West	Sussex
Project ID.: GL18017	Coordinate	es: 518	960.4E				Groun	d Level: 4.37n	hAOD
		105	345.7N					Sheet 2 of	2
Description	Legend	Depth (m)	O.D. Level (m)	Samı Type	Depth (m)	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
Brehole Complete at 15.00 m			-10.63						12.00
Hole Diameter Details Chiselling Details			Water		Standing	Stan	ding	Casing	Depth
Diameter Depth Casing From To Time (mm) (m) Depth (m) (m) (m) (hhmm)	Date		Strike (r	n) T	ime (mins)	Leve	l (m)	Depth (m)	Sealed (m)
200 4.00 4.00 150 15.00 15.00	29/01/14 30/01/14		3.00 5.40		20 20	1.00)	2.80 5.00	4.00
Client: Capita Engineer: Capita Contractor: Harrison Group Environmental Ltd Dates: 29/01/2014-30/01/2014 Plant: Dando 2000 Cable Percussive Rig Drilled By: D. Bowman Logged By: P. Price Checked By: J. Keay FM-Hn-R-3080 Print Date: 04/04/2014	Remarks:	Ha	ırrison Groı	up Enviror	nmental Ltd. Ur	nit A11, Poole	r Business	Park, 10 Prestons Ro	ad, London E14 9RL

	2	ha	rrisor	Igroi	qr	Percu	Issic	on Bo	reho	ole Re	cord		BH4	•
						Project: Hy	ydroge	eological	Grour	nd Investig	ation, N	ew Moi	nks Farm, Wes	st Sussex
Proiect	ID.: GL	18017				Coordinate	əs: 51	8960.4E				Groun	nd Level: 3.72	mAOD
							10	5290.7N					Sheet 1 o	of 1
		Descri	ption			Legend	Depth (m)	n O.D. Level (m)	Samı Type	Depth (m)	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
Dark bro silty CLA to subrou chalk.	wn slight Y TOPSC unded fir	ly gravelly DIL. Gravel le and med	slightly sa is subang dium flint a	ndy ular nd			- 0.10 - 0.15 -	3.62 3.57	D1 B1	0.10				0.20
MADE GI CHALK.	ROUND.	Off white o	comminute	d					D2	1.00				
MADE GI sandy sli subangu \concrete	ROUND. ghtly gra lar to sul , asphalt	Soft orang velly CLA prounded f , flint and c	jish brown Y. Gravel is ine to coar chalk.	slightly s se			 	1.82	U1 D3	1.50-1.95 2.00		20 blo	ws: 85% recovery	2.00
Soft light sandy sli subangu flint and o	brown n ghtly gra lar to sul chalk.	nottled off velly CLA prounded f	white sligh Y. Gravel is ine to coar	tly s se			2.50	1.22	B2 D4	2.50 2.50				2.90
Soft light sandy gra to subrou chalk.	brown n avelly CL Inded fir	nottled whi AY. Grave le to coarse	te slightly I is subang e flint and	jular			3.20	0.52 0.22	D5	3.50				
Structure SILT. Cla medium specs. M	less CH, sts are v density v atrix is li	ALK compo ery weak to vhite with c ght brown.	osed of gra o weak low occasional	avelly / and black		* * * * * * * * * * * * * * * * * * *		-1.08	U2	4.50		20 blo	ows: NR recovery	
Structure GRAVEL weak low occasion brown.	less CH and CO and me al black	ALK compo BBLES. Cla dium dens specks. Ma	osed of silt asts are ve ity white, v atrix is ligh	y ry weak t vith t	o	· · · · · · · · · · · · · · · · · · ·								
Structure GRAVEL weak low Occasion	less CH, and CO and me nal flint.	ALK compo BBLES. Cla dium dens	osed of silt asts are ve ity white.	y ry weak †	o									7.00-
									B3	9.00				
Borehole	Comple	te at 10.00	m						١	Water Level	Observat	ions		
Hole Diameter	Diameter Depth	Details Casing	Ch From	iselling D To	etails Time	Date		Water		Standing	Stan	ding	Casing	Depth
(mm) 200 150	(m) 0.00 10.00	Depth (m) 3.50	(m)	<u>(m)</u>	(hhmm)	24/01/14		Зтике (r 2.50		20	1.00))	2.00	Sealed (M)
Client: Engine Contrac Dates: Plant: Drilled Logged Checke	Cer: C Ctor: F 2 By: C By: C H By: F ed By: J	Capita Capita Iarrison Gr 4/01/2014 Dando 2000 D. Bowman D. Bowman D. Price . Keay	oup Envirc	onmental cussive F	Ltd	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instal from 10.00 2.90mbgl cap and to 5. Backfill dei 2.90mbgl, and concre	pit excav ter was en ntal seal lation det mbgl to 7 o GL. Sic p hat cov ails: Grav gravel filt gravel filt	rated from G ncountered : placed betw ails: 50mm d 7.00mbgl, pla tited from 1.9 rer. rel filter pack er packs froi 0.20mbgl to	L to 1.20r 2.50mbgl een from diameter I ain from 7 90mbgl to 90mbgl to 90mbg	mbgl. 3.50mbgl to 2 HDPE standpij 7.00mbgl to GL 2.90mbgl, pla 0.00mbgl to 7.0 ggl to 1.90mbg	.50mbg. be installed f 50mm diau ain from 1.90 00mbgl, ben I, bentonite	rom 10.00 meter HDF mbgl to G tonite pell pellets from	mbgl to GL. Slotted PE standpipe installe L with gas tap/bung ets from 7.00mbgl to 1.90mbgl to 0.20m	d from , end hbgl

	2	ha	rrisor	igrou	ıp	Percu	Issio	n Bo	reho	ole Re	cord		BH5	
						Project: Hy	ydroged	ological	Grour	id Investig	ation, N	ew Mor	nks Farm, Wes	t Sussex
Project	וח · כו	18017				Coordinate	es: 519	165.6E				Groun	id Level: 2.63	mAOD
Tojeci		10017					105	112.1N					Sheet 1 c	of 1
		Descri	ption			Legend	Depth (m)	O.D. Level (m)	Samp Type	oles/ Test Depth (m)	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
Dark bro CLAY TO subround	wn sligh PSOIL. led fine	tly gravelly Gravel is su to coarse fl	slightly sa ubangular i lint.	ndy to	/		0.30	2.33	D1 B1	0.20	(11)			0.20
Soft oran gravelly (subround	gish bro CLAY. G led fine	own slightly ravel is sub and mediu	sandy slig bangular to m flint.	jhtly	/				B1 C	1.00		N=	·6 (1,2,1,2,1,2)	1.50
Soft to fir white slig CLAY. Gr fine and r	m orang htly silty avel is s medium	ish brown slightly gr ubangular flint and ch	mottled off avelly to subrour nalk.	nded				0.93	C U1 D2	2.50 2.50-2.95 3.00		N= 30 blo	7 (1,2,2,1,2,2) ws: NR recovery	2.50
Structure SILT. Cla medium specs.	less CH sts are v density ⁻	ALK compo rery weak to white with c	osed of gra o weak low occasional	avelly v and black			- 3.80	-1.18	B2 U2	4.00 5.00-5.45		50 blc	ows: NR recovery	
Structure GRAVEL weak low	less CH and CO and me	ALK compo BBLES. Cla dium dens	osed of silt asts are ve ity white.	y ry weak t	D			-2.88	D3	6.00				7.00
Borehole	Comple	ete at 10.00) m							Nater Level	Observat	ions		
Hole Diameter	Diamete Depth	Details Casing	Ch From	ISelling De	Time	Date		Water Strike (n	n) T	Standing	Stan	ding I (m)	Casing Depth (m)	Depth Sealed (m)
200 150	3.80 10.00	3.80 10.00	(111)	((11)	<u>(mann)</u>	29/01/14 29/01/14		2.20 3.80	., 1	20 20 20	1.50)	3.50	3.80
Client: Engine Contrac Dates: Plant: Drilled Logged Checke	er: (ctor: 2 By: HBy: ed By: 100	Capita Capita Harrison Gr 28/01/2014 Dando 2000 D. Bowman P. Price I. Keay	oup Envirc -29/01/201) Cable Per	onmental 4 cussive R Print Date:	Ltd ig 04/04/2014	Remarks: 1. Inspection 2. Groundwal 3. Environme 4. Dual Instal from 10.00 2.50mbgl t tap/bung, 1 5. Backfill det 2.50mbgl, and concre	pit excava ter was enc ntal seal pi lation detai mbgl to 7.1 o GL. Slott end cap ar tails: Gravel filte: Gravel ate from 0.2	ted from G countered a aced betwi Is: 50mm c Dombgl, pla ed from 2.5 d top hat c l filter pack f placks from 20mbgl to 0	L to 1.20r at 2.20mb een from liameter H ain from 7 50mbgl to 50mbgl to 50mbgl to 50mbgl to 50mbgl to 50mbgl to 50mbgl 10 L 50mbgl 3L.	nbgl. 2.80mbgl to 3 4DPE standpip .00mbgl to GL 1.50mbgl, pla 0.00mbgl to 7.0 .00mbgl to 7.0 .00mbgl to 1.50mbg	bgl. 80mbg. be installed f 50mm diar in from 1.50 00mbgl, ben I, bentonite j it A11, Popla	rom 10.00 meter HDF mbgl to G otnite pell pellets fro r Business	mbgl to GL. Slotted PE standpipe installer iL. Finished with gas ets from 7.00mbgl to m 1.50mbgl to 0.20m s Park, 10 Prestons Ro	d from Ibgl vad, London E14 9RL

	2	ha	rrisor	ngroi	Jp	Percu	Issio	n Bo	reho	ole Re	cord		BH6	
						Project: Hy	ydrogeo	ological	Groun	id Investig	ation, N	ew Mo	nks Farm, Wes	t Sussex
Project	ID.: GI	18017				Coordinat	es: 518	8917.0E				Grour	nd Level: 3.95r	nAOD
	GL						105	5114.7N					Sheet 1 o	f 1
		Descri	ption			Legend	Depth (m)	O.D. Level (m)	Samp Type	Depth (m)	Casing (Water) Depth (m)	г	Remarks and ſest Results	Installations
Dark brow TOPSOIL fine to co rootlets.	wn sligh Gravel arse flin	tly gravelly is subangi t and chalk	silty CLAY ular to sub Occasior	rounded nal	/		0.40	3.55	D1	0.20				0.20
Soft light CLAY. Gr fine to co	brown s avel is s arse flin	lightly grav ubangular t and chalk	velly silty to subrour 	nded	/				B1 U1	1.00 1.50-1.95		20 blo	ows: 85% recovery	
								1.95	D2	2.00				2.00
Soft light silty CLA' subround	brown r Y. Grave led fine	nottled off I is subang and mediu	white grav gular to m flint and	elly chalk.				1.65	B2	3.00-3.60				
Structure SILT. Cla medium specs. O	less CH sts are v density v ccasiona	ALK compo rery weak to white with c al flint.	osed of gra o weak low occasional	avelly v and black			- 4.80 	-0.85	U2 D3 U3	5.00-5.45 6.00 6.00-6.45		,	No Recovery No Recovery	
Structure GRAVEL weak low Occasior	less CH and CO and me nal flint.	ALK compo BBLES. Cla dium dens	osed of silt asts are ve ity white.	y ry weak t	to		6.40	-2.45	B3 U4	7.00 7.00-7.45		,	No Recovery	
From 8.5 flint grave	0m to 9. ୬l.	60m: Occa	asional bar	nds of					U5	9.00		100 blo	ows: 65% recovery	
Borehole	Comple	ete at 10.00) m						\	Water Level	Observat	ions		
Hole Diameter	Diameter Depth	Details Casing	Ch From	iselling D To	etails Time	Date		Water	<u></u>	Standing	Stan	ding	Casing	Depth
(mm) 200 150	(m) 5.00 10.00	Depth (m) 5.00 10.00	(m)	(m)	(hhmm)	27/01/14 28/01/14		3.00 7.00	<u>n) T</u>	20 20 20	1.00 3.60	n (m) D D	2.50 10.00	Sealed (m) 4.20
Client: Engine Contrac Dates: Plant: Drilled Loggec Checke	er: C ctor: F 2 By: C By: C b By: S od By: S	Capita Capita Harrison Gr 27/01/2014 Dando 2000 D. Bowman D. Price I. Keay	oup Enviro -28/01/201) Cable Per	onmental 4 cussive F Print Date:	Ltd Rig 04/04/2014	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Install 10.00mbg 3.00mbgl tap/bung, 5. Backfill de 3.00mbgl, and concre	pit excava ter was en intal seal p lation deta to 7.00ml o GL. Slott end cap ar tails: Grave gravel filt ete from 0	ted from G countered i laced betw ils: 50mm o bgl, plain fi ted from 3.1 d top hat o al filter pack er packs fro .20mbgl to arrison Grou	L to 1.20r at 3.00mb diameter H om 7.00m 00mbgl to cover. (ss from 10 om 3.00m GL.	nbgl. gl and 7.00ml 5.50mbgl to 4 HDPE standpip bgl to GL 50 2.00mbgl, pla 0.00mbgl to 7.0 bgl to 2.00mbg nmental Ltd. Ur	ogl. .50mbg. be installed f mm diamete ain from 2.00 00mbgl, ben gl, bentonite	from 10.00 er HDPE s Dmbgl to G notnite pell e pellets fr ar Business	Dmbgl to GL. Slotted f tandpipe installed fro 3L. Finished with gas lets from 7.00mbgl to om 2.00mbgl to 0.20r s Park, 10 Prestons Ro	rom m nbgl ad, London E14 9RL

	2	ha	rrisor	ngrou	q	Percu	Issic	on Bo	reho	ole Re	cord		BH7		
						Project: H	ydroge	ological	Grour	nd Investig	ation, N	ew Mo	nks Farm, Wes	t Sussex	(
Proiect	ID.: GI	18017				Coordinat	es: 51	9321.8E				Grour	nd Level: 4.87r	nAOD	
							10	5102.8N					Sheet 1 o	f 2	
		Descri	ption			Legend	Depth (m)	n O.D. Level (m)	Samp Type	Depth (m)	Casing (Water) Depth (m)	F I	Remarks and Fest Results	Install	ations
MADE Gi sandy gi subangu medium ceramic a	ROUND avelly s ar to su flint, bric and met	Very soft b Ity CLAY. G brounded f k and chall al fragment	brown sligh Gravel is ine to coar k with glas s.	ntly rse is,	/		- - - - - - - - - - -	4.27	D1 B1	0.20					
MADE GI CLAY, w angular t brick and organic r	ROUND ith a low o suban l cerami natter. C	Soft dark I cobble co gular fine to fragments obbles are	brown grav ntent. Grav o coarse fli s. Occasio of concre	velly vel is int, nal te.					D2	2.00				2.00	
At 2.90m	: Concre	ete slab.						1 97	D2	3.50					
Firm brov Gravel is medium	vnish gr subang flint and	ey sandy g ular to subr chalk.	ravelly CL rounded fir	AY. ne and				1.37	U1	4.00-4.45			No Recovery		
Soft to fir CLAY. Gr fine and the fine and the sandy gr to weak I Matrix is Structure GRAVEL to weak I	less CH avel is s medium less CH avel y SI ow and light bro less CH and CO ow and	ALK compo The second se	ly gravelly to subrour nalk. Desed of slig are very we ensity, whit	nded ghtly eak e. ndy silty ry weak e.			7.50	-2.63	U1 B2 U2	4.00-4.45 4.00 4.45-4.95		15 blo	No Recovery ws: 100% recovery	9.00	
Continu	ued ne	xt sheet				p p p p p p	1		1	Nater Level	Observat	ions			
Hole	Diameter	Details	Ch	iselling De	etails	Data		Water		Standing	Stan	ding	Casing	Dept	th
Diameter (mm) 200 150	Depth (m) 7.70 12.00	Casing Depth (m) 7.50 12.00	From (m)	То (m)	Time (hhmm)	04/02/14 05/02/14		Strike (r 1.60 7.50	n) T	ime (mins) 20 20	Leve 0.40 1.00	l (m) D D	Depth (m) 1.50 7.50	Sealed 2.50	(m) D
Client: Engine Contrac Dates: Plant: Drilled Logged Checke	ctor: (ctor: F By: [By: F d By: S sol By: S	Capita Capita Harrison Gr 04/02/2014- Dando 2000 D. Bowman D. Bowman P. Price I. Keay	oup Enviro 05/02/201) Cable Per	onmental 4 cussive F	Ltd lig 04/04/2014	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instal 12.00mbg 2.00mbgl and top he 5. Backfil de 2.00mbgl, and concre	l pit excav ter was e ntal seal llation det I to 9.00n to GL. Slo to GL. Slo to GL. Slo tatls: Grav gravel fi gravel fi	ated from G ncountered placed betw alls: 50mm of nbgl, plain fr nbgl, plain fr titted from 2.1 vel filter packs fr 0.20mbgl to Harrison Grou	iL to 1.20r at 1.60mb veen from diameter I com 9.00n 00mbgl tc ks from 12 00m 2.00m GL. up Enviror	nbgl. ogl and 7.40ml 6.50mbgl to 7 HDPE standpj bbgl to GL. 50 1.00mbgl, pla 2.00mbgl to 9. bbgl to 1.00mb	J 50mbg. pe installed to mm diamete ain from 1.00 00mbgl, ber gl, bentonite	from 12.00 ar HDPE s)mbgl to atonite pel a pellets fr ar Busines	Dombgi to GL. Slotted from standpipe installed from with gas tap/bung, en- lets from 9.00mbgi to om 1.00mbgi to 0.20m s Park, 10 Prestons Ro	rom m d cap nbgl ad, London I	E14 9R∟

	2	ha	rrison	igroi	qr	Percu	issio	n Bo	reho	ole Re	cord		BH7	
						Project: H	ydroged	ological	Groun	nd Investig	ation, N	ew Moi	nks Farm, Wes	t Sussex
Project	ID · GI	18017				Coordinat	es: 519	321.8E				Grour	nd Level: 4.87r	nAOD
							105	102.8N					Sheet 2 o	f 2
		Descri	otion			Legend	Depth (m)	O.D. Level (m)	Samp Type	Depth	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
Structure GRAVEL to weak I	eless CH and CO ow and	ALK compo BBLES. Cla medium de	osed of sar asts are ve onsity, white	ndy silty ry weak e.			12.00	-7.13	U3	12.00-12.45		100 Ы	ows: NR recovery	12.00
Borehole								-7.13					ows: NH recovery	
Hala	Diamata	, Dotoilo	Ch						<u>۱</u>	Nater Level	Observat	ions		
Hole Diameter	Depth	Casing	Erom (m)		Time	Date		Water Strike (r	n) т	Standing ime (mins)	Stan Leve	ding I (m)	Casing Depth (m)	Depth Sealed (m)
200 150	7.70 12.00	7.50 12.00	(111)	(11)	(((((((((((((((((((((((((((((((((((((((04/02/14 05/02/14		1.60 7.50	,	20 20	0.40))	1.50 7.50	2.50
Client: Engine Contra Dates: Plant: Drilled Logged Checke	(er: (ctor:) By:] d By:] d By: 3 30	L Capita Capita Harrison Gr 04/02/2014 Dando 2000 D. Bowman P. Price J. Keay	oup Envirc 05/02/201 Cable Per	onmental 4 cussive F Print Date:	Ltd lig 04/04/2014	Remarks:	Ha	urrison Grou	μρ <u>Env</u> iror	nmental Ltd, Ur	I nit A11, Popla	ar Business	s Park, 10 Prestons Ro	ad, London E14 9RL

	2	ha	rrisor	Igroi	up	Percu	Issio	n Bo	reho	ole Re	cord		BH8	
						Project: Hy	ydroge	ological	Grour	nd Investig	ation, N	ew Mor	nks Farm, Wes	t Sussex
Project	ID · GI	18017				Coordinate	es: 519	9426.8E				Groun	d Level: 3.56	nAOD
Tiojoot	ib ai						105	5323.2N					Sheet 1 c	f 1
		Descri	ption			Legend	Depth (m)	O.D. Level (m)	Samı Type	Depth	Casing (Water) Depth (m)	Т	Remarks and est Results	Installations
MADE GI gravelly (subangul asphalt a	ROUNE CLAY. G lar fine .nd glas). Brown slig Gravel is ang to coarse co is fragments	ghtly sandy gular to oncrete, br s.	r slightly ick,	/		0.50	3.06	D1 D2	0.10				0.20
MADE GI to sandy clayey SI subangul and glass organic n fibres.	ROUNE slightly LT. Gra lar fine s fragm natter a	D. Dark grey gravel to g vel is angul to coarse a ents. Frequ nd occasio	r/black slig ravelly lar to sphalt, cera ent decom nal synthet	ntly sand amic posed ic	y		220	136	D3 ES1	1.00 1.50				2.00
Soft to fir Gravel is coarse cl	m brow subanç nalk.	n and grey gular to sub	gravelly C rounded fir	LAY.			· 2.20	1.35	D4	2.50				
Structure gravelly S low and r light brov	less CH SILT. CI medium vn.	IALK comp asts are ver a density, w	osed of sar y weak to hite. Matrix	ndy weak is			4.80	-1.24	D5	5.00				
Structure GRAVEL weak low occasion	less CF and CC and m al yello	IALK comp DBBLES. CI edium dens w staining.	osed of silt asts are ve sity, white v	y ry weak ⁻ vith	to			-2.64						7.00
Borehole	Comp	ete at 10.00) m							Water Level	Observat	ons		
Hole Diameter	Diamete Depth	Casing	Ch From	iselling D	etails Time	Date		Water	n) T	Standing	Stan	ding	Casing	Depth Sealed (m)
(mm) 200 150	(m) 5.00 10.00	5.00 10.00	(m)	(m)	(hhmm)	03/02/14		4.80		20	1.20)	4.00	5.00
Client: Engine Contrac Dates: Plant: Drilled Loggec Checke	er: ctor: By: d By: ed By: 30	Capita Capita Harrison Gi 03/02/2014 Dando 2000 D. Bowmar P. Price J. Keay	roup Envirc -04/02/201) Cable Per	onmental 4 cussive F Print Date:	Ltd Rig 04/04/2014	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instal 7.00mbgl 1 2.00mbgl 1 and top ha 5. Backfill de 2.00mbgl, and concre	pit excava ter was en intal seal p lation deta to 9.00mbg o GL. Slot tt cover. tails: Grave gravel fill ete from C	ated from G countered laced betw ills: 50mm o J, plain from ted from 2.0 el filter pack er packs fro .20mbgl to arrison Grou	L to 1.20r at 4.80mk een from diameter I n 7.00mbgl to Sombgl to Som 10 om 2.00rr GL. up Enviror	mbgl. ogl. 5.00mbgl to 4 HDPE standpij gl to GL. 50m b 1.00mbgl, pla 0.00mbgl to 7. hbgl to 1.00mbg nmental Ltd, Ur	.00mbg. pe installed f im diameter ain from 1.00 00mbgl, ben gl, bentonite nit A11, Popla	rom 10.00 HDPE sta mbgl to v tonite pell pellets fro r Business	Imbgl to GL. Slotted f ndpipe installed from vith gas tap/bung, er ets from 7.00mbgl to om 1.00mbgl to 0.200 s Park, 10 Prestons Ro	rom Id cap nbgl ad, London E14 9RL

harrisongroup					qr	Percu	Issia	on Bo	reho	ole Re	cord		BH9)
						Project: Hy	ydroge	eological	Grour	nd Investig	jation, N	ew Mor	nks Farm, We	st Sussex
Project I	D · GI	18017				Coordinate	es: 51	9315.5E				Ground Level: 4.02mAOD		
Појсски	D.: GL	10017					10)5501.7N					Sheet 1 of 2	
		Descri	otion			Legend	Deptl (m)	h O.D. Level (m)	Samı Type	Depth	Casing (Water) Depth (m)	т	Remarks and est Results	Installations
Brown slig Gravel is and medi	ghtly gra subangi um flint,	avelly silty (ular to subr chalk, bric	CLAY TOP rounded fir k and asp	SOIL. ne halt.	/		0.20	3.82	D1	0.10				- 0.20
MADE GF sandy slig CLAY. Gra to coarse flint	MADE GROUND. Light brown slightly sandy to sandy slightly gravelly to gravelly sity CLAY. Gravel is angular to subangular fine to coarse concrete, brick, asphalt and flint MADE GROUND. Soft dark bluish grey and dark brown slightly gravelly sity CLAY. Gravel													
MADE GF dark brov is angular brick, cha	MADE GROUND. Soft dark bluish grey and dark brown slightly gravelly silty CLAY. Gravel is angular to subangular fine to coarse brick, chalk and flint.						2.40 2.60 2.80	1.62 1.42 1.22	B1 D2 U1 D3	2.50 2.50 3.00-3.45 3.00		٦	No Recovery	
Soft bluish grey and brown gravelly silty CLAY. Gravel is subangular to subrounded fine and medium flint and chalk.						3.60	0.42							
Soft light brown gravelly silty CLAY. Gravel is subangular to subrounded fine and medium chalk.														
Soft bluis Gravel is medium f	h grey g subangi lint and	ravelly silty Jar to subr chalk.	/ CLAY. ounded fir	ne and					D4	5.00				
Soft bluis silty CLAY subround	h mottle 7. Grave led fine a	d off white I is subang and mediu	grey grave ular to m chalk.	əlly			6.20	-2.18						
Structurel gravelly S low and n occasiona	less CH, SILT. Cla nedium al yellow	ALK compo sts are ver density, wh v staining.	osed of sar y weak to v hite with	ndy weak			7.00	-2.98						
Structurel GRAVEL. and medi yellow sta	less CH Clasts a um den ining.	ALK compo are very we sity, white v	osed of silt ak to weał with occas	y (low ional										9.00
Continu	ied ne	xt sheet							N	Water Level	Observat	ions		
Hole I Diameter (mm) 200 150	Diameter Depth (m) 7.20 12.00	Details Casing Depth (m) 7.20 12.00	Ch From (m)	iselling De To (m)	etails Time (hhmm)	Date 31/01/14 31/01/14		Water Strike (r 1.20 7.10	n) T	Standing Time (mins) 20 20	Stan Leve 0.20 1.50	ding I (m)))	Casing Depth (m) 1.20 7.10	Depth Sealed (m) 3.00
Client: Capita Engineer: Capita Contractor: Harrison Group Environmental Ltd Dates: 31/01/2014-03/02/2014 Plant: Dando 2000 Cable Percussive Rig Drilled By: D. Bowman Logged By: P. Price Checked By: J. Keay					Ltd Rig 04/04/2014	Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instal 12.00mbgl 2.00mbgl and top ha 5. Backfill de 2.00mbgl, and concre	pit excan ter was e ental seal lation de to 9.00 to GL. Slo t cover. tails: Gra gravel f	vated from G encountered i placed betw tails: 50mm of mbgl, plain fr otted from 2.0 wel filter pack filter packs fro 0.20mbgl to Harrison Grou	L to 1.20n at 1.20ml een from liameter om 9.00r 00mbgl to 00mbgl to cs from 1: om 2.00m GL.	mbgl. 9g and 7.1mbg 6.20mbgl to 7 HDPE standpi nbgl to GL. 50 5 1.00mbgl, pla 2.00mbgl to 9. nbgl to 1.00mbg nmental Ltd, Ur	J. .20mbg. pe installed t mm diamete ain from 1.00 00mbgl, ber gl, bentonite	rom 12.00 ar HDPE si Imbgl to v tonite pell pellets fro ar Business) Dmbgl to GL. Slotted tandpipe installed fr with gas tap/bung, er lets from 9.00mbgl to om 1.00mbgl to 0.20 s Park, 10 Prestons R	from ym nd cap mbgl pad, London E14 9RL

	harrisongroup					Percu	Percussion Borehole Record BH9								
						Project: Hy	ydrogeo	ological	Groun	id Investig	ation, N	ew Mor	nks Farm, West	Sussex	
Project	ID.: GL	.18017				Coordinate	es: 519	315.5E				Groun	Ground Level: 4.02mAOD		
,							105	501.7N					Sheet 2 of	2	
		Descri	otion			Legend	Depth (m)	O.D. Level (m)	Samp Type	Depth (m)	Casing (Water) Depth (m)	т	Remarks and est Results	Installa	tions
Structure GRAVEL and med yellow sta	GRAVEL. Clasts are very weak to weak low and medium density, white with occasional yellow staining. Borehole Complete at 12.00 m						12.00	-7.98	U2	12.00-12.45		100 bl	ows: NR recovery	12.00	
Borehole Complete at 12.00 m								-7.98	02	12.00-12.45		100 bi	ows: NR recovery		
Hala	Diamata	r Dotoilo	Chi						V	Vater Level	Observat	ions			
Diameter	Depth	Casing	From (m)		Time (hbmm)	Date		Water Strike (n	n) T	Standing ime (mins)	Stan Leve	ding I (m)	Casing Depth (m)	Depth Sealed (r	m)
200 150	7.20 12.00	7.20 12.00	(111)	(11)	(11111111)	31/01/14 31/01/14		1.20 7.10	,	20 20 20	0.20)	1.20 7.10	3.00	
Client: Engine Contrad Dates: Plant: Drilled Logged Checke	er: (ctor: By: By: By: d By:	L Capita Capita Harrison Gr 31/01/2014- Dando 2000 D. Bowman D. Bowman P. Price J. Keay	oup Enviro 03/02/2014 Cable Per	onmental 4 cussive F <u>Print D</u> ate:	Ltd Rig 04/04/2014	Remarks:	Ha	urrison Grou	ıp Environ	imental Ltd, Ur	I	r Business	s Park, 10 Prestons Roa	id, London E1	14 9RL

	harrisongroup						issic	on Bo	reho	ole Re	cord		BH1	0	
						Project: Hy	ydroge	ological	Grour	nd Investig	ation, N	ew Mo	nks Farm, We	st Sussex	
Project	ID · GI	18017				Coordinate	es: 51	9338.1E				Ground Level: 2.96mAOD			
Tiojecti		10017					10	574.9N					Sheet 1 o	of 2	
		Descri	otion			Legend	Depth (m)	O.D. Level (m)	Samı Type	Depth	Casing (Water) Depth (m)	т	Remarks and Fest Results	Installa	tions
MADE GF slightly sa subangul	ROUND. andy CL ar fine to	Orangish I AY. Gravel coarse flir	brown grav is angular nt, brick.	velly to						(11)					
Soft grey	silty CL	AY.				x - x - x - x - x - x - x - x - x - x -	1.00	1.96	B1 D1 U1	1.00 1.00 1.50-1.95		10 blo	ws: 75% recovery		
									D2	2.00				2.00	
									D3	3.00				3.00	
									D4	4.00					
Structureless CHALK composed of gravelly slightly sandy SILT. Clasts are very weak to weak low and medium density, white.					$\frac{x}{x} - \frac{x}{x} - \frac{x}$	5.00	-2.04	U2	5.00-5.45						
to weak low and medium density, white.						<u> </u>	- - - - - - - - - - - - - - - - - - -	-3.54	D5	6.00					
Structurel GRAVEL weak low Occasion	less CH/ and COI and me al orang	ALK compo BBLES. Cla dium dens ge brown st	osed of silt asts are ve ity, white. aining.	y ry weak t	to				B2	7.00					
									D6	8.00					
						b b			D7	9.00					
Continu	ied ne	xt sheet				<u>, P. P. C. P. P</u>	1	1	<u>ا</u>	ı Nater Level	l Observat	ions			
Hole	Diameter	Details	Ch	iselling D	etails	D-t-		Water		Standing	Stan	ding	Casing	Depth	
Diameter (mm) 200 150	Uepth (m) 4.20 14.00	Casing Depth (m) 4.20 12.00	From (m)	10 (m)	Time (hhmm)	22/01/14 22/01/14		Strike (r 4.10 5.70	n) T	ime (mins) 20 20	Leve 0.00 3.80	l (m) D D	Depth (m) 3.50 5.70	Sealed (4.20	m)
Client: Capita Engineer: Capita Contractor: Harrison Group Environmental Ltd Dates: 22/01/2014 Plant: Dando 2000 Cable Percussive Rig Drilled By: D. Bowman Logged By: P. Price Checked By: J. Keay						Remarks: 1. Inspection 2. Groundwa 3. Environme 4. Dual Instal 13.50mbg 3.00mbgl and top ha 5. Backfill de 3.00mbgl, and concre	i pit excav tter was en intal seal llation det l to 10.50 to GL. Slo to CL. Slo t cover. tails: Grav gravel fill ete from C	ated from G ncountered placed betw ails: 50mm mbgl, plain tted from 3. rel filter pack rer packs fro .20mbgl to	L to 1.200 at 4.10mb diameter from 10.5 00mbgl to xs from 1. om 3.00m GL.	nbgl. gl and 5.70ml 4,20mbgl to 3 HDPE standpi 0mbgl to GL. 0 2.00mbgl, pla 4.00mbgl to 10 bgl to 2.00mbg	bgl. .20mbg. pe installed f 50mm diam ain from 2.00 0.50mbgl, be	from 13.50 eter HDPE Ombgl to v entonite pe pellets fro	Dmbgl to GL. Slotted E standpipe installed with gas tap/bung, er ellets from10.50mbgl om 2.00mbgl to 0.200	from from nd cap to mbgl	
FM-Hn-R-308	In-R-3080 Print Date: 04/04/2014 Harrison Group Environmental Ltd, Unit A11, Poplar Business Park, 10 Prestons Road, London E14 9RL									nmental Ltd, Ur	nit A11, Popla	ar Business	s Park, 10 Prestons R	14 9RL	

harrisongroup	Percussion Borehole Record BH10								
	Project: H	ydrogeo	ological	Grour	nd Investig	gation, N	ew Mon	ks Farm, West	Sussex
Project ID : GI 18017	Coordinat	es: 519	338.1E				Ground Level: 2.96mAOD		
		105	74.9N				Sheet 2 of 2		
Description	Legend	Depth (m)	O.D. Level	Samı Type	ples/ Test	Casing (Water) Depth	F Te	Remarks and est Results	Installations
Structureless CHALK composed of silty GRAVEL and COBBLES. Clasts are very weak to weak low and medium density, white. Occasional orange brown staining.				U3 D8 D9 D10 D11	10.00-10.45 10.00 11.00 12.00 13.00		Nc	o Recovery	
Borehole Complete at 14.00 m		14.00	-11.04	D12	14.00				
Hole Diameter Details Chiselling Details				'	Water Level	Observat	ions		
Diameter Depth Casing From To Time (mm) (m) Depth (m) (m) (m) (hhmm)	Date		vVater Strike (r	n) T	Standing Time (mins)	Stan Leve	aing I (m)	Casing Depth (m)	Depth Sealed (m)
200 4.20 4.20 1.20 1.00 <th1< td=""><td>22/01/14 22/01/14</td><td></td><td>4.10 5.70</td><td></td><td>20 20</td><td>0.00 3.80</td><td>2</td><td>3.50 5.70</td><td>4.20</td></th1<>	22/01/14 22/01/14		4.10 5.70		20 20	0.00 3.80	2	3.50 5.70	4.20
Client: Capita Engineer: Capita Contractor: Harrison Group Environmental Ltd Dates: 22/01/2014 Plant: Dando 2000 Cable Percussive Rig Drilled By: D. Bowman Logged By: P. Price Checked By: J. Keay FM-Hn-R-3080 Print Date: 04/04/2014	Remarks:	Ha	urrison Grou	up Enviroi	nmental Ltd. Li	hit A11. Popla	ar Business F	Park, 10 Prestons Roa	d, London E14 9RI

Project ID: GL18017 Coordinates: 518060.39E 105290.66N Ground Level: 3.72maOD Description Legend Depth (m) O.D. Legend Sample Test (m) Remarks and Test Results Installation (m) Dark brown slightly gravely slightly sandy slight Aut 70PSOL Gravel is subangular to suborunded fine do coase concrete, suphal, fint and chak. 013 327 Image: Sample Test (m) Remarks and Test Results Image: Sample Test (m) Remarks (m) Image: Sample Test (m) Image: Sample Test (m	hai	Wind	Window Sample Record WS4A Sheet 1 of 1								
Project ID: GL18017 Coordinates: 518960.35E 1052200.60N Ground Level: 3.72maOD Description Legend Depth O.D. Level (m) Sample Test Type Remarks and Type Installation Test Results Installation Test Res	4	0P	Project: H	lydrogeol	ogical Gro	ound Investig	gation, N	ew Mo	onks Farm, We	st Sussex	
Description Legend (m) Op (m) Op (m) Sample Test (m) Remarks and Test Results Installation (m) Date brown elightly gravelly slightly sandy subtroanded fram and medium filtune and halk. 0.5 0.57 Image: Complete and medium filtune and chalk. 0.5 0.57 Image: Complete and medium filtune and chalk. 0.5 0.57 Image: Complete and medium filtune and chalk. 0.5 0.57 Image: Complete and medium filtune and chalk. 0.5 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.5 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.5 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.5 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.5 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.5 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.5 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk. 0.57 Image: Complete and to the to coarse concrete, asphalt, fiint and chalk.	Project ID: GL18017		Coordinat	tes: 5189 1052	960.35E 290.66N			Grou	nd Level: 3.7	2maOD	
Description Level (m) Type (m) Depth (m) Test Results Dark brown slightly gravely slightly sandy slight Qarvely Coll. Grave is subangular to subconded fine and medium slightly gravely CLAV Gravel is ubangular to subconded fine to coarse concrete, asphalt, fiint and chalk. 01s 3.37 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. 01s 3.27 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. 01s 3.27 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. 01s 3.27 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. 150 2.22 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. 150 2.22 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. 150 2.22 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. 150 2.22 Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. Imise and to the subconded fine to coarse concrete, asphalt, fiint and chalk. Imise and to the subconded fine to coarse concrete	Description	.	Logond	Dopth	O.D.	Sample	e Test		Remarks	Installations	
Dark brown slightly gravelly slightly sandy sitly CLAY TOPSOL. Gravel is subangular to subounded fine and medium finar and chaik. Oits 3.57 Just How	Description		Legend	(m)	Level (m)	Type [Depth (m)	т	and est Results	Installations	
NADE CROUND. Soft of tim orangish torwon sightly sanual (CAX, Gravel is subangular to subcounded fine to coarse concrete, asphalt, flint and chaik. 1.50 2.27 1.80 1.80 Window Sample Complete at 1.50 m 1.50 2.27 1.80 1.80 1.80 Window Sample Complete at 1.50 m 1.50 2.27 1.80 1.80 1.80 1.80 1.80 Window Sample Complete at 1.50 m 1.50 2.27 1.80 1.90 1.80 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1	Dark brown slightly gravelly s silty CLAY TOPSOIL. Gravel i subrounded fine and medium	lightly sandy s subangular to n flint and chalk.		0.15	3.57		1 ()				
Window Sample Complete at 1.50 m 1.50 2.22 1.50	MADE GROUND. Soft to firm slightly sandy slightly gravelly Gravel is subangular to subro coarse concrete, asphalt, flin		-								
Drive Records Date Water Standing Time (Mins) Standing Level (m) Casing Depth (m) Depth (m) 87 0.50 1.50 100 <td>Window Sample Compl</td> <td></td> <td></td> <td>2.22</td> <td></td> <td></td> <td></td> <td></td> <td></td>	Window Sample Compl			2.22							
Drive Records Date Water Strike (m) Standing Time (Mins) Standing Level (m) Casing Depth (m) Depth Sealed (m) 87 0.50 1.50 100						Water Level	Observati	ons			
87 0.50 1.50 100 <td>Drive Rec</td> <td>ords To (m) Recovery (</td> <td>m Date</td> <td></td> <td>Water Strike (m)</td> <td>Standing Time (Mins)</td> <td>Stan Level</td> <td>iding (m)</td> <td>Casing Depth (m)</td> <td>Depth Sealed (m)</td>	Drive Rec	ords To (m) Recovery (m Date		Water Strike (m)	Standing Time (Mins)	Stan Level	iding (m)	Casing Depth (m)	Depth Sealed (m)	
	87 0.50	1.50 Hecovery (/0]				Level	(''')			
Client: Capita Engineer: Capita Contractor: Harrison Group Environmental Ltd Date: 19/03/2014 Plant: Hand Held Window Sampler Rig Drilled By: JS Logged By: JS Checked By: J. Keay Emit Date: Print Date:04/04/2014	Client: Capita Engineer: Capita Contractor: Harrison Group Date: 19/03/2014 Plant: Hand Held Win Drilled By: JS Logged By: JS Checked By: J. Keay	Environmental Ltd dow Sampler Rig	Remarks: 1. Borehole 2. Inspection 3. Groundw. 4. Installation GL. Slott cover. 5. Backfill de pellets from 2014	e located adj n pit excavat ater was not n details: 50 ed from 1.50 etails: Grave om 0.50mbç	acent to BH4 ted from GL t encountered mm diameter Dmbgl to 0.50 I filter packs f gl to 0.0mbgl.	- utilised same o 0.50mbgl. HDPE standp mbgl, plain fro rom 1.50mbgl	e co-ordinat ipe installed m 0.50mbg to 0.50mbg	d from 1. I to GL w II, bentor	50mbgl to vith end caps and nite	nad London 544 001	



harrisontesting SERVICES

Harrison Testing Services

Units 1 & 2 Alston Road Hellesdon Park Industrial Estate Norwich NR6 5DS Tel:+44 (0) 1603 416333 Fax +44 (0) 1603 416443

Client: Harrison Group Environmental Poplar Business Park 10 Preston Road London E14 9RL

For the attention of: John Keay

Date of Issue: 10/03/2014 Page Number 1 of 7

			Report Form FMR3	000 Rev.C Revision Date 26/11/08
Project	Hydrogeological Ground Investigation, New Monks Farm, West Sussex	Samples	Received	10/02/2014
Report No	GL18017	Instructio	on received	10/02/2014
Your Ref	GL18017	Testing c	ommenced	14/02/2014
	SUMMARY OF RESULTS ATTACHED			
	Test Method and Description		Quantity	UKAS Accredited
BS1377: Part 2: BS1377: Part 2: BS1377: Part 2: BS1377: Part 5: Non Standard -	1990:3.2 Moisture Content 1990:4.4/5.0 Liquid & Plastic Limits - Single Point Method 1990:7.3 Bulk Density - Immersion Method 1990:3.0 One Dimensional Consolidation Shear Strength by Hand Vane		15 5 1 2 5	Yes Yes No Yes No
Remarks:				
Issued by: M V	Villson			
Approved Signatorie	es:			
	s we are notified to the contrary samples will be disposed after a	neriod of o	ne month from th	nis date
	This report should not be reproduced except in full without the write	ten annrov	al of the laborato	no dato nv
Only those res	ults indicated in this report are UKAS accredited and any opinion scope of UKAS accreditation	or interpreta	ations expressed	are outside the
				/ /

TEST REPORT TRANSMITTAL



PROJECT NAME:Hydrogeological Ground Investigation, New Monks Farm, West SussexPROJECT NUMBER:GL18017CLIENT:Capita Property and InfrastructureDATE OF ISSUE:10/03/2014

SUMMARY OF MOISTURE CONTENT, LIQUID LIMIT (ONE POINT CONE PENETROMETER METHOD), PLASTIC LIMIT AND PLASTICITY INDEX TO BS1377 : PART 2 : 1990

BH/TP No	Depth (m)	Sample No.	Moisture Content (%)	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index	NHBC Modified Plasticity	Passing 0.425mm (%)	Soil Class	Sample Description
			<u> </u>	<u> '</u>			index			
BH1	1.00	D1	49	1						Grey brown CLAY
BH1	2.00	D2	77							Grey and brown CLAY
BH1	4.00	U2	71	84	30	55	55	100	CV	Grey and dark grey CLAY
BH1	7.00	D6	56							Grey CLAY
BH2	1.00	В1	29	50	17	33	33	99	СІ	Brown and orange brown slightly gravelly CLAY. Gravel is of chalk
BH3	1.00	B1	23							Brown CLAY
внз	2.00	20	17							Light brown and cream silty CLAY with pockets of
БПО	2.00	02								structureless chalk
ВНЗ	3.00	D3	21							Light grey brown and grey slightly gravelly silty CLAY. Gravel is of flint
				1						

BS1377 : Part 2 : Clause 3.2 : 1990 Determination of Moisture Content

BS1377 : Part 2 : Clause 4.4 : 1990 Determination of Liquid Limit (Single Point Cone Penetrometer Method)

BS1377 : Part 2 : Clause 5 : 1990 Determination of Plastic Limit and Plasticity Index

NHBC Standards Chapter 4.2 : Determination of the modified plasticity index

REMARKS (Including any abnormalities or departures from procedure)

Determination of modified plasticity index is not covered by UKAS accreditation



Page 2 of 7

PROJECT NAME:	Hydrogeological Ground Investigation, New Monks Farm, West Sussex
PROJECT NUMBER:	GL18017
CLIENT:	Capita Property and Infrastructure
DATE OF ISSUE:	10/03/2014

DETERMINATION OF BULK & DRY DENSITY (IMMERSION METHOD) TO BS1377 : PART 2 : 1990 : CLAUSE 7.3

BH/TP No.	Sample	Sample No.	Moisture	Bulk Density	Dry Density	Sample Description
	Depth (m)		Content (%)	(Mg/m ³)	(Mg/m ³)	
PHE	0.00	115	10	0.02	1 90	Wook to moderately wook high density white CHALK
БПО	9.00	05	10	2.23	1.09	weak to moderately weak high density white CHALK

REMARKS (Including any abnormalities or departures from procedure)

Insufficient intact sample to test in full accordance with BS1377



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PROJECT NAME:	Hydrogeological Ground Investigation, New Monks Farm, West Sussex	BH/TP No.:	BH6
PROJECT NUMBER:	GL18017	Depth (m):	1.50
CLIENT:	Capita Property and Infrastructure	Sample No.:	U1
DATE OF ISSUE:	10/03/2014		

DETERMINATION OF ONE DIMENSIONAL CONSOLIDATION PROPERTIES TO BS1377 : PART 5 : 1990 : CLAUSE 3

Description: Brown slightly gravelly CLAY. Gravel is of fine chalk

 Preparation:
 Undisturbed

 Orientation:
 Vertical

 Depth of sample within original sample (m):
 1.60

Initial Conditions:		Final Conditions		
Moisture Content	30 %	Moisture Content	27 %	
Voids Ratio	0.824	Voids Ratio	0.6974	
Diameter	74.91 mm			
Height	19.99 mm	Degree of Saturation	100 %	
Bulk Density	1.94 Mg/m ³	Particle Density	2.72 Mg/m ³	(Assumed)
Dry Density	1.49 Mg/m ³	Laboratory Temperature	18 °C	

Pressure Range kPa	Time Fitting Method	Mv (m²/MN)	Voids Ratio	Cv M²/year
30	t90	1.074	0.7651	0.902
60	t90	0.586	0.7340	0.565
120	t90	0.386	0.6939	1.249
60	t90	0.034	0.6974	~



REMARKS:

Harrison Geotechnical Engineering

Units 1 & 2 Alston Road Norwich NR6 5DS Tel: +44 (0)1603 416333 Fax: +44 (0)1603 416443 email: laboratory@harrisongroupuk.com


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PROJECT NAME:	Hydrogeological Ground Investigation, New Monks Farm, West Sussex	BH/TP No.:	BH1
PROJECT NUMBER:	GL18017	Depth (m):	4.00
CLIENT:	Capita Property and Infrastructure	Sample No.:	U2
DATE OF ISSUE:	10/03/2014		

DETERMINATION OF ONE DIMENSIONAL CONSOLIDATION PROPERTIES TO BS1377 : PART 5 : 1990 : CLAUSE 3

Description: Grey and dark grey CLAY

 Preparation:
 Undisturbed

 Orientation:
 Vertical

 Depth of sample within original sample (m):
 4.20

Initial Conditions:		Final Conditions		
Moisture Content	69 %	Moisture Content	46 %	
Voids Ratio	1.829	Voids Ratio	1.1372	
Diameter	74.79 mm			
Height	20.13 mm	Degree of Saturation	100 %	
Bulk Density	1.58 Mg/m ³	Particle Density	2.65 Mg/m ³	(Assumed)
Dry Density	0.94 Mg/m ³	Laboratory Temperature	18 °C	

Pressure Range kPa	Time Fitting Method	Mv (m²/MN)	Voids Ratio	Cv M²/year
50	t90	2.772	1.4368	0.208
100	t90	1.403	1.2659	0.173
200	t90	0.737	1.0990	0.151
75	t90	0.146	1.1372	~



REMARKS:

Harrison Geotechnical Engineering

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PROJECT NAME:Hydrogeological Ground Investigation, New Monks Farm, West SussexPROJECT NUMBER:GL18017CLIENT:Capita Property InfrastructureDATE OF ISSUE:10/03/2014

DETERMINATION OF SHEAR STRENGTH BY HAND VANE

BH/TP No.	Sample	Sample No.	Sample Description	Shear Strength (kPa)
	Depth (m)			
BH1	4 00	112	Very low strength grey and dark grey CLAY	6
DITI	4.00	02		0
вне	1 50	114	I ow strength brown slightly gravelly CLAY. Gravel is of fine flint	28
BHO	1.50	01		20
BH2	4.45	110	Vary low strangth brown slightly gravely slightly sandy silty CLAX. Gravel is of shalk	12
ВП/	4.45	02	very low strength brown slightly gravely slightly sandy slight CLAT. Graver is of chaik	12
BH10	1 50	114	Ligh strength arey brown, groonich brown and gronge brown slightly grouply CLAV	96
БПІО	1.50	01	Gravel is of chalk	00
BH10	F 00	110	TOP OF TUPE: Low strength light brown and day, grow slightly growelly CLAV. Crowel is	25
БПІО	5.00	02	of chalk.	25
			BASE OF TUBE: White structureless CHALK composed of slightly sandy silty GRAVEL.	
			Gravel is of very weak low density chalk. Hand vane determination carried out in top of	
			sample	

REMARKS (Including any abnormalities or departures from procedure)

Harrison Geotechnical Engineering Units 1 & 2 Norwich Norfolk NR6 5DS Tel: +44 (0)1603 416333 Fax: +44 (0)1603 416443 email: laboratory@harrisongroupuk.com



ha ha	rrisonaroup	U100 Photograph Sheet					
	indengroup	Job No: GL18017					
Client : Capita Property ar	nd Infrastructure	Project: Hydrogeological Ground Investigation, New Monks Farm, West Sussex					
Borehole No : BH6	Sample No.: U5	Sample Depth (m): 9.00	Date Logged: 14/2/14				
Sample diameter (mm): 10	3.11	Sample length (mm): 385	Sample mass (g): 6284.2				

Description:

Structureless CHALK composed of white and light grey gravelly sandy SILT. Gravel is of fine to coarse angular to subangular very weak to moderately weak low to high density white chalk. Grade Dm.

Coarse elongated flint at 9.08m

Photograph:



Sample disturbance:		
Details of sub samples: (type, depth etc) None	Remarks:	
	Logged by: MW	Checked By: MW



New Monks Farm CS/05631 April 2014 Commercial in Confidence Appendix B

Appendix B

Groundwater Levels (Compensated Logger Data)

	BH01D		BH01S		BH02D		BH02S		BH04D		BH04S		BH06D		BH06S	I	BH07D	I	BH07S	В
Date	Water head [cm]	temperature [oC]	Water head [cm]	temperature	Water head [cm]	temperature	Water head [cm]	temperature	Water head [cm]	temperature	Water head [cm] to	emperature	Water head [cm]	temperature	Water head [cm]	temperature	Water head [cm]	temperature	Water head [cm] ter	nperature V
	249.779	11.517	208.746	9.927	290.338	10.563	270.675	8.82	292.983	10.69	294.825	8.613	351.692	11.2/3	361.783	8.553	248.471	11.837	381.008	9.38
	249.779	11.523	208.238	9.953	290.104	10.557	270.967	8.793	292.692	10.743	294.317	8.653	351.575	11.253	361.808	8.573	8 250.571	. 11.837	382.233	9.407
07/02/2014	249.663	11.537	207.729	9.993	289.813	10.607	270.192	8.767	292.342	10.75	294.208	8.687	351.342	11.23	361.433	8.607	250.804	11.823	383.325	9.4
	249.838	11.543	208.021	10.293	289.463	10.62	270.083	8.767	292.692	10.77	294.633	8.687	351.283	11.243	361.725	8.573	249.238	11.823	384.283	9.393
	249.904	11.543	208.446	10.347	289.413	10.647	270.108	8.753	293.225	10.77	294.525	8.693	351.992	11.243	362.283	8.627	248.304	11.853	387.242	9.353
	249.554	11.55	208.196	10.293	289.413	10.613	270.392	8.793	292.875	10.777	293.875	8.707	352.225	11.253	362.567	8.6	247.546	11.837	388.458	9.347
	251.979	11.55	207.954	10.347	289.621	10.627	270.417	8.78	293.667	10.777	295.367	8.693	354.008	11.253	364.058	8.56	248.104	11.837	390.75	9.307
	249.679	11.543	207.921	10.107	290.704	10.607	270.383	8.807	296.733	10.783	298.8	8.693	359	11.223	373.358	8.533	249.946	11.837	393.383	9.347
	249.854	11.543	208.088	10.133	291.754	10.607	269.75	8.82	297.608	10.783	299.767	8.687	360.05	11.253	378.458	8.52	2 251.054	11.837	394.083	9.34
	250.354	11.543	208.321	10.36	292.3/1	10.62	270.25	8.82	297.933	10.783	300.667	8.687	360.55	11.253	380.692	8.48	3 252.896	11.823	394.85	9.34
	249.679	11.55	207.554	10.273	292.804	10.62	269.883	8.78	296.85	10.777	299.233	8.647	359.35	11.233	378.725	8.54	254.788	11.837	394.083	9.313
	250.179	11.557	208.096	10.313	293.479	10.62	270.292	8.793	297.35	10.777	299.642	8.653	359.5	11.253	378.2	8.533	255.288	11.837	394.758	9.333
	250.179	11.55	207.788	10.267	294.121	10.627	269.717	8.78	296.825	10.79	299.067	8.66	358.8	11.217	377.492	8.553	254.471	. 11.837	394.583	9.32
00/02/2014	250.179	11.557	207.321	10.313	294.004	10.647	269.583	8.76	296.125	10.783	298.933	8.66	358.158	11.243	374.825	8.56	5 251.788	11.837	394.583	9.333
08/02/2014	250.179	11.557	207.696	10.133	294.938	10.613	270.025	8.767	295.833	10.79	297.775	8.687	357.808	11.243	373.8	8.567	250.738	11.837	394.758	9.32
	250.238	11.563	208.038	10.133	294.821	10.647	270.1	8.78	295.717	10.79	297.05	8.68	357.517	11.243	373.608	8.593	250.154	11.837	395.1	9.3
	250.063	11.545	208.338	10.233	294.763	10.013	269.733	8.767	294.958	10.783	296.683	8.68	356.817	11.253	371.775	8.607	249.571	. 11.837	396.2	9.307
	250.063	11.55	207.754	10.16	294.471	10.627	269.95	8.787	294.492	10.79	295.967	8.707	356.35	11.253	370.792	8.607	249.979	11.823	396.283	9.287
	250.238	11.563	208.104	10.393	294.529	10.6	270.3	8.78	294.492	10.783	296.183	8.673	356.35	11.243	370.608	8.607	251.321	. 11.837	397.033	9.307
	250.003	11.55	208.288	10.113	294.121	10.627	269.817	8.793	293.907	10.783	295.5	8.693	355.125	11.20	369.192	8.587	253.304	11.823	396.683	9.333
	250.238	11.557	208.113	10.147	293.013	10.633	269.908	8.787	293.5	10.783	294.858	8.693	354.833	11.267	368.483	8.6	i 253.888	11.837	396.775	9.273
	250.413	11.563	208.038	10.093	292.954	10.6	270.233	8.787	293.267	10.783	293.85	8.687	355.125	11.273	368.542	8.62	253.888	11.837	395.367	9.333
	250.413	11.557	207.904	10.287	292.429	10.613	270.1	8.793	293.442	10.783	294.517	8.68	355.183	11.237	368.992	8.62	253.538	11.823	395.283	9.36
	250.354	11.557	207.788	10.387	292.021	10.627	269.983	8.76	292.742	10.777	294.267	8.693	353.9	11.253	368.692	8.633	3 251.029	11.823	394.983	9.32
	251.054	11.563	207.479	10.38	291.846	10.653	270.208	8.747	292.683	10.79	293.958	8.693	353.433	11.267	367.45	8.673	250.446	11.823	394.675	9.333
	250.729	11.577	207.688	10.287	291.404 291.088	10.64	2/0.017 269.633	8.753	292.708	10.783	293.233	8.687	353.05	11.26	365.808	8.653	249.479	11.823	394.617	9.367
	250.729	11.577	207.463	10.133	290.588	10.62	269.658	8.76	292.183	10.79	293.008	8.673	352.7	11.273	364.9	8.62	249.246	11.823	394.258	9.353
	250.729	11.57	207.646	10.2	290.238	10.627	269.842	8.747	291.833	10.77	292.392	8.707	352.233	11.267	364.95	8.693	3 249.071	11.823	394.175	9.353
	250.846	11.583	207.429	10.16	290.238	10.613	269.625	8.76	291.542	10.777	292.308	8.693	351.708	11.273	364.067	8.64	250.179	11.823	393.692	9.34
	250.988	11.59	207.538	10.033	289.213	10.555	269.333	8.767	290.575	10.783	291.083	8.713	350.275	11.20	362.175	8.553	251.313	11.823	391.933	9.347
	251.163	11.59	207.113	10.273	288.804	10.653	269.575	8.78	290.225	10.777	291.058	8.713	349.75	11.26	360.817	8.507	251.546	11.823	390.842	9.393
	250.813	11.597	207.263	10.147	288.396	10.583	269.592	8.787	289.817	10.777	290.808	8.707	349.167	11.26	359.9	8.553	250.904	11.823	389.925	9.353
09/02/2014	250.754	11.59	207.288	10.28	286.996	10.583	269.35	8.787	289.175	10.77	289.9	8.733	348.117	11.28	358.058	8.507	249.938	11.823	389.55	9.367
	250.779	11.597	207.196	10.26	285.971	10.64	269.258	8.793	288.033	10.777	288.875	8.747	347.267	11.273	356.767	8.553	3 247.488	11.823	388.525	9.4
	250.721	11.59	207.596	10.38	285.329	10.6	268.992	8.787	288.325	10.783	288.742	8.78	346.917	11.273	356.633	8.54	246.671	11.823	388.525	9.4
	250.896	11.597	207.429	10.313	284.979	10.62	269.225	8.807	288.207	10.77	288.792	8.713	346.625	11.267	355.533	8.54	245.738	11.823	387.958	9.393
	251.446	11.597	207.638	10.347	284.129	10.563	269.3	8.8	288	10.777	287.983	8.8	346.417	11.26	354.942	8.553	3 246.054	11.823	387.633	9.393
	251.271	11.603	207.871	10.393	283.429	10.62	269.533	8.787	287.592	10.777	287.683	8.78	345.775	11.267	355.175	8.54	246.404	11.823	386.8	9.407
	251.096	11.597	207.696	10.107	283.254	10.62	269.625	8.793	287.883	10.77	287.908	8.8	345.892	11.253	354.867	8.553	247.046	11.823	386.983	9.407
	251.388	11.597	207.654	10.367	281.971	10.627	269.05	8.82	287.533	10.783	287.333	8.78	345.192	11.273	354.425	8.567	249.146	11.823	386.983	9.393
	251.446	11.603	207.963	10.113	281.388	10.6	269.358	8.78	287.592	10.777	287.375	8.793	345.542	11.273	354.333	8.56	249.846	11.837	387.025	9.44
-	251.446	11.603	207.646	10.313	280.921	10.62	269.708	8./8/	287.65	10.777	287.458	8.8	345.367 346.767	11.26	353.617	8.553	249.904	11.823	387.242	9.393
	251.621	11.59	207.013	10.26	280.338	10.583	269.208	8.78	289.167	10.777	289.225	8.8	347.933	11.253	358.317	8.507	249.146	11.823	387.675	9.4
	251.421	11.597	207.379	10.113	280.546	10.607	269.308	8.787	289.492	10.777	289.725	8.793	348.142	11.243	359.617	8.533	248.363	11.823	388.308	9.42
	251.096	11.603	207.179	9.913	280.746	10.607	269.108	8.78	289.808	10.783	289.392	8.793	347.817	11.243	359.283	8.607	247.338	11.823	388.242	9.373
	251.654	11.597	207.188	10.16	281.888	10.633	269.25	8.767	290.192	10.777	290.867	8.693	348.667	11.253	359.692	8.507	247.371	. 11.823	389.583	9.373
	251.446	11.603	206.821	10.16	281.854	10.593	268.883	8.787	289.867	10.777	290.633	8.773	348.633	11.253	360.658	8.573	247.513	11.823	388.95	9.36
	251.//1	11.597	207.154	10.193	282.296	10.607	269.083	8.78	290.133	10.///	290.833	8.//3	348.31/	11.253	361.258	8.62	248.538	11.823	388.35	9.373
	251.646	11.603	206.779	10.107	282.871	10.607	268.708	8.787	290.125	10.777	290.725	8.773	348.133	11.253	360.75	8.567	251.038	11.837	387.575	9.42
	251.388	11.603	206.721	10.127	283.079	10.6	268.917	8.787	290.333	10.783	290.8	8.767	347.933	11.267	361.225	8.607	252.004	11.837	387.25	9.4
10/02/2014	251.563	11.603	206.904	10.293	283.838	10.6	269.367 268.792	8.8 8.9	290.508	10.783	290.983	8.8 8 7/17	347.933	11.253	360.475	8.473	252.238	11.837	387.167	9.42
	251.563	11.603	206.954	9.893	283.954	10.62	268.75	8.793	290.275	10.77	291.167	8.747	347.875	11.20	360.525	8.66	5 <u>250.</u> 429	11.853	386.55	9.4
	251.854	11.61	207.038	9.793	284.479	10.607	269.233	8.8	290.217	10.777	291.783	8.707	347.758	11.267	360.342	8.52	249.321	11.837	386.9	9.407
	251.329	11.61	206.471	10.26	284.538	10.593	268.667	8.813 8 813	289.633	10.763	290.95	8.627	347.35	11.26	358.842	8.607	248.038	11.853	386.333	9.407
	251.846	11.61	206.738	9.88	284.121	10.607	268.533	8.8	289.042	10.777	289.617	8.747	346.175	11.20	357.508	8.56	245.813	11.853	385	9.4
	251.996	11.603	206.771	9.813	284.154	10.6	268.967	8.813	288.667	10.777	289.517	8.747	345.975	11.237	356.608	8.5	245.788	11.837	383.967	9.427
	252.021	11.603	206.954	10.053	283.713	10.583	268.883	8.8 גפא	288.05	10.77	288.9	8.593	345.3	11.237	355.592	8.54	245.696	11.853	382.95	9.427
	252.254	11.603	206.954	10.313	282.663	10.607	268.75	8.82	287.408	10.77	288.233	8.607	344.133	11.243	353.858	8.6	240.330	11.853	381.217	9.427
	252.129	11.603	206.613	10.267	282.479	10.613	269.075	8.8	287.575	10.777	287.758	8.62	344.008	11.253	353.383	8.533	248.196	11.853	380.475	9.44
	252.129	11.603	206.846	10.347	281.488	10.607	269.042	8.793	287.05	10.777	287.458	8.613	343.658	11.26	352.683	8.527	248.779	11.853	380.042	9.453
	252.246	11.603	206.329	10.26	280.729	10.57	268.792	8.8	286.817	10.77	286.808	8.64	343.25	11.243	352.032	8.54	246.003	11.867	379.658	9.467
	252.621	11.603	206.396	10.26	279.996	10.607	268.992	8.767	286.9	10.777	287.142	8.62	343.158	11.243	351.7	8.527	246.646	11.853	379.725	9.467
	252.804	11.603	206.596	10.227	279.713	10.607	268.658	8.787	287.2	10.777	287.208	8.64	343.458	11.26	351.9	8.493	245.838	11.867	380.858	9.453
	252.254	11.61	206.329 205.921	10.093	279.513 279.046	10.6	268.917	8.767	287.292	10.77	287.333	8.62	343.958 343.492	11.26	351.9	8.527	245.346	11.853	381.525	9.467
	251.788	11.603	206.046	10.027	278.346	10.607	267.842	8.787	286.825	10.77	287.058	8.613	342.792	11.273	351.483	8.513	244.529	11.853	382.575	9.44
	251.996	11.603	206.129	9.927	278.438	10.593	268.325	8.767	287.092	10.777	287.008	8.627	343.408	11.237	351.967	8.593	245.204	11.853	383.992	9.453
	252.346	11.603	206.471	9.787	278.321	10.613	268.667 268.325	8.767	287.092	10.77	287.35	8.613	343.525 343.817	11.26	351./75	8.48	246./21	11.853	384.867	9.46 9.427
	251.704	11.603	206.021	10.227	277.679	10.607	268.083	8.793	287.5	10.763	287.967	8.607	344.167	11.237	352.525	8.553	249.871	11.853	387.217	9.453
11/02/2014	252.204	11.61	205.938	10.007	278.529	10.563	268.267	8.793	288.35	10.763	288.817	8.607	345.367	11.26	354.842	8.62	2 251.771	11.853	387.8	9.407
	252.113	11.603	206.188	10.193	278.729	10.6	268.117	8.787	290.183	10.763	289.867	8.593	347.725	11.26	359.492	8.48	252.846	11.853	387.517	9.433
	252.171	11.61	206.038	10.007	279.838	10.583	267.942	8.78	290.183	10.77	290.492	8.573	347.142	11.253	362.383	8.573	231.738	11.867	385.208	9.407
	252.288	11.61	206.113	10.193	280.304	10.6	268.308	8.76	289.775	10.763	290.858	8.58	346.792	11.253	362.35	8.527	248.763	11.853	384.775	9.407
	252.313	11.61	205.663	10.187	280.504	10.593	267.858	8.787	289.858	10.77	290.675	8.573	346.408	11.253	360.833	8.553	247.271	11.837	383.792	9.473
	252.888	11.61	205.884	9.967	281.288	10.007	267.983	8.78	269.417	10.763	290.4	8.56	346.083	11.243	359.375	8.527	245.546	11.837	382.467	9.433
	252.779	11.603	206.496	9.733	281.263	10.613	268.425	8.78	288.925	10.763	289.908	8.587	345.533	11.243	357.667	8.573	245.638	11.853	382.358	9.44

	BH10D		BH10S	BH10S Adjusted	
iture	Water head [cm]	temperature	Water head [cm]	Water Head (cm)	temperature
9.38	220.33	11.507	490.75	290.75	
9.407	220.11	11.533	491.3	291.3	
9.407 q л	220.02	11.52	491.975 // AQ1 0	291.975	
9.393	220.48	11.52	491.425	291.425	
9.367	221.28	11.52	490.3	290.3	
9.353	220.15	11.533	491.05	291.05	
9.347	221.13	11.533	490.8	290.8	
9.307	222.03	11.533	492.225	292.225	
9.347	222.83	11.55	492.8	292.8	
9.34	222.96	11.55	493.225	293.225	
9.34	222.69	11.55	492.725	292.725	
9.32	223.31	11.55	493.575	293.575	
9.313	223.73	11.55	493.225	293.225	
9.333	222.87	11.55	493.725	293.9	
9.313	222.12	11.563	493.725	293.725	
9.333	222.88	11.563	493.725	293.725	
9.32	223.63	11.577	493.9	293.9	
9.3	222.98	11.577	494.775	294.775	
9.287	224.27	11.577	493.3	293.3	
9.287	224.03	11.505	493.825	293.825	
9.307	225.14	11.577	494.175	294.175	
9.287	223.45	11.563	493.825	293.825	
9.333	224.22	11.563	493.825	293.825	
9.2/3	224.81	11.563	493.65 100 775	293.65	
9.36	224.51	11.577	492.775	292.775	-
9.32	224.93	11.563	493.425	293.425	
9.32	224.99	11.577	493.725	293.725	
9.333	225.58	11.577	493.55	293.55	
9.367 0.21	225.26	11.577	493.225	293.225	<u> </u>
9.353 9.353	225.41	11.577	493.375	293.375	<u> </u>
9.353	225.85	11.577	493.05	293.05	
9.34	225.5	11.577	494.7	294.7	
9.347	225.81	11.577	493.475	293.475	
9.347	225.38	11.577	494.275	294.275	
9.393	226.26	11.59	493.05	293.05	
9.373	226.31	11.577	492.8	292.8	
9.367	225.93	11.577	492.425	292.425	
9.4	225.68	11.577	491.4	291.4	
9.4	226.44	11.577	491.4	291.4	
9.393	220.80	11.577	492.03	292.03	
9.393	226.95	11.577	493.375	293.375	
9.407	227.78	11.577	492.675	292.675	
9.407	227.61	11.577	492.5	292.5	
9.42	227.43	11.577	492.325	292.325	
9.393	228.2	11.577	492.325	292.325	
9.393	227.96	11.577	492.85	292.85	
9.373	228.31	11.577	493.2	293.2	
9.4	227.89	11.577	493.55	293.55	
9.42	228.39	11.59	493.05	293.05	
9.3/3	227.83	11.577	492.25	292.25	
9.373	229.27	11.577	491.925	291.925	-
9.36	228.77	11.577	491.425	291.425	
9.373	228.57	11.577	494.225	294.225	
9.4	228.83	11.59	493.725	293.725	L
9.42	229.69	11.5/7	493.05 494 325	293.05	
9.42	229.19	11.577	493.975	293.975	
9.4	228.44	11.577	493.8	293.8	
9.4	229.61	11.577	493.625	293.625	
9.407	229.19	11.577	493.975	293.975	<u> </u>
9.407	229.26	11.577	493.275	293.275	
9.4	229.16	11.577	494.875	294.875	
9.427	229.79	11.577	493.975	293.975	
9.427	231.31	11.577	493.425	293.425	
9.433	229.91	11.577	493.025	293.025	
9.44	230.62	11.577	493.025	293.025	<u> </u>
9.453	230.98	11.577	492.45	292.45	
9.467	230.45	11.563	491.925	291.925	
9.467	230.69	11.577	491.4	291.4	
9.467	230.89	11.577	492.6	292.6	
9.453	231.13	11.5//	492.6 192.9	292.6	
9.44	230.79	11.577	492.325	292.325	
9.44	231.08	11.577	492.85	292.85	
9.453	231.28	11.577	492.4	292.4	
9.46	232.16	11.577	493.275	293.275	
9.427	231.78	11.577	494.2	294.2	
9.407	232.24	11.577	494.425	294.425	
9.433	231.41	11.563	495.125	295.125	
9.433	231.96	11.577	494.375	294.375	
9.407	232.27	11.563	494.15	294.15	
9.407	231.57	11.577	493.45	293.45	
9,453	232.25	11.563	493.6	293.6	
9.44	232.63	11.577	494.875	294.875	
9.44	232.45	11.563	494.5	294.5	

	252.779	11.597	206.196	9.82	2 281.204	10.593	268.258	8.78	288.692	10.757	289.875	8.56	345.358	11.26	357.233	8.453	245.929	11.853	382.058	9.453
	252.479	11.597	205.554	9.85	7 280.554 3 280.788	10.6 10.577	267.75	8.78	288.217 287.867	10.763	288.567	8.58 8.587	344.475	11.243	356.325	8.48	246.213	11.853	381.15	9.44
	252.771	11.603	206.288	10.00	6 280.846	10.593	268.217	8.78	288.1	10.757	288.767	8.58	344.3	11.243	354.925	8.433	248.546	11.853	379.883	9.46
	252.913	11.61	205.879	10.22	7 280.054	10.6	267.942	8.78	287.6	10.763	288.625	8.573	343.8	11.237	353.85	8.433	249.154	11.853	379.875	9.487
	252.913	11.603	205.929	10.03	4 279.704	10.593	208.058	8.767	287.892	10.77	288.408	8.58	343.8	11.243	352.833	8.407	249.213	11.853	379.92	9.473
	252.913	11.603	205.621	10.15	3 278.713	10.627	267.817	8.767	287.075	10.763	287.433	8.58	343.45	11.26	352.258	8.447	246.763	11.853	379.75	9.473
	252.913	11.603	205.796	9.91	3 278.771	10.6	268.125	8.76	287.25	10.763	287.208	8.58	343.275	11.237	352.033	8.42	245.479	11.853	379.525	9.493
	252.271	11.603	205.088 205.613	10.21	278.188 6 278.304	10.57	267.817	8.767	286.433 288.067	10.763	286.767	8.587	342.808	11.237	351.725	8.473	244.254 244.371	11.853	379.483	9.493
	252.921	11.597	206.213	10.26	7 280.704	10.55	268.008	8.76	298.575	10.77	297.892	8.587	357.167	11.26	365.917	8.473	247.646	11.853	381.408	9.473
	252.771	11.603	205.613	10.03	3 282.013	10.62	267.942	8.787	301.633	10.763	304.092	8.56	360.458	11.253	377.583	8.54	250.121	11.853	380.942	9.46
	253.154	11.603	205.421	10.11	283.446	10.593	268.058	8.733	302.833	10.77	305.675	8.487	362.533	11.237	382.058	8.48	252.838	11.853	383.858	9.453 9.46
12/02/2014	251.988	11.603	205.521	10.00	7 285.254	10.577	267.583	8.753	301.667	10.75	304.8	8.613	362.592	11.243	381.225	8.367	256.163	11.853	385.25	9.427
12,02,201	253.221	11.61	206.129	10.053	3 286.896	10.57	268.992	8.753	302.608	10.757	305.542	8.52	364.35	11.26	381.3	8.353	258.446	11.853	387.858	9.407
	253.079	11.61	205.796	10.11	3 287.804	10.577	268.792	8.753	302.642	10.763	305.608	8.553	364.267	11.23	380.7	8.387	259.354	11.853	390.058	9.393
	253.463	11.61	206.746	10.14	4 292.971	10.6	269.075	8.707	307.575	10.75	311.092	8.547	371.767	11.237	386.717	8.347	259.213	11.853	392.475	9.373
	253.113	11.61	206.204	10.02	2 295.771	10.6	268.667	8.72	310.725	10.763	315.35	8.527	375.85	11.237	389.775	8.32	258.863	11.853	392.867	9.393
	253.288	11.61	206.621	10.17	3 290.290	10.595	269.35	8.733	309.967	10.77	313.633	8.607	375.675	11.237	390.342	8.313	256.179	11.853	392.61	9.373
	253.313	11.603	206.613	10.14	4 297.663	10.577	268.808	8.693	308.825	10.763	312.292	8.533	375.35	11.23	389.383	8.34	255.913	11.853	391.675	9.407
	253.313	11.603	206.888	10.26	7 297.604	10.577	268.683	8.673	308.125	10.763	311.233	8.56	374.825	11.237	388.858	8.287	255.796	11.853	391.417	9.407
	253.138	11.603	206.504	10.11	2 298.304	10.577	268.967	8.633	307.25	10.75	308.983	8.58	373.892	11.237	387.008	8.247	258.071	11.837	391.033	9.393
	252.579	11.597	206.188	10.18	3 298.388	10.563	269.05	8.64	305.933	10.75	307.333	8.627	372.75	11.23	385.758	8.253	259.321	11.837	390.85	9.393
	253.129	11.603	206.313	10.22	7 297.421	10.607	268.908	8.647	305.258	10.763	306.658	8.52	372.542	11.26	385.35	8.26	260.104	11.853	390.708	9.4
	253.779	11.603	207.279	10.22	3 298.654	10.577	269.208	8.607	304.683	10.757	306.158	8.507	372.025	11.23	385.383	8.233	259.529	11.853	391.408	9.42
	254.129	11.603	207.088	10.03	3 299.179	10.57	269.417	8.593	304.625	10.75	305.833	8.52	371.908	11.23	384.658	8.227	258.363	11.837	392.283	9.4
	253.954	11.603	206.896	10.15	299.588 1 299.821	10.577	269.758	8.593	304.158	10.75	305.642	8.527	372.083	11.23	385.133	8.22	256.963	11.837	393.425	9.4
	253.663	11.597	207.150	10.23	3 299.646	10.583	270.017	8.593	303.167	10.757	304.167	8.533	371.092	11.223	383.792	8.22	254.163	11.837	394.083	9.373
	254.163	11.597	207.029	10.11	3 299.679	10.593	269.758	8.58	302.908	10.75	304.042	8.547	370.833	11.253	383.267	8.213	253.554	11.837	394.492	9.367
	254.013	11.603	206.696	9.95	1 299.588 3 299.913	10.583	269.692	8.607	302.467	10.763	303.442	8.547	370.567	11.243	383.067	8.227	253.579	11.837	394.825	9.38
	254.188	11.603	206.871	9.99	3 299.238	10.557	269.733	8.593	302.233	10.757	303.083	8.62	370.1	11.237	382.575	8.22	255.388	11.837	395	9.373
13/02/2014	254.129	11.61	207.013	10.18	7 299.413	10.577	269.875	8.58	301.708	10.757	302.158	8.613	369.342	11.243	382.317	8.16	256.554	11.837	394.342	9.34
	253.604	11.603	206.571	10.23	3 298.829	10.577	269.533	8.58	300.717	10.763	301.15	8.613	368.35	11.237	381.175	8.287	257.313	11.837	393.6	9.347
	253.779	11.603	206.704	10.093	3 297.779	10.57	269.3	8.58	299.783	10.75	299.983	8.647	366.542	11.26	380.142	8.213	257.313	11.837	392.167	9.353
	254.271	11.603	206.879	10.14	7 297.454	10.577	269.208	8.593	299.108	10.75	299.492	8.56	365.75	11.23	378.583	8.233	256.054	11.837	391.542	9.34
	254.038	11.603	206.888	9.72	7 296.263	10.565	269.142	8.58	298.558	10.757	298.492	8.507	364.442	11.237	376.458	8.193	254.240	11.837	389.417	9.393
	254.554	11.603	207.029	10.04	7 295.404	10.557	270.025	8.593	298.05	10.757	297.508	8.58	363.408	11.243	375.533	8.213	251.379	11.837	388.892	9.373
	254.879	11.603	206.929	9.91	3 294.679	10.53	269.525	8.58	297.15	10.743	297.542	8.593	362.917	11.23	374.367	8.2	250.479	11.837	388.258	9.4
	254.821	11.597	200.854	9.88	8 293.513	10.557	269.583	8.6	290.8	10.757	296.8	8.50	362.042	11.243	373.492	8.233	251.238	11.837	387.783	9.393
	254.721	11.603	206.813	10.00	6 292.713	10.577	269.542	8.593	296.35	10.75	296.092	8.58	361.242	11.23	372.25	8.22	252.129	11.837	386.808	9.373
	254.871	11.597	206.879	9 81	6 292.279 3 291.579	10.557	269.742	8.6	296.442	10.75	296.292	8.56	361.042	11.237	371.783	8.173	253.796	11.837	387.142	9.393
	254.846	11.597	206.729	9.64	4 290.971	10.537	269.458	8.593	296.067	10.75	295.608	8.587	359.792	11.223	370.167	8.14	256.571	11.837	386.992	9.42
	255.221	11.603	206.746	9.64	7 290.704	10.557	270.142	8.593	296.442	10.757	295.625	8.573	359.875	11.23	370.05	8.127	257.121	11.837	387.542	9.387
	254.821	11.597	206.554 206.138	9.86	7 290.129 3 289.279	10.53	269.55	8.593	296.217	10.743	295.567	8.587	359.475	11.23/	369.725	8.113	255.963	11.837	387.73	9.387
	254.696	11.603	206.521	10.09	3 288.663	10.563	269.783	8.58	294.983	10.743	294.733	8.58	358.3	11.243	367.825	8.167	252.338	11.837	387.583	9.387
	254.646	11.603	206.329	10.18	7 288.321	10.537	269.592	8.553	294.817	10.75	294.675	8.58	357.958	11.23	367.767	8.16	251.121	11.837	388.058	9.393
	254.821	11.603	206.679	9.9	7 288.263 6 287.679	10.55	269.808	8.58	294.642	10.75	294.358	8.593	357.783	11.237	367.85	8.173	250.654	11.837	388.275	9.373
	255.554	11.597	206.971	10.08	8 288.121	10.563	270.233	8.573	295.958	10.75	296.117	8.573	359.567	11.23	368.808	8.127	252.263	11.837	389.9	9.407
	255.063	11.603	207.088	10.10	6 287.979	10.543	270.217	8.587	296.692	10.737	297.033	8.533	361.058	11.243	371.458	8.127	253.871	11.837	392.283	9.367
14/02/2014	255.354	11.603	207.296	10.14	7 289.904	10.545	270.158	8.54	301.825	10.757	302.842	8.587	368	11.243	380.2	8.287	259.296	11.823	394.758	9.313
	255.038	11.597	207.179	9.96	7 292.388	10.563	270.175	8.553	307.925	10.75	310.325	8.507	374.858	11.23	387.017	8.187	263.063	11.823	397.708	9.333
	254.746 255.479	11.597	206.763	9.91	3 296.004 3 299.363	10.563	270.025	8.513	316.033 320.558	10.75 10.757	319.375 324.642	8.487	382.733	11.23 11.23	392.333	8.2 8.18	266.154	11.837	397.825	9.313
	255.629	11.597	206.529	9.64	4 300.971	10.55	269.792	8.527	320.125	10.75	325.008	8.44	389.858	11.237	395.567	8.153	267.971	11.837	400.525	9.287
	255.629	11.597	207.529	9.6	6 301.729	10.537	270.925	8.527	320.358	10.757	325.208	8.44	390.092	11.237	395.633	8.213	267.329	11.837	401.792	9.307
	255.338	11.597	206.979	9.85	3 303.713	10.563	271.308	8.527	319.192	10.743	323.158	8.453	389.1	11.223	395.483	8.147	205.988 265.054	11.837	401.875	9.287
	255.488	11.597	207.204	10.14	4 305.088	10.557	271.4	8.527	318	10.757	321.683	8.46	389.25	11.243	395.042	8.247	264.621	11.837	403.067	9.24
	255.371	11.597	207.054	9.92	/ 306.254 7 308.170	10.543	271.783	8.527 8.512	317.242	10.737	321.4	8.46 8.452	388.958	11.23	395.025	8.193 g p	265.496	11.823	403.583	9.267
	256.013	11.597	207.288	10.12	7 308.763	10.563	271.883	8.513	315.725	10.757	318.567	8.467	387.033	11.26	393.792	8.227	269.113	11.837	402.883	9.267
	255.338	11.597	207.204	10.16	7 308.846	10.53	271.933	8.507	314	10.743	317.95	8.42	385.833	11.223	393.442	8.267	271.121	11.837	401.333	9.227
	255.338 256.854	11.603	206.771	9.91	3 307.796 3 307.854	10.563 10.537	272.167	8.513	313.65 313.592	10.75 10.75	316.583 316.017	8.487 8.387	385.367 385.425	11.23 11.217	393.142	8.233	272.871	11.837	400.767	9.247
	257.696	11.597	206.863	10.17	3 307.529	10.543	272.525	8.513	312.917	10.75	315.208	8.453	385.333	11.223	392.7	8.28	273.188	11.837	399.925	9.307
	258.863	11.603	207.054	10.17	3 307.879	10.543	273.117	8.513	312.567	10.75	314.2	8.44	384.458	11.223	392.892	8.193	272.079	11.837	399.18	9.307
	260.204	11.603	207.254	9.79	3 307.938	10.55	272.867	8.493	312.625	10.75	314.933	8.3	385.217	11.23	393.758	8.26	269.804	11.837	398.45	9.313
	262.888	11.597	206.788	10.14	4 308.113	10.537	272.983	8.507	311.867	10.737	313.4	8.427	384.167	11.223	392.758	8.247	267.004	11.837	397.183	9.3
	264.254	11.603	207.363	10.22	7 307.904	10.537	273.158	8.487	311.367	10.75	312.775	8.407	383.842	11.23	393.067	8.193	266.621	11.837	396.692	9.287
	268.304	11.603	206.713	10.02	2 307.288	10.557	273.042	8.467	310.925	10.75	311.458	8.453	383.283	11.223	392.55	8.22	267.054	11.837	395.108	9.32 9.34
15/02/2014	270.346	11.61	206.771	10.14	7 306.529	10.557	273.367	8.44	310.692	10.75	311.383	8.42	382.758	11.23	391.542	8.113	268.688	11.837	394.367	9.3
	272.738	11.603	207.138	9.96	/ 306.471 4 305.304	10.537	273.733	8.433 8.452	310.808	10.757	311.483	8.3 8 /137	382.525	11.237	391.642 390 922	8.16 8.253	270.671	11.837	393.933	9.333
	276.121	11.61	206.663	10.02	7 304.488	10.545	273.658	8.453	309.758	10.757	309.942	8.46	382	11.223	390.767	8.193	273.529	11.837	393.592	9.333
	275.913	11.617	206.088	9.93	3 302.996	10.483	272.817	8.453	308.908	10.75	308.833	8.507	380.625	11.223	388.992	8.293	272.563	11.837	392.35	9.347
	275.854	11.617	205.904	9.88	7 302.263 3 301.129	10.53	273.033	8.453 8.46	308.35	10.75	308.117	8.54/	379.6	11.237	388.542	8.287	2/1.013	11.823	391.767	9.36
	276.054	11.61	206.304	10.17	3 300.279	10.55	273.033	8.44	307.533	10.75	306.517	8.527	379.192	11.223	388.542	8.22	267.338	11.823	389.633	9.38
	276.171	11.617	206.679	9.85	3 298.354	10.523	273.275	8.427	307.125	10.75	306.358	8.5	378.667	11.223	388.783	8.293	265.938	11.823	388.808	9.373
	275.263	11.61/	206.371 206.213	9.64	7 296.979	10.543	273.233	8.453 8.44	306.158	10.743	305.225	8.52	378.108	11.267	387.942	8.4	205.146 264.913	11.823	386.875	9.38
	275.438	11.617	205.696	9.813	3 295.346	10.537	272.958	8.453	305.925	10.75	305.108	8.553	377.058	11.21	387.133	8.367	265.321	11.837	386.358	9.373
	275.579	11.61	206.138	10.04	7 294.788 8 294.379	10.543	272.733	8.433 8.437	305.892	10.743	304.883	8.547 8 532	377.025	11.237	386.508	8.287 8 197	266.863	11.823	385.733	9.373
1	273.404	11.01	200.0/1	3.30	- 234.379	10.001	212.333	0.42/	202.122	10./ 3/	504.017	ددد.ن	515.575	11.233	200.200	0.107	200.379	11.023	504.0	5.30

0.450	222.22	44 577	102.0	202.0	
9.453	232.33	11.577	493.8	293.8	
9.44	232.68	11.577	495.625	295.625	
9.473	234.11	11.563	494.75	294.75	
9.46	234.35	11.577	494.225	294.225	
0 / 97	222.69	11 562	101 55	204 55	
9.407	233.08	11.503	494.55	234.33	
9.473	233.33	11.563	495.2	295.2	
9.473	234.27	11.563	495.375	295.375	
9.473	233.15	11.577	495.025	295.025	
9.493	234.09	11.577	494.2	294.2	
9.493	233.92	11.577	494.025	294.025	
9.46	233.68	11.577	493.55	293.55	
0 472	233.00	11.577	404 55	203.55	
9.475	255.91	11.577	494.55	294.33	
9.46	233.34	11.577	494.75	294.75	
9.453	233.88	11.563	495.825	295.825	
9.46	233.15	11.563	495.2	295.2	
9.427	233.68	11.577	495.925	295.925	
9.407	234.85	11.74	495.2	295.2	
9.393	235.15	11.74	494.8	294.8	
94	235.45	11 753	496.4	296.4	
0 272	235.13	11.74	406.75	206 75	
9.575	255.05	11.74	490.75	290.75	
9.393	234.79	11.74	497.275	297.275	
9.373	234.86	11./2/	496.575	296.575	
9.367	235.28	11.713	496.225	296.225	
9.407	235.37	11.713	497.55	297.55	
9.407	235.61	11.713	497.025	297.025	
9.393	235.68	11.7	496.325	296.325	
9.38	236.09	11.7	495,975	295,975	
0 202	225.24	11.7	407 125	203.375	
2.202	255.24	11./	437.123	237.125	
9.4	236.1	11.7	496.45	296.45	-
9.407	235.83	11.7	496.95	296.95	
9.42	236.4	11.7	496.75	296.75	
9.4	237.28	11.7	497.625	297.625	
9.4	236.62	11.7	496.5	296.5	
9,407	237 22	11 7	497 2	297.2	
9 272	207.02	11.7	107.02	207.2	
0.3/3	237.14	11./	437.025	237.025	
3.50/	237.05	11./	490.7	290.7	
9.38	237.25	11.7	496.9	296.9	
9.36	237.75	11.7	496.4	296.4	
9.373	237.43	11.7	496.075	296.075	
9.34	236.9	11.7	496.55	296.55	
9.347	237.56	11.7	496.675	296.675	
9.373	237.28	11.7	496.625	296.625	
9.353	236.8	11.7	496.575	296.575	
9.34	237.31	11.7	496.55	296.55	
9.393	238.21	11.7	497.15	297.15	
9.373	238.25	11.7	497.425	297.425	
9 3 7 3	239.23	11.7	/96.1	296.1	
0.4	235.25	11.7	405.2	200.1	
0.202	239.09	11.7	493.2	233.2	
9.595	256.22	11.7	490.525	290.323	
9.393	239.56	11.7	495.325	295.325	
9.373	238.58	11./	496.35	296.35	
9.393	239.92	11.7	496.15	296.15	
9.407	239.39	11.7	495.625	295.625	
9.42	240.13	11.7	495.6	295.6	
9.387	239.92	11.7	496.15	296.15	
9.387	239.63	11.7	496.625	296.625	
9.367	239.48	11.7	496.475	296.475	
9.387	240.86	11.7	496.325	296.325	
9 3 9 3	239.8	11 7	496.8	296.8	
0 272	200.0	11.7	450.0	200.0	
0.202	235.30	11.7	400.025	207.15	
9.595	240.20	11.7	490.025	290.025	
9.407	241.23	11.7	496.575	296.575	
9.367	241.95	11.7	497.825	297.825	
9.34	240.38	11.7	497.55	297.55	
9.313	241.03	11.7	498.5	298.5	
9.333	241.1	11.7	499.45	299.45	
9.313	239.85	11.7	500.5	300.5	
9.333	240.15	11.7	501.1	301.1	
9.287	239.88	11.7	501.6	301.6	
9,307	240 52	11 7	502	302	
9,287	210.52	11 7	502 35	302 35	
9.20	240.1	11.7	502.33 E02.05	202.33	
0.20	240.8	11.7	503.05	202.05	
9.24	241.00	11./	505.075	303.075	
3.20/	242.11	11./	501.125	501.125	
9.22	240.94	11.7	503.3	303.3	
9.267	240.64	11.7	503.425	303.425	ļ
9.227	241.39	11.7	502.875	302.875	
9.247	241.46	11.7	503.175	303.175	
9.307	242.29	11.7	502.475	302.475	
9.307	241.62	11.7	501.8	301.8	
9.307	241.51	11.7	503.925	303.925	
9.3	241.23	11.7	503.875	303.875	
9.313	243.18	11.7	503.525	303.525	
9.3	242.35	11.687	503.125	303.125	
9.287	242.86	11.7	505.1	305.1	
9.32	242 58	11 687	504.05	304.05	
0.34	242.30	11 607	504.05 504.05	204.05	
0.34	242.91	11.00/	504.65 EN2 07E	204.65 202.07F	-
9.5	242.8	11.08/	505.975	201.375	-
9.333	243.63	11.687	504.275	304.275	
9.333	244.23	11.687	504.1	304.1	
9.333	242.76	11.687	503.4	303.4	
9.347	242.92	11.687	504.025	304.025	
9.36	242.83	11.687	503.175	303.175	
9.367	242.75	11.687	503.75	303.75	
9.38	242.91	11.687	504.375	304.375	
9.373	243.98	11.687	504.15	304.15	
9.38	243.38	11.687	503.775	303.775	
9.367	242.92	11.687	505.55	305.55	
9.373	244.17	11.687	504.5	304.5	
9,373	2.1.17	11 687	503 /75	202 //75	
9.38	243.72	11 687	504.075	304.075	
2.20	243.03	11.00/	504.075	504.075	

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	275.454	11.61
 | 10.53 | 272.508 | 8.433
 | 305.125 | 10.743 | 303.592 | 8.56
 | 375.325 | 11.223
 | 385.617
 | 8.227 | 270.471 | 11.823 | 384.175
 |
| | 281.404 | 11.597 | 205.746 | 10.047 | 293.496
 | 10.523 | 272.875 | 8.44
 | 304.6 | 10.737 | 303.025 | 8.533
 | 374.625 | 11.253
 | 384.917
 | 8.187 | 272.046 | 11.823 | 383.742
 |
| | 289.254 | 11.583 | 205.813 | 9,767 | 294.054
 | 10.557 | 273.342 | 8.44
 | 304.867 | 10.743 | 303.625 | 8.547
 | 374.892 | 11.26
 | 384,983
 | 8.093 | 272.604 | 11.837 | 383.675
 |
| | 202.209 | 11 593 | 228.070 | 0.76 | 202.006
 | 10 527 | 272.009 | 9.46
 | 204 225 | 10 727 | 202.025 | 9 5 4 7
 | 274.075 | 11 227
 | 204.017
 | 0.000 | 271 554 | 11 922 | 202.042
 |
| | 502.766 | 11.565 | 238.979 | 9.70 | 295.990
 | 10.557 | 272.906 | 0.40
 | 304.223 | 10.757 | 502.925 | 6.347
 | 574.075 | 11.237
 | 564.617
 | 0.2 | 2/1.554 | 11.625 | 562.642
 |
| | 325.304 | 11.563 | 279.254 | 9.833 | 294.288
 | 10.537 | 272.783 | 8.44
 | 304.167 | 10.737 | 302.8 | 8.553
 | 373.725 | 11.237
 | 383.758
 | 8.067 | 269.804 | 11.823 | 382.717
 |
| | 335.046 | 11.557 | 278.421 | 10.207 | 294.229
 | 10.523 | 272.617 | 8.427
 | 303.642 | 10.75 | 302.5 | 8.56
 | 373.025 | 11.23
 | 383.725
 | 8.113 | 267.821 | 11.823 | 382.283
 |
| | 344 346 | 11 517 | 278 854 | 10 293 | 294 079
 | 10 55 | 272.65 | 8 / 33
 | 303 492 | 10.75 | 301 733 | 8 5 3 3
 | 372 467 | 11.26
 | 382 825
 | 8.08 | 266 738 | 11 823 | 381 917
 |
| | 349.494 | 11.517 | 270.034 | 10.200 | 202.400
 | 10.55 | 272.05 | 0.433
 | 303.432 | 10.75 | 301.735 | 0.555
 | 372.407 | 11.20
 | 302.025
 | 0.00 | 200.750 | 11.025 | 301.317
 |
| | 348.421 | 11.437 | 278.438 | 10.433 | 293.488
 | 10.53 | 2/1.96/ | 8.473
 | 302.608 | 10.743 | 301.317 | 8.547
 | 3/1.642 | 11.223
 | 382.008
 | 8.027 | 265.154 | 11.823 | 381.367
 |
| | 346.729 | 11.35 | 278.713 | 10.4 | 292.963
 | 10.51 | 272.508 | 8.453
 | 302.725 | 10.737 | 300.658 | 8.58
 | 371.175 | 11.23
 | 381.617
 | 8.04 | 264.863 | 11.823 | 380.708
 |
| | 304.321 | 11.45 | 279.171 | 10.02 | 292.554
 | 10.523 | 272,167 | 8.46
 | 302.025 | 10.743 | 299.917 | 8,553
 | 370.767 | 11.253
 | 380.608
 | 8.047 | 264.804 | 11.823 | 379,967
 |
| | 201 799 | 11 / 2 | 281.654 | 10.052 | 202 670
 | 10.52 | 272 117 | 9.11
 | 201.8 | 10 727 | 200 967 | 9 572
 | 270 267 | 11 217
 | 291 225
 | 8 022 | 266.446 | 11 9 2 2 | 270 017
 |
| 16/02/201 | 14 231.788 | 11.43 | 281.034 | 10.055 | 232.079
 | 10.55 | 2/2.11/ | 0.44
 | 301.8 | 10.737 | 233.807 | 8.373
 | 370.307 | 11.217
 | 381.223
 | 8.033 | 200.440 | 11.823 | 575.517
 |
| | 291.638 | 11.423 | 281.554 | 10.593 | 292.004
 | 10.543 | 2/1.35 | 8.453
 | 301.475 | 10./3/ | 299.767 | 8.533
 | 369.517 | 11.253
 | 379.925
 | 8.013 | 267.579 | 11.823 | 3/9.41/
 |
| | 291.238 | 11.423 | 281.988 | 10.893 | 292.013
 | 10.53 | 271.517 | 8.46
 | 301.6 | 10.743 | 300.2 | 8.533
 | 369.35 | 11.267
 | 379.292
 | 8.013 | 270.154 | 11.823 | 379.45
 |
| | 289.863 | 11.423 | 282.588 | 10.797 | 295,188
 | 10.523 | 271.317 | 8.46
 | 301.333 | 10.75 | 299.733 | 8.527
 | 369.025 | 11.21
 | 378.825
 | 8.013 | 271.638 | 11.823 | 379.917
 |
| | 200.262 | 11 422 | 281 271 | 10 747 | 204.020
 | 10 51 | 270.022 | 9 46
 | 301 308 | 10 742 | 200 492 | 0 533
 | 268 522 | 11 22
 | 270 700
 | 9 OC | 271.062 | 11 0 2 2 | 380.067
 |
| | 290.505 | 11.425 | 201.271 | 10.747 | 294.929
 | 10.31 | 270.955 | 0.40
 | 301.308 | 10.745 | 299.405 | 6.335
 | 506.555 | 11.25
 | 578.708
 | 8.00 | 271.905 | 11.625 | 580.007
 |
| | 290.213 | 11.423 | 281.954 | 10./2/ | 294.371
 | 10.503 | 2/1.35 | 8.46
 | 301.042 | 10.737 | 299.5 | 8.553
 | 367.975 | 11.243
 | 378.592
 | 8.067 | 2/1.696 | 11.823 | 380.35
 |
| | 290.421 | 11.423 | 282.321 | 10.84 | 293.996
 | 10.537 | 271.983 | 8.433
 | 301.075 | 10.75 | 300 | 8.507
 | 368.183 | 11.217
 | 378.558
 | 8.073 | 269.921 | 11.823 | 381.117
 |
| | 290.096 | 11.423 | 282.088 | 10.793 | 293.088
 | 10.53 | 271.883 | 8.453
 | 300.692 | 10.743 | 299.367 | 8.473
 | 367.683 | 11.237
 | 377,258
 | 8.073 | 267.729 | 11.823 | 380.617
 |
| | 200.000 | 11.120 | 202.000 | 10.013 | 200.000
 | 10.55 | 271,005 | 0.155
 | 300 513 | 10.72 | 200.000 | 0.175
 | 200.000 | 11.207
 | 270.0
 | 0.075 | 207.1725 | 11.023 | 280.017
 |
| | 290.090 | 11.425 | 282.129 | 10.015 | 292.079
 | 10.517 | 2/1./92 | 0.435
 | 300.317 | 10.75 | 296.006 | 0.355
 | 500.965 | 11.21
 | 570.9
 | 0.00 | 200.058 | 11.025 | 560.058
 |
| | 290.271 | 11.423 | 282.213 | 10.86 | 292.329
 | 10.497 | 272.275 | 8.46
 | 300.575 | 10.743 | 298.958 | 8.533
 | 367.217 | 11.237
 | 376.583
 | 8.107 | 265.163 | 11.823 | 381.008
 |
| | 290.271 | 11.423 | 281.679 | 10.807 | 292.154
 | 10.537 | 272.008 | 8.46
 | 300.225 | 10.743 | 299.092 | 8.493
 | 366.808 | 11.253
 | 375.783
 | 8.127 | 264.288 | 11.823 | 381.008
 |
| | 290 271 | 11 423 | 282 121 | 10 867 | 291 863
 | 10 53 | 272.05 | 8 453
 | 300.4 | 10 743 | 298 867 | 8 507
 | 366 983 | 11 217
 | 375 958
 | 8 127 | 264 463 | 11 823 | 381 317
 |
| | 200.700 | 11 422 | 201.220 | 10.072 | 201.271
 | 10.55 | 271 702 | 0.472
 | 200.1 | 10 742 | 200.742 | 0.537
 | 200.1 | 11.22
 | 275 5 67
 | 0.127 | 201.070 | 11 022 | 201 225
 |
| | 289.796 | 11.423 | 281.329 | 10.873 | 291.271
 | 10.55 | 2/1./92 | 8.473
 | 300.1 | 10.743 | 298.742 | 8.527
 | 300.1 | 11.23
 | 3/5.50/
 | 8.127 | 264.979 | 11.823 | 381.325
 |
| | 289.571 | 11.423 | 281.813 | 10.847 | 291.104
 | 10.483 | 271.742 | 8.46
 | 299.933 | 10.75 | 298.558 | 8.513
 | 365.875 | 11.23
 | 375.25
 | 8.14 | 266.796 | 11.823 | 381.275
 |
| | 289.921 | 11.423 | 281.721 | 10.827 | 290.929
 | 10.53 | 272.183 | 8.453
 | 299.758 | 10.75 | 298.333 | 8.5
 | 365.642 | 11.223
 | 374.625
 | 8.167 | 268.838 | 11.823 | 381.317
 |
| | 289 746 | 11 //23 | 281 188 | 10.88 | 290 404
 | 10 557 | 271 917 | 8.46
 | 200 583 | 10 737 | 298 733 | 8 5 2 7
 | 365 | 11 237
 | 37/ 225
 | 8 167 | 270 529 | 11 823 | 381 183
 |
| | 200.034 | 11.423 | 201.100 | 10.00 | 200.404
 | 10.557 | 271.517 | 0.450
 | 255.565 | 10.737 | 200.733 | 0.527
 | 303 | 11.207
 | 374.223
 | 0.107 | 270.525 | 11.025 | 300.050
 |
| | 289.921 | 11.423 | 281.496 | 10.867 | 289.996
 | 10.517 | 271.692 | 8.453
 | 299.758 | 10.743 | 298.242 | 8.533
 | 364.65 | 11.223
 | 3/3.86/
 | 8.167 | 2/1.521 | 11.823 | 380.958
 |
| 1 | 289.396 | 11.423 | 281.229 | 10.86 | 290.113
 | 10.53 | 271.692 | 8.46
 | 299.758 | 10.743 | 297.842 | 8.507
 | 364.3 | 11.21
 | 373.333
 | 8.16 | 271.113 | 11.823 | 381.092
 |
| 1 | 289.746 | 11.423 | 281.671 | 10.867 | 289.938
 | 10.523 | 272.133 | 8.46
 | 299.292 | 10.75 | 298.017 | 8.52
 | 364.3 | 11.217
 | 372.842
 | 8.14 | 269.596 | 11.823 | 381
 |
| 1 | 200 /// | 11 /17 | 281 220 | 10 947 | 280 246
 | 10 /77 | 271 202 | 0 10
 | 209 917 | 10.75 | 207 /09 | 9 40 2
 | 262.2 | 11 217
 | 272 267
 | 0 1/7 | 267 070 | 11 072 | 380 659
 |
| 1 | 205.440 | 11.41/ | 201.323 | 10.047 | 203.340
 | 10.477 | 2/1.592 | 0.40
 | 230.017 | 10.75 | 237.400 | 0.495
 | 0.00 | 11.21/
 | 372.307
 | 0.147 | 207.079 | 11.025 | 200.050
 |
| 1 | 289.396 | 11.423 | 281.504 | 10.967 | 289.413
 | 10.523 | 272.1 | 8.48
 | 298.592 | 10.75 | 296.783 | 8.507
 | 362.9 | 11.217
 | 3/1.342
 | 8.147 | 265.396 | 11.823 | 380.167
 |
| 1 | 289.396 | 11.423 | 281.471 | 10.867 | 289.121
 | 10.517 | 272.067 | 8.453
 | 298.533 | 10.743 | 296.35 | 8.527
 | 362.725 | 11.223
 | 370.508
 | 8.213 | 263.879 | 11.823 | 379.733
 |
| 1 | 289.246 | 11.423 | 281.504 | 10.913 | 289.088
 | 10.517 | 271.967 | 8.453
 | 297.917 | 10.737 | 296.65 | 8.52
 | 362.108 | 11.223
 | 370.142
 | 8.14 | 263.146 | 11.823 | 379.633
 |
| 1 | 200.000 | 11 417 | 201 706 | 10.027 | 200 762
 | 10 51 | 272.250 | 0 4 6
 | 207 042 | 10.75 | 206 542 | 0 52
 | 261.0 | 11 217
 | 260 622
 | 0 1 6 7 | 262 404 | 11 012 | 270.250
 |
| 1 | 289.096 | 11.41/ | 201./90 | 10.92/ | 208./03
 | 10.51 | 2/2.258 | 8.46
 | 237.942 | 10.75 | 290.542 | 8.52
 | 201.9 | 11.41/
 | 509.633
 | 8.10/ | 203.404 | 11.823 | 5/3.238
 |
| 17/02/201 | 289.421 | 11.417 | 281.371 | 10.927 | 289.146
 | 10.537 | 272.767 | 8.453
 | 298.383 | 10.743 | 296.517 | 8.52
 | 361.758 | 11.21
 | 369.342
 | 8.18 | 264.371 | 11.823 | 379.633
 |
| 1,02,20 | 289.421 | 11.417 | 281.329 | 10.947 | 289.029
 | 10.53 | 272.592 | 8.46
 | 298.033 | 10.75 | 296.875 | 8.507
 | 361.525 | 11.197
 | 369.033
 | 8.147 | 265.888 | 11.823 | 379.192
 |
| 1 | 288 806 | 11 417 | 281 288 | 10.907 | 288 563
 | 10 51 | 272 017 | 8 433
 | 298 208 | 10.75 | 296.3 | 8 493
 | 361 233 | 11.223
 | 368 325
 | 8 102 | 267 579 | 11 823 | 378.75
 |
| 1 | 200.000 | 11 400 | 201 220 | 10.052 | 200.000
 | 10 51 | 272.017 | 0 470
 | 200.200 | 10.75 | 200.0 | 0 -
 | 260 002 | 11 217
 | 200.020
 | 0.10 | 260 621 | 11 012 | 279 075
 |
| | 200.721 | 11.425 | 201.329 | 10.955 | 200.215
 | 10.31 | 272.436 | 6.475
 | 297.742 | 10.75 | 290.008 | 8.5
 | 300.883 | 11.217
 | 506.5
 | 0.10 | 209.021 | 11.625 | 578.925
 |
| | 287.696 | 11.417 | 281.529 | 10.953 | 288.179
 | 10.517 | 272.658 | 8.433
 | 297.942 | 10.737 | 296.275 | 8.52
 | 360.908 | 11.223
 | 367.633
 | 8.173 | 270.638 | 11.823 | 379.392
 |
| | 287.996 | 11.417 | 281.254 | 10.94 | 288.129
 | 10.517 | 272.383 | 8.46
 | 298.008 | 10.73 | 296 | 8.507
 | 360.217 | 11.203
 | 367.625
 | 8.233 | 270.588 | 11.823 | 379.25
 |
| | 287.696 | 11.417 | 281.263 | 10.913 | 287.654
 | 10.49 | 271,992 | 8.433
 | 297.417 | 10.75 | 296.008 | 8.5
 | 359.858 | 11.217
 | 367,367
 | 8.22 | 268.888 | 11.81 | 378.725
 |
| | 207 046 | 11 417 | 281.004 | 10.047 | 200 020
 | 10 527 | 373 167 | 9 46
 | 207 217 | 10 727 | 205.95 | 0 5 7 7
 | 250.267 | 11 22
 | 267.075
 | 0 173 | 266 921 | 11.01 | 370.1
 |
| | 207.040 | 11.417 | 281.904 | 10.947 | 200.030
 | 10.557 | 2/5.10/ | 0.40
 | 297.217 | 10.757 | 293.63 | 6.327
 | 559.507 | 11.25
 | 507.075
 | 0.1/5 | 200.821 | 11.01 | 579.1
 |
| | 287.521 | 11.41/ | 281.579 | 10.953 | 287.479
 | 10.51 | 272.442 | 8.433
 | 297.242 | 10.743 | 295.258 | 8.507
 | 359.042 | 11.203
 | 366.217
 | 8.22 | 265.038 | 11.81 | 378.508
 |
| | 287.496 | 11.417 | 281.779 | 10.973 | 287.396
 | 10.497 | 272.508 | 8.433
 | 296.867 | 10.75 | 295.592 | 8.5
 | 358.842 | 11.21
 | 365.617
 | 8.26 | 263.671 | 11.823 | 378.308
 |
| | 287.846 | 11.417 | 281.513 | 10.967 | 287.279
 | 10.503 | 273,175 | 8.44
 | 297.217 | 10.737 | 295,725 | 8.493
 | 358.842 | 11.21
 | 365,483
 | 8.253 | 262,504 | 11.81 | 378.442
 |
| | 207.010 | 11.117 | 201.010 | 10.047 | 207.273
 | 10.505 | 273.173 | 9 407
 | 207.217 | 10.75 | 205.125 | 9.53
 | 350.012 | 11 217
 | 366.017
 | 0.200 | 262.001 | 11 022 | 378 708
 |
| | 200.340 | 11.417 | 202.313 | 10.947 | 207.005
 | 10.525 | 275.042 | 8.407
 | 297.217 | 10.75 | 290.125 | 0.32
 | 559.508 | 11.217
 | 500.017
 | 0.207 | 202.634 | 11.625 | 378.708
 |
| | 288.196 | 11.41/ | 282.004 | 10.927 | 287.221
 | 10.51 | 2/3.533 | 8.453
 | 297.508 | 10.743 | 296.617 | 8.507
 | 359.192 | 11.203
 | 365.975
 | 8.267 | 263.496 | 11.823 | 3/8.267
 |
| | 288.021 | 11.417 | 281.779 | 11.02 | 287.396
 | 10.497 | 273.042 | 8.473
 | 297.683 | 10.737 | 296.792 | 8.533
 | 359.833 | 11.21
 | 366.817
 | 8.233 | 264.721 | 11.823 | 378.442
 |
| | 288.546 | 11.417 | 281.729 | 10.96 | 287.454
 | 10.51 | 273.125 | 8.427
 | 298.208 | 10.75 | 297.408 | 8.52
 | 359.892 | 11.223
 | 367.967
 | 8.32 | 266.529 | 11.823 | 378.258
 |
| | 288 546 | 11 /17 | 282 529 | 10 973 | 287 629
 | 10 / 97 | 273 258 | 8.42
 | 208 325 | 10 7/13 | 297 275 | 8 507
 | 360 183 | 11 217
 | 368 633
 | 8 2/17 | 268 396 | 11 873 | 378 658
 |
| | 200.540 | 11.417 | 202.525 | 10.373 | 207.025
 | 10.457 | 273.230 | 0.42
 | 200.525 | 10.745 | 257.275 | 0.507
 | 350.103 | 11.217
 | 300.033
 | 0.247 | 200.330 | 11.025 | 378.050
 |
| | 288.521 | 11.41/ | 282.854 | 10.783 | 287.954
 | 10.55 | 2/3.31/ | 8.433
 | 298.183 | 10.737 | 298 | 8.507
 | 359.692 | 11.223
 | 368.692
 | 8.227 | 269.946 | 11.823 | 378.717
 |
| | 288.021 | 11.417 | 281.463 | 10.953 | 287.629
 | 10.503 | 272.725 | 8.4
 | 297.858 | 10.743 | 297.408 | 8.507
 | 359.192 | 11.223
 | 368.367
 | 8.253 | 269.504 | 11.81 | 378.258
 |
| | 288.221 | 11.417 | 281.571 | 10.947 | 288.354
 | 10.517 | 273.367 | 8.427
 | 298.233 | 10.743 | 297.383 | 8.5
 | 359.042 | 11.237
 | 367.808
 | 8.247 | 268.654 | 11.81 | 378.767
 |
| | 287 821 | 11 417 | 281 521 | 10 967 | 288 071
 | 10 51 | 272 917 | 84
 | 297 367 | 10 75 | 297.2 | 8 5 2
 | 358 525 | 11 21
 | 367 758
 | 8 293 | 266 446 | 11 823 | 378.05
 |
| | 207.021 | 11.117 | 201.521 | 10.072 | 200.071
 | 10.51 | 272.317 | 0.1
 | 207.075 | 10 727 | 206 667 | 9 507
 | 350.525 | 11.10
 | 366.059
 | 0.255 | 266.110 | 11.025 | 378.45
 |
| | 207.021 | 11.417 | 281.788 | 10.373 | 288.071
 | 10.51 | 273.317 | 0.433
 | 237.075 | 10.737 | 230.007 | 8.307
 | 338.175 | 11.19
 | 300.338
 | 8.233 | 204.223 | 11.01 | 578.45
 |
| | 287.846 | 11.417 | 282.304 | 10.953 | 288.388
 | 10.51 | 273.167 | 8.42
 | 297.042 | 10.743 | 296.383 | 8.507
 | 358.2 | 11.203
 | 367.075
 | 8.247 | 262.621 | 11.81 | 378.167
 |
| | 287.846 | 11.417 | 281.729 | 10.967 | 288.213
 | 10.49 | 273.125 | 8.44
 | 296.692 | 10.73 | 296.208 | 8.5
 | 357.675 | 11.21
 | 366.233
 | 8.227 | 261.454 | 11.81 | 377.858
 |
| | 288.171 | 11.417 | 282.054 | 11.007 | 288.538
 | 10.49 | 273.45 | 8.42
 | 297.075 | 10.737 | 296.533 | 8.52
 | 357.767 | 11.197
 | 365.358
 | 8.3 | 261.313 | 11.81 | 378.183
 |
| | 200 021 | 11 / 17 | 282 028 | 11 007 | 200 116
 | 10 517 | 272.2 | 9 427
 | 206 575 | 10 72 | 206 117 | 9 5
 | 2575 | 11 202
 | 265.075
 | 9 267 | 261 206 | 11 01 | 277 767
 |
| 18/02/201 | 14 200.021 | 11.41/ | 202.030 | 10.007 | 200.440
 | 10.31/ | 273.3 | 0.427
 | 2,0.070 | 10.75 | 2./0.11/ | 0.5
 | 257.3 | 11.203
 | 303.073
 | 0.207 | 201.330 | 11.01 | 377.707
 |
| | 288.221 | 11.41/ | 283.079 | 10.997 | 288.646
 | 10.51 | 2/36/5 | 8.407
 | 300 05 | 10/3/ | 205 025 | 8.547
 | 357.525 | 11.21
 | 36/1/83
 | 8.253 | /6/8/1 | 44.04 |
 |
1	288.696	11.417		
 | | 275.075 |
 | 296.95 | 10.757 | 295.825 |
 | |
 | 504.705
 | | - | 11.81 | 3/8.2/5
 |
| | 288.871 | | 282.396 | 11.027 | 288.771
 | 10.537 | 273.925 | 8.42
 | 296.95
297.308 | 10.737 | 295.825
296.608 | 8.527
 | 357.825 | 11.197
 | 365.433
 | 8.28 | 264.521 | 11.81
11.81 | 378.658
 |
| 1 | 288.404 | 11.417 | 282.396
282.788 | 11.027
11.02 | 288.771
288.829
 | 10.537
10.503 | 273.925
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 |
| 1 | -00.704 | 11.417
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9.407	243.53	11.687	503.925	303.925	
9.42	243.72	11.687	504.575	304.575	
9.407	243.96	11.687	504.05	304.05	
9.42	243.08	11.687	503.175	303.175	
9.42	243.8	11.687	503.125	303.125	
9.427	242.53	11.687	502.625	302.625	
9.42	242.83	11.687	502.925	302.925	
9.433	243.03	11.687	503.125	303.125	
9.407	243.95	11.687	503.275	303.275	
9.42	243.73	11.687	503.825	303.825	
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9.407	244.43	11.087	504.525	304.323	
9.4	244.31	11.687	504.4	304.4	
9.4	244.26	11.687	504.35	304.35	
9.393	245.2	11.687	504.525	304.525	
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9.42	244.61	11.687	504.7	304.7	
9.38	243.84	11.687	504.7	304.7	
9.407	244.78	11.687	504.875	304.875	
9.407	244.31	11.687	504.4	304.4	
9.4	244.85	11.687	504.175	304.175	
9.42	246.26	11.687	503.475	303.475	
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9.4	247.29	11.687	502.975	302.975	
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9.367	247.53	11.687	502.45	302.45	
9.427	247.53	11.687	502.45	302.45	
9.427	247.53	11.687	504.45	304.45	
9.427	247.36	11.687	504.275	304.275	
9.44	247.53	11.687	503.45	303.45	
9.407	247.88	11.687	503.8	303.8	
9.433	248.65	11.687	502.8	302.8	
9.42	247.44	11.687	503.125	303.125	
9.42	247.88	11.687	502.8	302.8	
9.413	249.03	11.687	503.175	303.175	
9.407	248.21	11.687	503.125	303.125	
9.407	248.98	11.687	503.125	303.125	
9.373	248.83	11.673	502.975	302.975	
9 393	249.42	11 673	502.8	302.8	
9 4 2 7	250 51	11.673	503 125	303 125	
9.127	250.31	11.673	502.975	302.975	
9.427	250.50	11.073	503 35	303 35	
0.433	250.75	11.075	503.55	204	
9.435	250.02	11.007	503 535	202 504	
9.427	251.14	11.007	505.525	303.323	
9.595	250.97	11.007	505.55	303.33	
9.433	251.14	11.673	503.525	303.525	
9.4	251.32	11.68/	503.7	303.7	
9.4	251.91	11.6/3	503.525	303.525	
9.4	252.38	11.673	504.225	304.225	
9.42	252.38	11.673	504.225	304.225	
9.433	251.98	11.673	503.825	303.825	
9.433	252.97	11.673	504.05	304.05	
9.427	253.86	11.673	504.175	304.175	
9.42	253.51	11.673	503.825	303.825	
9.42	253.16	11.673	503.475	303.475	
9.4	254.28	11.673	503.825	303.825	
9.407	254.33	11.673	503.875	303.875	
9.373	254.28	11.673	503.825	303.825	
9.407	254.69	11.673	503.475	303.475	
9.453	254.39	11.673	503.175	303.175	
9.42	255.88	11.673	503.125	303.125	
9.44	254.96	11.673	502.975	302.975	
9.453	255.6	11.673	503.275	303.275	
9.453	255.6	11.673	502.275	302.275	
9.433	255.3	11.673	501.975	301.975	
9.427	255.13	11.673	501.8	301.8	
9.433	256.02	11.673	501.925	301.925	
9,433	256.78	11.673	501.925	301.925	
9.4	256.70	11.673	502.625	302.625	
9.44	256.67	11.673	502.575	302.575	
9 /152	256.90	11.672	502.373	302.373	<u> </u>
2.433 0.44	20.89	11.073	502.8 503 075	202.8	
2.44	257.07	11.075	502.375	202.375	
0.44	(30.0	11.073	502.275	202.275	
9.44	250.0	11.6	502.475	5UZ.4/5	
9.44	257.57	11.673	E00 475	2117.175	
9.44 9.427 9.387	257.57	11.673	502.175	302.175	
9.44 9.427 9.387 9.4	257.57 257.5 257.08	11.673 11.673 11.673	502.175 502.325	302.325	
9.44 9.427 9.387 9.4 9.42	257.57 257.5 257.08 257.63	11.673 11.673 11.673 11.673	502.175 502.325 502.875	302.325 302.875	
9.44 9.427 9.387 9.4 9.42 9.42 9.44	257.57 257.5 257.08 257.63 257.63	11.673 11.673 11.673 11.673 11.657	502.175 502.325 502.875 501.7	302.325 302.875 301.7	
9.44 9.427 9.387 9.4 9.42 9.44 9.43	257.57 257.5 257.08 257.63 257.68 257.68	11.673 11.673 11.673 11.673 11.657 11.673	502.175 502.325 502.875 501.7 502.95	302.325 302.875 301.7 302.95	
9.44 9.427 9.387 9.4 9.42 9.44 9.433 9.427	257.57 257.57 257.63 257.63 257.68 257.64 257.4 256.74	11.673 11.673 11.673 11.673 11.657 11.673 11.673	502.175 502.325 502.875 501.7 502.95 501.825	302.325 302.875 301.7 302.95 301.825	
9.44 9.427 9.387 9.4 9.42 9.44 9.433 9.427 9.407	257.57 257.5 257.68 257.68 257.68 257.44 256.74 257.38	11.673 11.673 11.673 11.673 11.673 11.673 11.673 11.673	502.175 502.325 502.875 501.7 502.95 501.825 503.225	302.325 302.875 301.7 302.95 301.825 303.225	
9.44 9.427 9.387 9.4 9.42 9.44 9.433 9.427 9.407 9.407 9.4	257.57 257.57 257.63 257.63 257.63 257.64 257.44 257.44 257.48 257.48 257.48 257.48	11.673 11.673 11.673 11.673 11.673 11.673 11.673 11.673 11.657	502.175 502.325 502.875 501.7 502.95 501.825 503.225 503.225	302:173 302:325 302:875 301.7 302:95 301:825 303:225 303:25	

	289.696 290.071	11.417 11.417	285.021 285.029	11.027 11.04	287.263 287.988	10.51 10.49	277.35	8.487 8.493	296.792 297.517	10.723	297.233 297.508	8.593 8.587	354.975	11.203	365.792 366.6	8.527	262.954 261.871	11.81 11.797	383.017 384.092	9.42 9.38
	289.021	11.417	284.588	11.047	287.988	10.503	276.783	8.487	296.642	10.717	296.933	8.587	354.825	11.197	365.358	8.56	259.188	11.797	383.917	9.373
	289.146 288.854	11.417 11.417	284.796 284.521	11.047 11.04	288.638 288.696	10.443	276.858 277.25	8.48 8.48	296.3 296.183	10.717	295.942 295.933	8.62	354.308 354.017	11.177 11.21	364.767 364.492	8.573 8.553	257.563 256.571	11.797 11.783	383.858 383.85	9.393 9.367
20/02/2014	289.029	11.417	284.471	11.047	289.046	10.477	277.067	8.487	296.183	10.717	295.883	8.607	354.658	11.217	364.575	8.567	256.046	11.783	384.2	9.36
	288.679	11.417	284.104 284.146	11.067	289.279 289.571	10.483	276.433 276.608	8.48 8.493	296.767 297.583	10.723	297.117 298.358	8.593	356.058 357.4	11.19	367.942 371.183	8.567	256.979 256.804	11.783	384.767 384.675	9.373
	288.829	11.417	284.254	11.067	289.896	10.483	276.583	8.487	297.85	10.703	298.333	8.613	357.083	11.19	371.958	8.573	258.646	11.797	384.65	9.373
	288.504	11.417	283.838 284.104	11.06	290.038	10.497	276.167	8.487	297.7 297.408	10.717	298.45 298.05	8.607	356.058	11.197	370.742 369.942	8.567	259.779 261.238	11.797	384.367 384.767	9.367
	289.204	11.417	284.679	11.06	291.146	10.477	277.008	8.487	297.583	10.717	298.225	8.593	356.583	11.177	369.717	8.587	261.996	11.797	384.808	9.367
	289.029	11.417	284.990	11.047	291.140	10.45	277.108	8.487	297.058	10.717	297.792	8.607	355.708	11.203	367.417	8.6	259.546	11.797	383.708	9.393
	289.404	11.417	284.846	11.073	291.521	10.483	277.308	8.493 8 507	296.967 296.392	10.71	297.325	8.587	355.558	11.217	367.217	8.567	258.113	11.783	384.708	9.367
	289.029	11.417	284.604	11.087	290.913	10.477	276.933	8.507	295.892	10.71	296.55	8.593	354.833	11.183	365.642	8.62	254.821	11.783	384.333	9.393
	289.204 289.054	11.417 11.417	284.379 284.629	11.08 11.087	290.796 290.354	10.457 10.483	277.642 277.492	8.493 8.513	296.242 295.625	10.703 10.71	296.058 295.642	8.627 8.593	354.658 354.392	11.183 11.19	364.75 364.067	8.62 8.64	254.179 253.621	11.783 11.783	384.642 384.492	9.38 9.367
	289.554	11.417	285.179	11.08	290.446	10.503	277.775	8.513	295.425	10.71	295.792	8.533	354.542	11.203	363.55	8.64	254.588	11.783	384.508	9.353
	289.171 288.996	11.417 11.417	284.504 284.863	11.08 11.047	289.538 289.479	10.483	276.833 277.192	8.487	294.575 294.75	10.71	295.117 294.942	8.547	353.342 353.167	11.19	362.608 361.9	8.607	254.963 256.129	11.783 11.797	384.1 383.792	9.373
	288.796	11.417	284.846	11.093	288.929	10.457	277.175	8.507	294.492	10.717	294.525	8.473	352.267	11.177	361.35	8.64	256.571	11.797	383.508	9.393
	288.846	11.41	283.340	11.087	288.540	10.303	277.375	8.513	294.107	10.71	294.425	8.593	351.707	11.19	360.217	8.64	257.613	11.783	382.775	9.4
	288.646 288.321	11.41 11.41	284.579 284.929	11.08 11.087	287.438	10.483 10.49	277.308	8.513 8.52	293.758 293.433	10.717	293.458 292.608	8.607	351.417	11.19	359.617	8.653 8.627	256.363 254.463	11.783 11.783	382.842	9.36 9.38
	289.963	11.417	284.004	11.107	286.421	10.47	276.6	8.52	292.333	10.717	291.95	8.62	349.817	11.223	358.108	8.593	252.079	11.783	380.933	9.4
	287.588 287.863	11.41 11.41	283.513 284.104	11.087 11.087	285.329 285.254	10.463 10.463	276.642 276.7	8.527 8.52	291.883 291.808	10.71 10.717	291.592 291.25	8.64 8.613	349.367 349.117	11.19	356.95 356.475	8.66 8.607	250.638 249.921	11.783 11.783	380.842 380.9	9.4 9.393
21/02/2014	287.913	11.41	283.621	11.087	284.488	10.477	276.483	8.52	291.858	10.717	291.433	8.587	348.817	11.183	356.392	8.653	249.563	11.783	381.35	9.373
	288.213	11.41 11.41	284.004	11.107 11.093	284.846 284.204	10.497	276.733	8.52	291.983 291.692	10.703	291.683 291.15	8.62	348.942 348.767	11.19 11.19	356.108 356.242	8.633	250.446	11.783 11.783	381.333 381.6	9.393
	287.363	11.41	283.679	11.08	283.413	10.477	276.275	8.54	290.9	10.71	290.692	8.573	348.092	11.19	356.05	8.593	251.813	11.797	381.408	9.42
	288.238	11.41	284.296	11.073	203.308	10.45	276.892	8.56	291.075	10.71	290.6	8.607	347.975	11.103	354.933	8.62	253.588	11.797	381.758	9.407
	288.113 288.288	11.41	284.396 284.479	11.087 11.093	282.821 282.821	10.463	276.458	8.54 8.553	290.6 291.242	10.703	290.342 290.025	8.607	347.325	11.177	355.033	8.62	254.313 253.846	11.783	381.858 382.208	9.373 9.407
	287.888	11.41	284.738	11.093	282.013	10.49	276.4	8.54	290.783	10.71	290.283	8.62	347.1	11.183	354.708	8.62	251.871	11.783	382.2	9.387
	287.596 287.763	11.41 11.41	284.029 283.679	11.093 11.113	281.663 281.421	10.497 10.483	276.225 276.542	8.547 8.547	290.083 290.133	10.71 10.703	289.308 289.625	8.653 8.607	347.1 346.8	11.197 11.183	354.4 354.317	8.653 8.66	250.238 248.829	11.783 11.783	382.292 382.208	9.38 9.4
	287.771	11.41	284.071	11.12	281.196	10.477	276.267	8.547	289.792	10.71	289.217	8.56	346.283	11.183	353.775	8.593	247.904	11.783	382.2	9.393
	287.246	11.41 11.41	283.671 284.079	11.107	280.729 280.429	10.49	276.808	8.56	289.442 289.492	10.697	288.817 288.958	8.593	346.458 346.333	11.1// 11.19	353.642 354.183	8.62	246.971 247.429	11.//	382.2 381.942	9.373
	287.413	11.41	283.596	11.107	280.079	10.457	276.592	8.56	289.142	10.71	288.875	8.56	346.158	11.177	353.433	8.62	247.663	11.783	381.592	9.353
	287.238	11.41	283.513	11.12	279.613	10.457	276.242	8.547	288.733	10.703	288.392	8.58	345.4	11.103	353.483	8.653	249.354	11.783	381.508	9.4
	287.563 287.563	11.41 11.41	284.029 283.904	11.12 11.113	279.354 279.004	10.47 10.49	276.492 276.9	8.56 8.56	288.592 288.358	10.71 10.703	287.975 288.25	8.62 8.593	344.733 344.558	11.177	352.8 353.075	8.653 8.653	250.088 250.146	11.783 11.783	380.825 380.7	9.4
	287.038	11.41	283.963	11.107	278.421	10.49	276.692	8.56	287.833	10.697	287.508	8.62	343.508	11.21	351.933	8.647	249.388	11.77	379.825	9.4
	286.854 286.654	11.41	283.679 283.446	11.12	278.354 277.454	10.45	276.275	8.547	286.775 286.867	10.697	286.958 286.592	8.62	342.975 342.425	11.177	350.85	8.653	247.746 246.029	11.783	378.875	9.393
	286.304	11.41	283.413	11.12	276.929	10.483	275.742	8.58 8.56	286.458	10.717	286.158	8.573	341.55	11.183	350.183	8.627	244.046	11.753	377.142	9.4
22/02/2014	286.479	11.41	283.646	11.113	276.404	10.437	275.975	8.553	285.642	10.703	285.592	8.627	341.375	11.203	349.483	8.633	242.529	11.753	377.108	9.407
	286.479 286.479	11.41 11.41	282.804 283.163	11.127 11.127	276.054 276.054	10.49 10.47	275.667 275.892	8.58 8.573	285.467 285.817	10.697 10.697	285.55 285.508	8.627 8.547	341.025 340.85	11.177	349.575 349.8	8.653 8.667	242.763 243.229	11.753 11.753	376.933 376.758	9.393 9.407
	286.946	11.41	284.188	11.123	275.588	10.43	275.983	8.56	285.408	10.69	285.467	8.593	340.675	11.19	349.092	8.627	243.871	11.753	376.983	9.4
	286.796	11.41 11.41	283.463 283.996	11.12 11.127	275.554 275.088	10.443	276.058	8.573	285.433 285.317	10.703	285.408 285.142	8.573	340.35 340.525	11.1// 11.163	348.633 349.567	8.607	245.004 245.938	11.753 11.77	376.392 376.658	9.393
	286.621	11.41	283.563	11.133	274.679	10.477	275.625	8.56	285.025	10.703	284.575	8.653	339.767	11.17	348.6	8.68	246.054	11.77	375.825	9.407
	286.621	11.41	284.188	11.127	274.323	10.497	276.117	8.58	284.385	10.703	284.4	8.593	339.3	11.177	348.425	8.687	245.588	11.753	375.783	9.393
	286.796 286.496	11.41 11.41	283.613 284.113	11.147 11.13	273.979 273.563	10.457 10.47	275.808 275.508	8.58 8.58	284.558 284.083	10.69 10.683	284.492 284.058	8.593 8.573	339.242 338.65	11.17 11.183	347.583 347.817	8.66 8.587	244.188 242.604	11.753 11.753	375.608 375.708	9.4 9.427
	286.446	11.41	283.613	11.133	273.221	10.423	275.808	8.573	284.208	10.717	283.825	8.607	338.6	11.177	347.183	8.607	241.679	11.753	375.608	9.42
	286.646 286.471	11.41 11.41	283.721 283.713	11.153 11.133	273.246 272.838	10.477 10.463	276.05 275.775	8.58 8.58	283.942 283.825	10.703 10.71	283.667 283.658	8.573 8.587	338.508 337.983	11.203	347.158 346.883	8.627 8.62	241.004 240.713	11.753 11.753	375.583 376.642	9.407 9.407
	286.446	11.41	284.263	11.137	272.521	10.443	275.392	8.573	283.625	10.71	283.675	8.593	337.958	11.19	346.233	8.653	240.863	11.753	376.658	9.407
	286.529	11.41	283.429 283.429	11.127	272.263	10.483	275.492	8.593	283.6	10.703	283.375	8.593	337.467	11.177	346.333	8.653	241.538 242.579	11.753	376.892 377.025	9.427
	285.954 285.954	11.41 11.41	283.246 283.296	11.133 11.133	271.796 271.738	10.47 10.463	275.708 275.625	8.587 8.573	283.017 282.958	10.69 10.703	283.192 282.708	8.607 8.587	336.942 336.592	11.17 11.177	346.417 345.533	8.667 8.687	243.171 243.929	11.753 11.77	377.242	9.393 9.427
	286.179	11.41	283.696	11.147	271.496	10.49	275.358	8.593	282.717	10.703	282.975	8.58	336.467	11.17	346.067	8.66	244.446	11.753	377.425	9.42
	286.129 285.779	11.41 11.41	284.179 283.521	11.153 11.153	271.446 270.746	10.463 10.45	275.442 275.317	8.593 8.593	282.667 282.025	10.69 10.697	282.525 281.733	8.593 8.587	336.125 335.542	11.183 11.17	345.617 344.825	8.673 8.68	243.988 242.238	11.74 11.753	376.842 376.717	9.393 9.393
	285.629	11.41	283.371	11.153	270.479	10.49	275.033	8.6	281.817	10.69	281.583	8.613	334.867	11.197	344.675	8.693	240.396	11.753	376.3	9.427
23/02/2014	285.979	11.41	283.638	11.15	270.304	10.485	275.433	8.58	281.175	10.685	281.942	8.573	334.925	11.185	344.767	8.593	239.404	11.753	375.9	9.38
	286.179	11.41	283.388 283.163	11.16 11 147	270.388	10.437	275.317	8.593	281.608	10.697	281.6	8.607	334.6	11.183	344.825	8.627	238.263	11.753	376.85	9.4
	285.429	11.41	283.296	11.167	269.054	10.463	274.425	8.593	280.333	10.69	280.708	8.613	333.383	11.105	343.267	8.687	237.629	11.753	376.625	9.4
	285.779 285.954	11.41 11.41	283.071 283.863	11.167 11.167	269.054 269.113	10.45 10.463	275 275.258	8.6 8.593	280.508 280.45	10.703 10.71	280.617 280.875	8.587 8.587	333.383 333.383	11.19	343.842 343.967	8.66 8.707	238.388 239.321	11.753 11.753	376.667 377.458	9.393 9.4
	285.929	11.41	283.304	11.173	268.621	10.457	275.1	8.58	280.425	10.697	280.717	8.587	332.892	11.183	343.675	8.687	239.821	11.77	376.9	9.433
	285.604	11.41	283.029 282.929	11.16	268.346	10.457	274.558	8.6 8.6	279.8 279.925	10.697	279.908 279.942	8.587	332.092 332.042	11.163	342.867 342.233	8.687	239.546 239.788	11.77	376.625 376.525	9.407
	285.604	11.41	283.054	11.173	268.238	10.483	274.85	8.607	279.983	10.71	279.933	8.613	332.392	11.163	342.492	8.713	239.438	11.753	377.45	9.393
	285.513	11.41	283.829	11.16/	267.504	10.43	275.092	8.613	279.95	10.717	279.908	8.607	331.95	11.183	342.6	8.653	238.588	11.753	377.908	9.38
	285.513 285.638	11.41 11.41	283.721 283.971	11.173 11.173	267.388 267.104	10.47 10.443	274.983 274.7	8.613 8.613	279.425 279.375	10.69 10.683	279.533 279.517	8.587 8.593	331.775 331.783	11.17	341.958 341.942	8.713 8.713	236.488	11.753	377.85	9.42 9.393
	285.788	11.41	283.704	11.173	267.371	10.437	274.833	8.613	279.817	10.697	279.783	8.593	331.583	11.177	342.475	8.713	236.121	11.77	379.7	9.367
	285.696 285.671	11.41 11.41	284.604 283.771	11.17 11.193	266.988 266.846	10.457 10.463	274.533 274.767	8.607 8.607	279.667 279.35	10.69 10.703	280.017 279.317	8.613 8.613	331.492 331.292	<u>11.177</u> 11.17	341.642 341.742	8.693 8.727	236.554 236.821	11.753 11.753	380.733 380.167	9.367 9.387
	285.646	11.41	283.604	11.187	266.879	10.437	275.133	8.613	279.267	10.697	279.417	8.613	330.742	11.17	341.175	8.72	237.729	11.74	380.267	9.4
	285.496	11.41 11.41	283.046 284.079	11.173 11.177	266.021	10.47	273.875	8.613	278.942	10.683	279.392 278.558	8.607	330.592 329.825	11.17	341.95	8.753	238.513 238.854	11.753	380.908 380.342	9.367
	285.671	11.417	283.721	11.173	266.088	10.397	273.917	8.613	278.242	10.69	278.333	8.607 8.613	329.133	11.177	340.758	8.74 8.72	239.446	11.753	380.383	9.367
	284.646	11.41	282.913	11.173	265.121	10.425	273.242	8.627	277.8	10.677	278.1	8.613	328.05	11.103	339.15	8.713	236.771 237.721	11.753	379.175	9.367

9 4 2	257 68	11 673	503 825	303 825	
0.29	257.00	11.657	504.9	204.9	
0 272	257.50	11.057	502 725	202 725	
0.202	257.01	11.057	502.725	202.725	
9.595	257.52	11.057	505.2	202.2	
9.307	257.47	11.657	502.725	302.725	
9.30	257.82	11.657	503.075	303.075	
9.373	258.52	11.657	503.775	303.775	
9.347	257.93	11.673	501.95	301.95	
9.373	257.13	11.657	502.925	302.925	
9.367	257.75	11.657	502.775	302.775	
9.393	257.75	11.657	503.775	303.775	
9.367	258.69	11.657	503.95	303.95	
9.38	258.34	11.657	503.6	303.6	
9.393	258.57	11.657	503.25	303.25	
9.367	259.53	11.657	503.45	303.45	
9.373	259.31	11.657	503.225	303.225	
9.393	259.16	11.657	503.075	303.075	
9.38	260.1	11.657	503.25	303.25	
9.367	258.42	11.657	502.1	302.1	
9.353	259.33	11.657	501.25	301.25	
9.373	258.00	11.657	500.575	300.575	
9.4	260.02	11.057	300.4	300.4	
9.595	259.47	11.057	499.03	299.03	
9.373	259.73	11.057	500.85	300.85	
0.26	255.25	11.057	500.65	200.65	
9.38	259.72	11.643	499.8	299.8	
9.4	258.79	11.643	498.875	298.875	
9.4	258.93	11.643	498.25	298.25	
9.393	259.43	11.643	498.175	298.175	
9.373	258.91	11.643	498.225	298.225	
9.393	258.79	11.643	497.875	297.875	
9.4	258.79	11.643	496.875	296.875	
9.42	258.47	11.643	496.55	296.55	
9.4	259.41	11.643	496.725	296.725	
9.407	259.58	11.643	496.9	296.9	
9.373	259.28	11.643	496.6	296.6	
9.407	260.21	11.643	496.95	296.95	
9.387	259.76	11.643	497.075	297.075	
9.38	260.16	11.643	495.9	295.9	
9.4	259.63	11.643	495.95	295.95	
9.393	260.33	11.643	496.075	296.075	
9.373	259.76	11.643	495.075	295.075	
9.373	259.63	11.643	494.95	294.95	
9.353	259.86	11.643	494.6	294.6	
9.38	259.28	11.643	494.6	294.6	
9.4	259.51	11.643	495.25	295.25	
9.4	258.96	11.643	493.7	293.7	
9.393	259.2	11.63	495.175	295.175	
9.4	259.86	11.63	494.3	294.3	
9.393	260.04	11.617	492.95	292.95	
9.393	259.14	11.63	493.05	293.05	
9.4	259.21	11.63	493.35	293.35	
9.393	259.6	11.63	492.975	292.975	
9.407	259.28	11.617	492.65	292.65	
9.393	259.1	11.617	492.475	292.475	
9.407	259.69	11.617	492.3	292.3	
9.4	260.28	11.617	492.125	292.125	
9.393	259.96	11.617	491.8	291.8	
9.393	259.96	11.63	491.8	291.8	
9.407	259.26	11.63	492.1	292.1	
9.407	260.44	11.63	490.75	290.75	
9.393	260.62	11.61/	491.925	291.925	
9.4	260.44	11.61/	490.75	290.75	
9.42/	259.38	11.617	491.45	291.45	-
9.42	259.68	11.01/	490.75	290.75	
9.407	260.05	11.617	491.125	291.125	
9.4U/ Q 407	260.58	11.01/	491.05	291.65	
9.40/ Q 177	259.96	11.01/	490.8	290.8	
9 202	203.09	11 617	490.3	230.3	
9 202	200.00	11 617	450.7	200.7	
9.427	260.81	11 617	490.05	230.03	
9.42	260.86	11.617	490.7	290.7	
9.393	260.81	11.617	490.65	290.65	
9.393	260.28	11.603	490.125	290.125	
9.427	260.9	11.603	488.975	288.975	
9.427	260.73	11.617	489.8	289.8	
9.38	260.9	11.617	488.975	288.975	
9.4	260.68	11.617	489.525	289.525	
9.4	261.23	11.617	488.3	288.3	
9.4	259.69	11.617	488.3	288.3	
9.393	259.87	11.603	488.475	288.475	
9.4	260.39	11.617	488	288	
9.433	261.13	11.603	488.975	288.975	
9.407	260.86	11.603	487.7	287.7	
9.44	260.39	11.603	487	287	
9.393	260.92	11.577	487.525	287.525	
9.38	261.29	11.603	487.9	287.9	
9.393	260.88	11.603	487.25	287.25	
9.42	260.22	11.59	487.125	287.125	
9.393	260.87	11.603	487.775	287.775	
9.367	261.3	11.603	485.975	285.975	
9.367	261.63	11.603	486.875	286.875	
9.387	260.59	11.603	486.375	286.375	
9.4	261.67	11.59	486.875	286.875	
9.367	260.51	11.59	486.25	286.25	
9.367	260.21	11.59	486.95	286.95	
9.367	260.94	11.603	485./25	285./25	
9.347	261.21	11.603	486.225	286.225	
0.207	A 6 6 7 1			305 05	

24/02/2014	284.771	11.41	283.446	11.187	264.838	10.463	273.908	8.607	277.05	10.697	277.125	8.613	327.3	11.17	339.283	8.727	236.504	11.74	378.908	9.353
	284.646	11.41	283.138	11.173	264.771	10.45	273.867	8.613	276.925	10.69	276.95	8.613	327.233	11.143	338.842	8.713	235.271	11.74	379	9.367
	284.421	11.417	282.996	11.187	264.079	10.45	272.925	8.613	276.35	10.69	276.808	8.613	326.833	11.163	338.567	8.727	234.171	11.74	3/8.858	9.347
	284.946	11.417	283.304	11.173	264.254	10.417	273.9	8.627	2/6./	10.69	2/6.85	8.613	326.658	11.157	338.608	8.753	233.529	11.74	379.033	9.353
	284.971	11.41	283.588	11.173	264.046	10.41	2/3.05	8.033	276.783	10.69	276.733	8.013	320.858	11.157	338.492	8.747	233.438	11.74	379.45	9.367
	285.029	11.41	203.271	11.195	204.590	10.405	273.735	8 622	276.008	10.67	276.622	8 612	320.742	11.21	229 125	0.773	233.700	11.74	280.15	9.54
	283.023	11.417	283.488	11 187	263.929	10.47	273.083	8 633	276.025	10.037	276.183	8.013	326.332	11.13	338.125	8.773	234.371	11.753	380.15	9.347
	284.854	11.417	283.654	11.2	263.696	10.457	273.317	8.64	275.908	10.697	276.4	8.613	325.925	11.19	338.025	8.76	236.063	11.74	380,183	9.34
	285.204	11.417	283.863	11.2	263.579	10.45	273.658	8.627	276.433	10.677	276.475	8.613	326.1	11.177	337.567	8.76	236.938	11.753	380.925	9.373
	285.054	11.417	283.304	11.2	263.313	10.45	273.767	8.633	275.992	10.677	276.183	8.607	325.658	11.177	337.408	8.773	237.721	11.753	380.767	9.34
	284.888	11.417	283.604	11.187	263.146	10.477	273.133	8.64	275.942	10.69	275.55	8.627	325.375	11.197	336.908	8.76	237.438	11.753	381.067	9.34
	284.713	11.417	283.288	11.2	262.563	10.437	272.95	8.64	275.3	10.683	275.9	8.64	324.792	11.177	336.325	8.793	236.388	11.77	381.55	9.34
	284.363	11.417	283.013	11.2	262.621	10.457	273.342	8.64	275.475	10.683	275.492	8.64	324.558	11.17	336.583	8.793	235.396	11.74	381.275	9.333
	284.563	11.417	283.029	11.2	262.704	10.45	273.492	8.633	275.208	10.683	275.508	8.627	324.642	11.17	336.6	8.78	234.488	11.753	381.958	9.347
	284.563	11.41	283.646	11.207	262.238	10.443	273.308	8.64	274.917	10.65	275.592	8.647	324.467	11.17	336.417	8.773	233.613	11.74	381.642	9.347
	284.596	11.417	282.804	11.207	262.329	10.463	273.4	8.64	275.475	10.683	275.683	8.627	324.85	11.163	336.375	8.787	233.588	11.74	382.4	9.34
	284.746	11.417	283.121	11.213	262.246	10.43	2/2.91/	8.633	276.15	10.683	2/6	8.627	325.81/	11.17	337.225	8.78	233.796	11.74	382.85	9.313
	284.721	11.417	283.404	11.207	262.513	10.443	2/3.46/	8.647	275.95	10.69	275.617	8.64	325.325	11.163	336.975	8.787	234.588	11.74	382.6	9.333
	284.571	11.417	283.040	11.207	262.240	10.463	273.308	8.04	276.033	10.692	275.858	8.055	325.058	11.103	226.059	8.793	235.138	11.74	383.242	9.313
	284.571	11.417	283.388	11 207	262.240	10.43	272.517	8 647	275.000	10.005	275.2	8 647	325.050	11.177	335.892	8 787	237 529	11.74	382 317	9 307
	284.046	11.41	282.596	11.207	261.546	10.417	272.658	8.64	274.808	10.69	275.342	8.647	323.483	11.177	335.367	8.833	237.704	11.77	381.525	9.32
	284.246	11.417	282.938	11.2	261.688	10.457	272.2	8.66	274.833	10.69	275.15	8.647	323.333	11.163	335.175	8.807	237.496	11.783	381.733	9.34
25/02/2014	284.246	11.417	282.946	11.207	261.629	10.41	272.475	8.66	274.425	10.683	275.025	8.64	323.625	11.15	335.317	8.813	236.679	11.797	380.675	9.34
25/02/2014	284.363	11.417	283.488	11.207	261.746	10.477	272.483	8.64	276.525	10.703	275.3	8.64	325.667	11.163	336.792	8.807	235.921	11.797	380.683	9.35
	284.188	11.417	282.729	11.24	262.096	10.437	272.258	8.647	276.875	10.69	276.408	8.647	326.017	11.163	338.567	8.813	234.871	11.797	380.592	9.333
	284.188	11.41	282.638	11.233	262.854	10.45	272.033	8.667	276.875	10.677	276.85	8.66	326.483	11.17	338.608	8.793	233.763	11.797	381.033	9.367
	284.188	11.417	283.221	11.213	263.496	10.443	272.217	8.66	276.933	10.697	277.167	8.673	326.133	11.17	338.392	8.813	233.004	11.797	380.15	9.333
	284.013	11.417	282.696	11.213	263.904	10.437	271.958	8.647	276.175	10.683	277.308	8.647	325.842	11.15	338.533	8.813	232.188	11.81	379.625	9.347
Ⅰ ⊢	284.013	11.417	282.663	11.227	264.488	10.463	272.592	8.66	276.117	10.683	276.875	8.647	325.608	11.157	337.967	8.833	231.896	11.81	379.325	9.34
Ⅰ ⊢	283.838	11.41/	282.496	11.227	264.429	10.45	272.158	8.66	2/5./67	10.683	276.708	8.6/3	324./33	11.1//	337.667	8.813	233.296	11.81	377.958	9.34
	203./13	11.417	203.004	11.22/	204.390	10.423	272.133	0.007	213.292	10.09	270.017	0.047	324.33 274.33	11.17	226 006	610.0 C0 Q	200.090	11.01	277 222	3.555
	283.654	11.417	282.579	11.227	264.246	10.463	271.842	8.673	274.883	10.69	275.592	8.66	323.558	11.105	336.15	8.847	234.804	11.81	376.308	9.353
	283.854	11.417	282.529	11.233	264.096	10.43	271.792	8.673	274.5	10.683	275.142	8.647	323.35	11.157	335.967	8.833	235.238	11.823	375.725	9.313
	283.829	11.417	282.821	11.227	263.838	10.417	271.683	8.66	274.475	10.67	275.433	8.673	322.858	11.15	335.325	8.82	235.504	11.823	375.35	9.3
	283.829	11.417	282.696	11.24	263.663	10.403	272.225	8.673	274.125	10.677	274.908	8.673	322.333	11.177	335.2	8.847	234.338	11.823	374.825	9.3
	283.771	11.417	282.621	11.227	263.371	10.463	271.883	8.673	273.717	10.683	274.433	8.673	322.1	11.163	334.458	8.86	232.879	11.823	374.35	9.333
	283.921	11.417	283.046	11.233	262.879	10.41	271.775	8.673	273.692	10.69	274.192	8.66	322.25	11.177	334.217	8.82	231.629	11.823	374.108	9.32
	283.471	11.417	282.913	11.24	262.546	10.41	270.708	8.66	273.358	10.683	273.525	8.68	321.742	11.17	333.817	8.84	230.246	11.823	373.442	9.34
	283.121	11.417	282.171	11.24	262.021	10.41	2/1.56/	8.667	2/2.833	10.69	2/3.183	8.68	321.21/	11.197	333.075	8.82	229.371	11.823	372.833	9.333
	283.088	11.417	282.579	11.20	261.788	10.417	271.308	8.66	272.0	10.69	272.925	8.66	320.923	11.105	332 367	8.84	229.234	11.823	372.442	9.32
	283.313	11.417	282.329	11.253	260.579	10.43	271.058	8.673	271.567	10.677	272.142	8.68	319.717	11.163	332.167	8.84	229.446	11.823	370.858	9.34
	283.238	11.417	282.404	11.233	260.271	10.423	271	8.667	271.142	10.683	271.95	8.673	319.058	11.157	332.242	8.82	230.654	11.823	370	9.32
	283.004	11.417	281.979	11.247	259.454	10.443	270.708	8.667	270.85	10.683	271.658	8.68	318.533	11.157	331.017	8.793	231.063	11.823	369.042	9.367
	282.979	11.417	282.496	11.247	259.079	10.417	270.425	8.673	270.65	10.677	270.975	8.68	318.158	11.17	330.733	8.813	231.971	11.823	368.625	9.373
26/02/2014	282.829	11.417	281.863	11.247	258.929	10.423	270.858	8.667	270.5	10.683	271.142	8.673	317.542	11.163	330.633	8.82	232.696	11.823	368.258	9.36
	282.979	11.417	282.504	11.247	259.021	10.437	2/1.1	8.6/3	270.65	10.683	2/1.11/	8.68	317.458	11.157	330.342	8.84	232.263	11.823	368.367	9.333
	283.204	11.417	281.338	11.233	258.204	10.423	270.8	8.66	269.95	10.677	270.33	8.68	316.642	11.15	329.242	8.847	229.288	11.823	367.533	9,393
	283.154	11.417	282.246	11.26	258.496	10.437	270,708	8.667	270.125	10.69	270.592	8.653	316.817	11.15	329.683	8.807	228.413	11.823	368.108	9.367
	282.804	11.417	281.854	11.247	257.679	10.423	270.317	8.673	269.6	10.69	270.2	8.64	316.233	11.157	328.892	8.84	226.838	11.823	367.183	9.373
	282.904	11.417	282.179	11.24	257.779	10.417	270.908	8.667	269.642	10.677	270.125	8.66	316.333	11.157	329.35	8.847	226.588	11.823	367.375	9.373
	282.796	11.417	282.229	11.24	257.029	10.41	270.825	8.667	269.067	10.677	269.375	8.653	315.642	11.163	328.333	8.84	225.838	11.823	366.758	9.38
	283.321	11.417	282.404	11.24	257.321	10.403	271	8.68	269.592	10.677	270.083	8.653	315.992	11.163	328.908	8.84	226.654	11.823	367.067	9.393
	283./21	11.417	282.671	11.253	257.138	10.43	2/1.4	8.673	269.642	10.683	269.95	8.653	316.217	11.163	328.108	8.8/3	227.638	11.823	367.2	9.373
	283.490	11.417	282.796	11.247	256.913	10.437	270.858	8.08	269.592	10.677	269.542	8.0/3	315.467	11.103	327.907	8.80	228.813	11.823	307.458	9.393
	283.404	11.417	283 254	11.247	256.304	10.423	270.517	8 673	269.092	10.603	269 333	8 673	315.400	11.17	327.625	8 867	230.050	11.823	368 317	9 387
	283.229	11.417	282.479	11.247	256.296	10.417	270.542	8.68	269.442	10.683	269.758	8.66	315.55	11.15	327.783	8.86	231.579	11.823	369.408	9.367
	283.579	11.417	282.504	11.26	256.413	10.45	270.833	8.68	269.5	10.67	269.917	8.653	315.608	11.15	327.675	8.86	230.938	11.823	369.967	9.393
	283.388	11.417	282.763	11.24	255.988	10.437	270.825	8.68	269.542	10.697	269.642	8.673	315.708	11.157	327.4	8.873	229.988	11.823	371.025	9.373
	283.038	11.417	282.788	11.26	255.988	10.45	270.583	8.68	269.425	10.683	270.067	8.66	315.592	11.15	327.558	8.867	228.704	11.823	371.983	9.38
	283.446	11.417	283.163	11.273	255.929	10.437	270.425	8.693	269.717	10.683	270.175	8.653	315.417	11.157	327.8	8.847	227.829	11.823	373.292	9.373
	283.154	11.417	283.129	11.247	255.988	10.417	270.792	8.693	270.008	10.69	270.275	8.66	316.525	11.17	327.5	8.867	227.596	11.823	374.458	9.373
	283.154	11.417	282.529	11.267	256.279	10.423	270.058	8.7	270.417	10.67	270.742	8.6/3	317.458	11.15	327.7	8.867	228.588	11.823	374.925	9.347
	202.013	11.417	202.238	11 272	250.229	10.43	270.107	8 712	2/1./0/	10.07	271.317	80.0 8 66	320 002	11 157	323.400	0.073 8 8/17	229.121	11 872	373.907	9.34
	282.104	11.417	281.829	11.267	256.863	10.417	269.092	8.7	272.342	10.69	272.175	8.673	320.083	11.17	331.667	8.873	231.038	11.823	374.358	9.34
	282.429	11.417	282.038	11.26	257.713	10.43	269.433	8.693	272.725	10.703	272.383	8.673	319.592	11.177	331.342	8.84	232.354	11.823	373.367	9.34
27/02/2014	282.429	11.417	281.471	11.273	258.646	10.423	269.4	8.693	272.025	10.69	272.617	8.653	319.183	11.157	331.042	8.847	233.346	11.823	372.4	9.36
2770272014	282.604	11.417	281.913	11.253	259.229	10.443	269.308	8.693	272.55	10.683	272.925	8.64	319.592	11.163	331.483	8.867	233.871	11.837	372.975	9.32
	282.579	11.417	282.279	11.28	259.963	10.41	269.542	8.713	272.233	10.677	273.425	8.647	319.217	11.15	330.917	8.847	233.788	11.823	373.342	9.34
-	282.904	11.417	282.513	11.28/	260.696	10.417	270.042	8.7	2/3.083	10.663	274.058	8.653	320.067	11.1//	331.15	8.86	232.7/1	11.837	3/4.108	9.34
	282.804	11.417	281.979	11.28	260.771	10.423	269.775	8.093	272.283	10.67	273.058	8.047	320.083	11.15	331.55	8.833	230.513	11.837	373.308	9.333
	282.934	11.417	281.904	11.20	260.746	10.43	209.342	8.68	272.9	10.665	273.025	8 673	320.383	11.13	331.23	8 833	229.379	11.657	373.367	9.555
	282.454	11.417	281.888	11.287	261.529	10.443	269.55	8.693	272.925	10.69	273.833	8.647	320.783	11.143	331.725	8.833	227.596	11.753	373.083	9,333
	282.629	11.417	282.421	11.293	262.054	10.423	269.283	8.693	273.275	10.677	274.233	8.653	321.075	11.157	332.125	8.833	227.363	11.753	373.217	9.373
	282.979	11.417	282.721	11.307	262.229	10.43	269.583	8.713	273.625	10.67	274.533	8.673	321.425	11.157	332.292	8.86	228.471	11.74	373.917	9.347
	282.979	11.417	282.538	11.26	262.463	10.43	269.8	8.713	273.508	10.677	274.35	8.673	321.308	11.157	332.242	8.86	229.638	11.753	374.133	9.32
	282.804	11.417	282.529	11.293	262.929	10.39	269.392	8.713	273.508	10.677	274.342	8.647	321.483	11.17	332.233	8.86	231.038	11.74	374.525	9.333
	282.838	11.417	282.529	11.287	263.196	10.437	269.392	8.713	273.425	10.683	274.742	8.68	321.517	11.143	332.367	8.86	232.646	11.74	375.458	9.313
	282.813	11.417	282.438	11.28	263.113	10.417	269.033	8.7	2/3.808	10.65	275.183	8.647	321.9	11.15	332.008	8.813	233.788	11.74	3/6.433	9.34
Ⅰ ⊢	282.346	11.417	202.738	11.32	203.140	10.397	269.333	0.093 8.7	274.25	10.67	274.867	8.647	322.05	11.157	331.425	0.833 8.833	234.038 233.613	11.713	378.917	9.353
	282.879	11.417	282.696	11.327	263.646	10.41	269.425	8.72	274.283	10.683	275.708	8.627	322.667	11.15	332.933	8.84	233.271	11.713	380.958	9.32
	282.879	11.417	282.454	11.313	263.413	10.437	269.05	8.713	274.342	10.677	275.867	8.627	323.6	11.15	332.158	8.807	231.638	11.74	381.517	9.373
	282.913	11.417	282.529	11.293	263.446	10.417	269.258	8.713	276.242	10.69	276.608	8.627	326.142	11.15	334.5	8.82	231.379	11.74	383.058	9.313
	282.421	11.417	281.871	11.307	263.013	10.41	269.4	8.713	277.617	10.677	277.95	8.653	327.983	11.157	336.775	8.807	231.063	11.7	383.467	9.353
	282.771	11.417	282.179	11.32	263.946	10.417	269.042	8.7	278.433	10.67	279.058	8.62	328.683	11.157	337.75	8.793	231.646	11.7	383.242	9.393
Ⅰ ⊢	282.771	11.417	282.671	11.297	264.763	10.41	269.133	8.713	278.9	10.683	280.217	8.62	329.325	11.157	338.642	8.787	232.696	11.7	383.6	9.387
Ⅰ ⊢	282,213	11.417	201.504	11 327	265.3/1	10.443	269.033	o./13 8 72	2/8.925	10.69	279.85	0.047 8.67	329.233	11.15	338 15	0.793 8.793	233.013	11.08/	381,908	9,42
	282.388	11.417	281.921	11.327	267.004	10.41	268.517	8.7	278.517	10.677	280.133	8.647	328.825	11.157	338.558	8.793	235.521	11.713	381.917	9.427
28/02/2014	282.738	11.417	282.321	11.313	267.821	10.397	268.383	8.7	278.692	10.677	280.8	8.607	329.35	11.15	338.958	8.787	237.388	11.713	382.183	9.393
	282.738	11.417	282.371	11.32	268.229	10.37	268.433	8.693	278.458	10.677	280.317	8.673	329.35	11.15	338.342	8.78	238.088	11.713	382.233	9.407
	282.388	11.417	282.296	11.32	268.113	10.39	268.225	8.72	278.108	10.67	279.708	8.693	328.65	11.183	338.4	8.787	236.804	11.713	381.492	9.393
1	282.704	11.417	281.846	11.313	267.788	10.403	268.442	8.7	277.608	10.67	279.392	8.68	328.617	11.15	338.083	8.793	234.671	11.7	381.175	9.287

9.353	259.87	11.603	485.65	285.65	
9.367	261.63	11.603	485.875	285.875	
9.347	261.56	11.577	485	285	
9.353	260.97	11.59	485,175	285,175	
9.367	260.94	11.603	485.725	285.725	
9.34	261.1	11.503	486.075	286.075	
9 247	260.68	11.57	494 425	284 425	
9.347	200.08	11.55	484.423	204.423	
9.547	200.40	11.59	404.775	204.775	
9.34	260.81	11.59	485.125	285.125	
9.373	260.92	11.59	486	286	
9.34	261.29	11.59	486.375	286.375	
9.34	260.83	11.59	484.675	284.675	
9.34	260.41	11.603	485.025	285.025	
9.333	260.93	11.603	485.55	285.55	
9.347	260.72	11.59	485.1	285.1	
9.347	260.3	11.59	484.45	284.45	
9.34	260.56	11.577	485.475	285.475	
9.313	260.64	11.577	485.325	285.325	
9.333	260.79	11.59	484.475	284.475	
9 313	261 17	11 59	484.85	284.85	
9.313	261.34	11.603	485.025	285.025	
9.307	260.64	11.59	484.325	284.325	
9.32	260.12	11 59	/83.8	283.8	
9 34	261.33	11.59	484 475	284 475	
9 34	261.55	11.59	483.95	283.95	
9.35	261.81	11 577	184 425	284 425	
0 222	201.81	11.577	404.425	204.425	
0.367	201.38	11.577	482.0	202.0	
9.307	201.33	11.55	482.775	282.775	
3.333	201.04	11.5//	483.425	283.425	
9.54/	201.28	11.563	482.9	282.9	
9.34	261.35	11.5/7	483.2	283.2	
9.34	261.42	11.577	482.5	282.5	-
9.333	260.59	11.577	482.675	282.675	
9.36	261.16	11.577	481.475	281.475	
9.353	260.71	11.59	482.45	282.45	
9.313	261.39	11.59	481.6	281.6	
9.3	261.02	11.59	482.225	282.225	
9.3	260.49	11.577	480.7	280.7	
9.333	261.15	11.577	481.825	281.825	
9.32	261.54	11.59	481.45	281.45	
9.34	260.74	11.603	480.65	280.65	
9.333	260.63	11.603	479.775	279.775	
9.32	260.88	11.59	479.25	279.25	
9.32	261.56	11.577	478.4	278.4	
9.34	260.56	11.563	479.4	279.4	
9.32	261.54	11.577	479.275	279.275	
9.367	261.08	11.577	479.05	279.05	
9.373	260.53	11.59	478.5	278.5	
9.36	260.8	11.577	478	278	
9 333	260.78	11 577	478 975	278 975	
9 367	261.76	11.577	477 675	277.675	
0 202	201.24	11.577	477.075	277.075	
0.367	200.04	11.577	477.275	277.275	
9.307	201.78	11.577	479.43	273.43	
9.373	201.20	11.55	478.525	278.323	
9.575	201.95	11.577	470.03	270.03	
9.38	261.97	11.577	4/9.1	2/9.1	
9.393	262.14	11.577	4/9.2/5	2/9.2/5	
9.373	261.78	11.59	4/9.6/5	2/9.0/5	
9.393	262.67	11.577	4/9.8	2/9.8	
9.38	262.08	11.577	476.975	276.975	
9.387	261.09	11.59	477.525	277.525	
9.367	262.32	11.577	4/8./5	2/8./5	
9.393	262.78	11.59	477.975	2/7.9/5	
9.373	261.99	11.577	479.3	279.3	
9.38	262.45	11.577	478.525	278.525	
9.373	262.49	11.577	478.1	278.1	-
9.373	262.29	11.563	478.2	278.2	
9.347	262.16	11.577	478.6	278.6	
9.34	263.33	11.55	478.775	278.775	
9.333	261.87	11.577	478.075	278.075	
9.34	262.23	11.563	476.9	276.9	
9.34	261.5	11.563	478.175	278.175	
9.36	262.33	11.577	477.475	277.475	
9.32	261.74	11.577	477.65	277.65	
9.34	261.48	11.577	477.15	277.15	
9.34	262.74	11.577	478.65	278.65	
9.333	261.94	11.577			
9.333	262.44	11.59			
9.38	262.27	11.577			
9.333	262.12	11.577			
9.373	262.88	11.577			
9.347	262.82	11.563			
9.32	263.17	11.577			
9.333	262.35	11.563			
9.313	262.59	11.577			
9.34	262.43	11.577			
9.353	262.23	11.577			
9.32	262.71	11.577			
9.32	262.98	11.577			
9.373	262.87	11.563			
9.313	262.45	11.577			
9.353	262.55	11.577			
9.393	262.73	11.577			
9.387	263.13	11.55			
9.47	263.13	11 577			
9,453	262.03	11 577			
9/127	202.1	11.577			
9 202	202.34	11.3//			
9,107	203.88	11.55			
3.407	202.18	11.503			
9.393	261.88	11.577			-
9.287	262.57	11.577			

	202 720	11 417	202 220	11 212	200 221	10 202	200 7	0.7	277 575	10.000	270 202	0.070	220 642	11 1 1 2	220 242	0.70	222 520	11 7	200 222	
-	282.729	11.417	282.238	11.313	268.221	10.383	208.7	8.7	277.575	10.663	2/9.383	8.6/3	328.642	11.143	338.342	8.78	232.538	11.7	380.233	
	282.729	11.417	282.604	11.313	267.988	10.403	268.133	8./13	277.342	10.69	278.95	8.68	328.642	11.163	337.642	8.807	231.021	11.7	380.333	-
	282.496	11.417	281.871	11.327	267.521	10.417	268.6	8.693	276.583	10.683	278.217	8.733	327.708	11.157	337.442	8.793	228.804	11.7	378.667	1
	282.521	11.417	282.046	11.327	267.313	10.403	268.108	8.72	276.375	10.683	277.725	8.74	327.733	11.15	337.35	8.807	228.188	11.687	378.442	
	282.321	11.423	281.713	11.313	266.938	10.403	268.308	8.7	276.175	10.683	277.658	8.733	327.825	11.157	336.883	8.813	228.163	11.713	378.642	
I F	282.521	11.423	281.704	11.313	266.496	10.43	267.767	8.68	276.025	10.69	277.117	8.733	327.5	11.157	336.608	8.773	228.363	11.7	378.1	-
1	282.463	11.423	282.246	11.313	266.088	10.403	267.775	8.72	275.85	10.677	277.258	8,733	327.5	11.157	337.017	8.813	229.879	11.7	377,708	1
	282.613	11.417	282.004	11.327	265.888	10.423	267,933	8,713	275.767	10.677	277.017	8,733	326.95	11.15	336,775	8,793	231,196	11.7	377,733	
	202.020	11 / 72	282.006	11 2 2 7	265 529	10.42	267 902	9 72	275 502	10.67	276 709	9 7 2	226.05	11 15	226 722	9 702	222.062	11.7	277.059	
1 F	202.438	11.423	282.030	11.327	205.558	10.43	207.832	0.72	275.532	10.07	270.708	0.72	320.33	11.15	330.733	8.793	233.003	11 712	377.338	+
	202.400	11.417	282.140	11.52	203.366	10.597	208.208	0.075	275.042	10.085	277.023	8.087	327	11.15	337.03	8.807	254.571	11./15	5/7.6/5	
1 -	282.488	11.417	281.921	11.327	265.296	10.41	268.117	8.72	275.525	10.69	276.4	8./33	326.825	11.15	336.958	8.793	234.571	11.7	378.45	
	282.613	11.417	281.913	11.32	265.071	10.417	267.708	8.68	275.475	10.677	276.525	8.72	326.658	11.15	336.817	8.787	233.238	11.713	378.575	-
	282.438	11.417	281.779	11.307	265.071	10.383	267.575	8.68	275.125	10.67	276.525	8.713	326.133	11.15	336.15	8.807	231.138	11.713	378.842	
	282.463	11.423	281.713	11.327	264.804	10.39	268.175	8.707	274.975	10.65	276.058	8.707	325.983	11.183	336.217	8.807	229.296	11.713	379.042	
	282.488	11.423	282.363	11.343	264.363	10.397	267.625	8.713	274.533	10.683	275.775	8.707	326.008	11.163	335.667	8.793	227.688	11.687	378.892	
	282.196	11.423	282.363	11.363	264.188	10.397	268.025	8.72	274.008	10.683	275.508	8.733	325.658	11.15	335.8	8.787	226.813	11.687	379.425	
	281.796	11.423	281.646	11.333	263.671	10.41	267.308	8.727	273.842	10.677	275.058	8.733	325.55	11.17	336.017	8.807	226.179	11.7	379.775	
	281.471	11.417	280.838	11.327	262.354	10.43	266.367	8.68	272.467	10.657	273.85	8.713	324,583	11.15	334,942	8.787	225.679	11.713	378.833	
1 -	281 596	11 417	281 313	11 307	262 654	10 397	267 242	8 693	273 467	10.67	273 925	8 733	324 592	11 137	335.017	8 807	227 438	11 7	379 442	
	201.550	11 422	201.515	11.307	262.001	10.001	267.212	8.68	272 142	10.67	273 503	8 74	224 617	11.15	224 692	9 797	220,130	11.7	270 642	
01/03/2014	201.730	11.423	281.040	11.34	202.388	10.41	207.442	8.08	273.142	10.07	273.332	0.74	324.017	11.15	334.083	0.707	223.271	11.7	373.042	
1 F	282.321	11.417	281.504	11.32	262.096	10.403	267.3	8.693	273.025	10.677	274.117	8.74	324.208	11.157	335.075	8.787	230.846	11.7	380.167	
1 -	282.321	11.423	281.854	11.293	261.688	10.397	267.517	8.673	273.083	10.683	2/3.667	8./13	323.975	11.163	334.758	8.807	232.421	11.713	380.383	
	282.471	11.423	282.046	11.36	261.663	10.403	267.308	8.72	272.883	10.677	273.992	8.72	323.775	11.15	334.817	8.787	233.213	11.713	381.108	
1 L	282.471	11.423	281.596	11.327	261.079	10.41	267.525	8.72	272.883	10.677	273.942	8.713	323.542	11.157	334.233	8.813	232.279	11.727	381.325	1
1 L	282.321	11.423	282.421	11.353	260.929	10.397	267.283	8.7	272.442	10.683	273.3	8.713	323.275	11.177	333.992	8.813	230.263	11.713	380.95	1 1
I I	282.171	11.423	282.404	11.33	260.488	10.403	267.267	8.693	272.117	10.67	272.35	8.733	322.775	11.163	333.575	8.793	228.188	11.7	381.067	
I L	282.171	11.423	281.696	11.34	260.313	10.377	267.092	8.7	271.767	10.67	272.442	8.733	322.6	11.17	334.067	8.793	226.379	11.7	381.025	/
I F	282.321	11.423	282.121	11.34	259.938	10.377	267.517	8.713	271.567	10.677	272.6	8.733	322.4	11.15	333.558	8.807	225.188	11.713	381.183	
1 [282.321	11.423	281.863	11.327	259.238	10.397	266.992	8.693	271.217	10.683	271.675	8.733	321.408	11.143	333.167	8.787	224.254	11.7	380.258	
1 F	281.871	11.423	281.771	11.347	258.904	10.377	266.767	8.733	270.767	10.677	271 45	8.747	321 25	11.15	332.942	8.813	224.038	11 7	379.9	1
1 F	282 196	11 //23	282.220	11 32	250.504	10 307	200.707	2.703 2.707	270.017	10.677	271 500	Q 722	221.20	11.15	222 122	2.015 2.21	22 1.030	11 712	380 225	
	202.150	11.423	202.225	11.33	250.471	10.357	200.025	9 707	270.517	10.077	271.500	0.733	220.675	11.15	222.075	0.04	223.413	11.713	380.0	
	202.340	11.425	282.104	11.555	258.504	10.597	207.3	8.707	270.93	10.077	271.03	0.747	320.073	11.157	332.875	0.007	227.313	11.715	200.007	
1 F	282.321	11.423	281.938	11.34	257.838	10.39	200.007	8.7	270.925	10.677	2/1.483	8./33	320.883	11.17	332.975	8.787	229.271	11.727	380.867	-
1 -	282.146	11.423	281.671	11.333	257.546	10.383	266.667	8.693	270.633	10.683	2/1.083	8.733	320.358	11.157	332.575	8.793	230.904	11.74	381.4	
1 L	281.971	11.423	281.629	11.353	256.438	10.417	266.225	8.713	270.108	10.677	270.642	8.733	319.833	11.157	332.267	8.807	231.604	11.753	380.425	
1 L	281.821	11.423	281.563	11.333	255.879	10.41	266.158	8.733	269.842	10.683	270.442	8.733	319.567	11.163	331.4	8.793	231.163	11.753	381.292	
	282.146	11.423	282.154	11.36	256.029	10.397	267.15	8.72	269.817	10.67	270.233	8.74	319.308	11.17	331.325	8.78	229.796	11.753	381.35	
	281.271	11.423	281.404	11.34	255.038	10.403	266.4	8.707	269.117	10.67	269.35	8.747	318.025	11.15	330.708	8.78	226.996	11.74	381	
	281.471	11.423	281.913	11.343	254.771	10.423	266.375	8.72	268.85	10.663	269.458	8.707	318.225	11.163	330.55	8.787	225.038	11.74	381.242	
	281.096	11.423	280.863	11.36	254.571	10.39	265.992	8.72	268.358	10.683	268.942	8.733	317.5	11.163	330.167	8.787	223.788	11.727	381.525	
I	281.796	11.423	281.563	11.36	254.513	10.417	266.425	8.713	268.883	10.677	269.508	8.713	317.558	11.143	330.2	8.793	223.438	11.727	381.958	
I F	281.479	11.423	281.396	11.333	253,904	10.43	265.725	8.7	268.392	10.663	268.808	8.74	317.183	11.183	330,433	8,78	223,529	11.74	382.458	1
1 1	281.329	11,423	281.371	11.36	253.463	10.403	266.1	8,727	268.125	10.677	268.517	8.74	316,917	11.15	329.342	8,793	223,904	11.74	383.1	
1 -	281 479	11 423	281 246	11 347	253 379	10 423	265 842	8 72	268 158	10 683	268 925	8 72	316 717	11 163	329 35	8 813	225 396	11 727	382 975	
02/03/2014	292.004	11 / 22	201.210	11.24	253.575	10.125	265.267	9.7	269 159	10.603	268 782	9.76	216.425	11 177	220 242	8 907	223.336	11.72	292.5	1
1 F	202.004	11.423	201.571	11.54	253.040	10.35	200.307	9 712	268.075	10.677	260.703	9 722	216 775	11.177	220.017	0.007	227.140	11.74	295 775	-
1 F	202.415	11.423	202.175	11.353	254.075	10.37	200.242	0.713	208.573	10.077	203.132	0.733	216.092	11.157	330.017	0.02	230.003	11.74	207.722	-
-	282.090	11.425	202.050	11.555	253.704	10.39	203.907	0.727	206.542	10.077	209.317	0.72	510.965	11.15	328.942	0.007	231.700	11.74	307.233	
1 -	282.096	11.423	282.371	11.333	253.704	10.37	266.033	8.72	268.658	10.677	269.117	8./4/	316.342	11.183	329.675	8.78	232.138	11.74	387.7	
1 -	282.479	11.423	282.446	11.333	253.854	10.383	266.108	8.7	269.392	10.677	269.458	8.72	316.842	11.157	329.217	8.847	231.529	11.713	389.242	
1 L	281.488	11.423	282.338	11.363	253.504	10.397	266.4	8.727	268.342	10.677	269.35	8.747	316.025	11.157	329.242	8.82	228.788	11.713	390.067	
1 L	281.696	11.423	282.154	11.373	253.654	10.377	266.75	8.7	268.433	10.683	269.433	8.72	316.117	11.15	328.925	8.82	227.421	11.713	390.55	-
	282.196	11.423	283.071	11.377	253.979	10.383	267	8.7	268.7	10.657	269.817	8.74	316.617	11.157	329.708	8.813	226.754	11.713	392.133	
	281.204	11.423	282.121	11.36	253.104	10.383	266.183	8.727	268.117	10.677	269.267	8.733	316.033	11.15	328.225	8.813	225.529	11.713	391.983	
I I	281.354	11.423	281.463	11.353	253.021	10.397	265.658	8.72	269.142	10.683	269.408	8.693	317.7	11.15	329.833	8.813	225.563	11.713	392.125	
I L	281.763	11.423	281.979	11.327	253.254	10.397	265.775	8.72	273.108	10.657	272.058	8.707	322.833	11.15	334.083	8.86	227.896	11.713	393.175	
I [281.588	11.423	281.929	11.347	254.071	10.383	265.458	8.713	274.45	10.683	273.875	8.693	324.233	11.177	336.967	8.813	230.113	11.713	393.392	
	281.938	11.423	281.704	11.353	255.354	10.37	265.633	8.727	275.092	10.683	274.983	8.72	324.817	11.157	337.675	8.78	231.921	11.727	393.3	
	282.113	11.423	282.054	11.34	256.521	10.39	266.117	8.733	275.442	10.67	276	8.687	325.05	11.15	337.758	8.793	234.604	11.713	393.517	1
	282.113	11.423	281.788	11.347	257.629	10.363	266.117	8.727	275.792	10.637	276.8	8.68	325.342	11.157	337.892	8.773	236.471	11.727	393.25	
1 F	282 288	11 423	281 979	11 353	257 921	10 403	265 725	8 712	275 617	10 677	276 275	8 707	374 875	11 1/12	337 367	8 787	236 938	11 727	393 125	
1 F	281 613	11 //23	281 604	11 367	257.521	10 / 1	2001720	Q 73	275.017	10.677	276.275	93.9	22/1.375	11 15	226 775	8 703	235,631	11 727	207 522	t i
03/03/2014	201.015	11.423	201.004	11.307	250.525	10.41	205.4	9 722	275.252	10.677	276.002	8.69	225.225	11.13	227 292	9 797	222.021	11.727	202.225	
1 F	201.950	11.425	201.979	11.347	259.015	10.55	200.308	0./33	275.207	10.065	270.992	0.00	325.225	11.15	337.203	0.707	255.729	11.713	392.373	
1 F	202.200	11.425	282.590	11.507	200.004	10.565	200.123	0.727	2/3./92	10.67	277.473	0.073	323.223	11.145	337.307	0.775	231.740	11.715	393.236	
1 -	281.763	11.423	281.579	11.333	260.429	10.39	265.642	8.707	274.742	10.67	2/6.858	8.68	324.525	11.15	336.883	8.773	229.354	11./13	392.642	
1 L	281.413	11.423	281.538	11.327	260.721	10.39	264.933	8.733	274.275	10.677	276.15	8.68	323.883	11.143	335.775	8.78	228.363	11.7	392.067	<u>+</u>
	281.413	11.423	281.404	11.367	260.721	10.41	265.333	8.733	274.275	10.67	276.283	8.687	323.883	11.143	335.375	8.78	227.721	11.687	392.067	+ *
03/03/2014	281.238	11.423	281.629	11.367	261.013	10.39	264.892	8.733	273.75	10.677	275.975	8.66	323.533	11.143	335.6	8.76	227.313	11.7	392.025	-
03/03/2014	-500.837	8.747	-5.696	9.327	260.488	10.403	264.5	8.727	-403.092	10.36	1101.983	8.127	323.3	11.143	335.342	8.78	228.479	11.7	391.767	
03/03/2014	-499.612	8.5	-5.212	8.713	-218.896	8.597	171.783	8.913	-402.275	8.783	171.667	8.803	-354.533	9.293	233.692	9.513	-299.438	9.883	308.25	9
03/03/2014	-495.379	7.75	-0.462	7.347	-214.371	8.06	177.467	10.36	-397.692	7.863	173.617	8.583	-350.358	8.457	237.508	8.527	-295.263	8.927	312.467	
03/03/2014	-500.354	8.683	-4.546	9.187	-219.112	10.253	172.05	11.4	-402.608	8.813	169.133	9.837	-355.392	8.903	233.425	9.493	-300.296	9.557	309.317	[!
03/03/2014	-500.121	9.957	-4.979	10.387	-219.346	10.613	171.35	11.713	-402.492	9.933	229.767	10.423	-355.275	10.013	232.192	10.407	-299.946	10.413	308.617	10
03/03/2014	-500.179	9.787	-5.012	9.86	-219.521	9.773	172.117	10.9	-402.55	9.977	227.467	9.89	-354.808	10.1	233.358	10.253	-300.063	10.11	307.917	
03/03/2014	-499 821	9 517	-11 221	9.74	-219 687	9 477	170 308	9 953	-402.55	9.577	165 202	9 552	-354 742	9 68	233.555	9 833	-300 404	9 512	304 775	t
03/03/2014	-500 729	9.913	-5 704	10 //	_210.007	10 227	171 202	10 622	_/02 092	Q 05	165.352	10 277	-355 65	Q 75	232.55	10.06	-300 104	0.97	307 225	1
03/02/2014	-500.723	10 0/7	-5.704	11 207	-210.779	11 24	171.292	14 747	-402.903	5.03	170 217	10.277	-353.03	3.75 11 267	232.007	11 697	300.490	5.07	200.223	1
02/02/2014	-300.202	10.947	-2.130	12.20/	-219.002	11.34	1/1.20/	14.707	-402.983	12 707	1/0.21/	11.43	-554./1/	11.00/	200.442	11.007			506.267	+
03/03/2014		14.727		12.82				14.527		12.707				12.833						+
03/03/2014		14./3/		13.8				14.233	1	13.323	1	1	1	13.35/		1				1

9.24	262.66	11.563		
9.307	263.49	11.563		
9.287	262.86	11.563		
9.28	262.6	11.563		
9.273	263.17	11.563		
9.28	262.49	11.563		
9.253	262.73	11.533		
9.247	263.13	11.563		
9.3	262.95	11.563		
9.313	263.58	11.55		
9.28	263.75	11.55		
9.307	263.11	11.577		
9.3	262.53	11.577		
9.32	263.5	11.563		
9.313	263.35	11.563		
9.333	263.35	11.563		
9.313	262.53	11.563		
9.353	263.2	11.55		
9.333	263.68	11.55		
9,333	262.53	11,563		
9 36	263.06	11.563		
9.34	263.41	11.55		
9.367	263.73	11.563		
9.347	264.08	11.55		
9.353	264.11	11.55		
9.347	263.19	11.563		
9.347	263.78	11.563		
9.34	263.98	11.55		
9.347	264.42	11.563		
9.333	263.03	11.563		
9.313	263.35	11.563		
9.36	264.03	11.563		
9.34	263.76	11.563		
9.333	263.76	11.563		
9.307	262.82	11.563		
9.313	263.78	11.55		
9.307	262.58	11.563		
9.313	263.76	11.55		
9.307	263.37	11.563		
9.307	262.75	11.577		
9.28	264.22	11.55		
9.273	263.95	11.55		
9.273	263.56	11.55		
9.253	262.7	11.563		
9.28	263.99	11.55		
9.3	263.97	11.563		
9.247	263.58	11.563		
9.28	263.45	11.563		
9.28	263.99	11.563		
9.247	263.68	11.563		
9.247	262.93	11.533		
9.227	264.42	11.55		
9.253	263.93	11.55		
9.32	263.84	11.55		
9.407	262.78	11.533		
9.433	263.9	11.55		
9.34	263.31	11.533		
9.24	263.66	11.533		
9.273	263.66	11.533		
9.433	263.9	11.533		
9.42	264.34	11.55		
9.433	264.32	11.55		
9.407	263.9	11.533		
9.453	263.55	11.533		
9.433	264.14	11.55		
9.42/	263.38	11.533		
9.307	254.96	11.55		
9.32	-362.54	7.923		
9.013	-360.85	8.023		
1.893	-357.08	7.203		
3.113	-301.45	9.063		
0.413	-302.15	10.137	-	-
3.32/	-301.32	9.56/		
3.747	-301.83	9.363		
1 3/17	-302.04	11.123		
	-201.22	11.02/		
.1.5 17		17 95		



New Monks Farm CS/05631 April 2014 Commercial in Confidence Appendix C

Appendix C

Groundwater Levels (Manual Dip Measurements)

		Grou	iawater iet	/ci bips 05/001	Cordary 2014		
Location	AOD of casing	Date	Time	Water	Level	Ва	se
				Dip (m)	m AOD	Dip (m)	m AOD
BH01S	2.801	05/02/2014	09:53	0.770	2.031	5.100	-2.299
BH01D	2.801	05/02/2014	09:53	0.280	2.521	12.550	-9.749
BH02S	3.854	06/02/2014	10:12	1.190	2.664	2.980	0.874
BH02D	3.854	06/02/2014	10:12	1.130	2.724	7.450	-3.596
BH03S	4.728	06/02/2014	10:17	1.830	2.898	2.080	2.648
BH03D	4.728	06/02/2014	10:17	1.830	2.898	11.980	-7.252
BH04S	3.864	06/02/2014	10:03	n/r		3.300	0.564
BH04D	3.864	06/02/2014	10:03	n/r		9.550	-5.686
BH05S	2.981	06/02/2014	10:30	0.440	2.541	2.670	0.311
BH05D	2.981	06/02/2014	10:30	0.440	2.541	6.400	-3.419
BH06S	4.31	06/02/2014	10:23	0.960	3.350	3.050	1.260
BH06D	4.31	06/02/2014	10:23	1.040	3.270	9.940	-5.630
BH07S	5.185	06/02/2014	10:38	1.480	3.705	3.260	1.925
BH07D	5.185	06/02/2014	10:38	11.550	-6.365	2.720	2.465
BH08S	3.919	06/02/2014	10:51	0.500	3.419	2.400	1.519
BH08D	3.919	06/02/2014	10:51	0.940	2.979	9.770	-5.851
BH09S	4.353	06/02/2014	11:21	0.610	3.743	2.620	1.733
BH09D	4.353	06/02/2014	11:21	1.050	3.303	0.476	3.877
BH10S	3.262	05/02/2014	09:46	0.300	2.962	2.700	0.562
BH10D	3.262	05/02/2014	09:46	1.170	2.092	8.270	-5.008

2044

					(Groundwater Lev	/el Dips 04/05 m	narch 2014
Location	AOD of casing	Date	Time	Water	Level	Ва	se	Comments
				Dip (m)	m AOD	Dip (m)	m AOD	
BH01S	2.801	04/03/2014	12:30	0.000	2.801	nr		Deep well under artesian conditions and overflowing, shallow well level is
BH01D	2.801	04/03/2014	12:30	0.000	2.801	nr		
BH02S	3.854	04/03/2014	14:15	1.235	2.619	2.950	0.904	
BH02D	3.854	04/03/2014	14:16	1.310	2.544	7.300	-3.446	
BH03S	4.728	04/03/2014	15:23	1.930	2.798	2.300	2.428	
BH03D	4.728	04/03/2014	15:27	1.940	2.788	11.700	-6.972	
BH04S	3.864	04/03/2014	13:24	1.180	2.684	3.300	0.564	
BH04D	3.864	04/03/2014	13:24	1.190	2.674	9.500	-5.636	
BH05S	2.981	05/03/2014	15:54	0.435	2.546	2.400	0.581	BH05S and BH05D connected.
BH05D	2.981	05/03/2014	15:54	0.430	2.551	5.500	-2.519	
BH06S	4.31	05/03/2014	14:39	1.095	3.215	3.050	1.260	
BH06D	4.31	05/03/2014	14:41	1.245	3.065	9.920	-5.610	
BH07S	5.185	05/03/2014	12:26	1.560	3.625	3.250	1.935	
BH07D	5.185	05/03/2014	12:27	2.990	2.195	11.400	-6.215	
BH08S	3.919	05/03/2014	10:56	0.605	3.314	2.300	1.619	
BH08D	3.919	05/03/2014	10:58	1.370	2.549	9.800	-5.881	
BH09S	4.353	05/03/2014	09:48	0.665	3.688	2.600	1.753	
BH09D	4.353	05/03/2014	09:50	1.560	2.793	11.200	-6.847	
BH10S	3.262	04/03/2014	10:30	0.530	2.732	2.560	0.702	
BH10D	3.262	04/03/2014	10:30	0.670	2.592	8.010	-4.748	

s uncertain.

We | Listen Create Deliver

						Groundwater L	Level Dips 06 N	larch 2014
Location	AOD of casing	Date	Time	Water	Level	Ba	ase	Comments
				Dip (m)	m AOD	Dip (m)	m AOD	
BH01S	2.801	06/03/2014	09:50	0.000	2.801			Deep well under artesian conditions and overflowing, shallow wel level is
BH01D	2.801	06/03/2014	09:48	0.000	2.801			
BH02S	3.854	06/03/2014	11:26	1.520	2.334			
BH02D	3.854	06/03/2014	11:25	1.524	2.330			
BH03S	4.728							
BH03D	4.728							
BH04S	3.864	06/03/2014	11:08	1.290	2.574			
BH04D	3.864	06/03/2014	11:10	1.295	2.569			
BH05S	2.981							
BH05D	2.981							
BH06S	4.31	06/03/2014	11:39	1.180	3.130			
BH06D	4.31	06/03/2014	11:42	1.320	2.990			
BH07S	5.185	06/03/2014	12:04	1.580	3.605			
BH07D	5.185	06/03/2014	11:53	3.080	2.105			
BH08S	3.919							
BH08D	3.919							
BH09S	4.353							
BH09D	4.353							
BH10S	3.262	06/03/2014	09:34	0.560	2.702			
BH10D	3.262	06/03/2014	09:40	0.450	2.812			

						Groundwater Le	evel Dips 14th N	Narch 2014
Location	AOD of casing	Date	Time	Water	Level	Ba	ase	Comments
				Dip (m)	m AOD	Dip (m)	m AOD	
BH01S	2.801							
BH01D	3.076	14/03/2014	11:19	0.270	2.806			0.275m standpipe installed on top of BH01D.
BH02S	3.854							
BH02D	3.854							
BH03S	4.728							
BH03D	4.728							
BH04S	3.864							
BH04D	3.864							
BH05S	2.981							
BH05D	2.981							
BH06S	4.31							
BH06D	4.31							
BH07S	5.185							
BH07D	5.185							
BH08S	3.919							
BH08D	3.919							
BH09S	4.353							
BH09D	4.353							
BH10S	3.262							
BH10D	3.262							





New Monks Farm CS/05631 April 2014 Commercial in Confidence Appendix D

Appendix D

Water Quality Data (Lab certification and in-situ index testing)



Martin Weil Capita Property and Infrastructure Ltd Capita House Wood Street East Grinstead West Sussex RH19 1UU

t: 01342 327161

f: 01342 315927

e: martin.weil@capita.co.uk

Analytical Report Number : 14-51791

Project / Site name:	New Monks Farm	Samples received on:	10/03/2014
Your job number:		Samples instructed on:	10/03/2014
Your order number:		Analysis completed by:	19/03/2014
Report Issue Number:	1	Report issued on:	19/03/2014
Samples Analysed:	29 water samples		

Signed:

Dr Claire Stone Quality Manager For & on behalf of i2 Analytical Ltd.

Other office located at: ul. Pionierów 39, 41 -711 Ruda Śląska, Poland

Standard sample disposal times, unless otherwise agreed with the laboratory, are :

Excel copies of reports are only valid when accompanied by this PDF certificate.



Thurstan Plummer Organics Technical Manager For & on behalf of i2 Analytical Ltd.

 4 weeks from reporting
- 2 weeks from reporting
- 2 weeks from reporting
- 6 months from reporting



i2 Analytical Ltd. 7 Woodshots Meadow, Croxley Green Business Park, Watford, Herts, WD18 8YS

t: 01923 225404 f: 01923 237404 e: reception@i2analytical.com





l ab Sample Number				321797	321788	321780	321700	321701	321702
Sample Reference				BH10D	BH10S	BH01D	BH04S	BH04D	BH02S
Sample Number				None Supplied					
Denth (m)				0.67	0.55	0.00	1.18	1.19	1.235
Date Sampled				04/03/2014	05/03/2014	04/03/2014	04/03/2014	04/03/2014	04/03/2014
Time Taken				1115	1415	1230	1330	1340	1430
				1110	1110	1200	1000	1010	2.100
		융ᆔ	. 6						
Analytical Parameter	u u	ite ini	Stat						
(Water Analysis)	ថ	ti č	tat						
		B	i.						
General Inorganics									
pH	pH Units	N/A	ISO 17025	7.9	7.5	7.6	7.5	7.4	7.5
Total Cyanide	µg/l	10	ISO 17025	< 10	< 10	< 10	< 10	< 10	< 10
Sulphate as SO₄	ug/l	45	ISO 17025	26600	162000	24900	17900	45900	37700
Chloride	mg/l	0.15	ISO 17025	45	240	85	48	51	69
Ammonium as NH ₄	µg/l	15	ISO 17025	< 15	< 15	< 15	< 15	< 15	< 15
Alkalinity	mg/l	3	ISO 17025	120	220	120	200	150	140
Iotal Phenois									
i otai Phenois (monohydric)	µg/l	10	ISO 17025	< 10	< 10	< 10	< 10	< 10	< 10
Speciated PAHs									
Nanhthalene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
	µg/1	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
	µg/1	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Fluorene	µg/i	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Phenanthrene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Anthracene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Fluoranthene	ua/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Pyrene	ua/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(a)anthracene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Chrysene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(b)fluoranthene	µq/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(k)fluoranthene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(a)pyrene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Indeno(1,2,3-cd)pyrene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Dibenz(a,h)anthracene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(ghi)perylene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Total PAH									
Total EPA-16 PAHs	µg/l	0.2	ISO 17025	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20
Heavy Metals / Metalloids									
Arsenic (dissolved)	ua/l	1	ISO 17025	4.6	9.4	6.4	10	7.0	6.5
Boron (dissolved)	ug/l	10	ISO 17025	37	220	46	72	35	42
Cadmium (dissolved)	ug/l	0.08	ISO 17025	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08
Chromium (hexavalent)	ua/l	5	ISO 17025	< 5.0	< 5.0	< 5.0	< 5.0	< 5.0	< 5.0
Chromium (dissolved)	ua/l	0.4	ISO 17025	< 0.4	< 0.4	< 0.4	< 0.4	< 0.4	< 0.4
Copper (dissolved)	μα/l	0.7	ISO 17025	< 0.7	< 0.7	0.9	0.8	< 0.7	< 0.7
Lead (dissolved)	µg/l	1	ISO 17025	4.1	3.1	2.9	< 1.0	3.9	1.9
Manganese (dissolved)	µg/l	0.06	ISO 17025	390	2700	9.1	180	6.9	70
Mercury (dissolved)	µg/l	0.5	ISO 17025	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5
Nickel (dissolved)	µg/l	0.3	ISO 17025	20	16	< 0.3	1.5	0.8	1.4
Selenium (dissolved)	µg/l	4	ISO 17025	< 4.0	< 4.0	< 4.0	< 4.0	< 4.0	< 4.0
Zinc (dissolved)	µg/l	0.4	ISO 17025	69	5.3	3.2	1.8	2.6	2.5
	1		1						
Calcium (dissolved)	mg/l	0.012	ISO 17025	100	130	110	110	140	100
Magnesium (dissolved)	mg/l	0.005	150 17025	5.5	23	/.9	9.9	8.2	/.4
Soaium (aissoived)	mg/l	0.01	150 1/025	31	210	58	32	22	5/





Lab Sample Number 321789 321790 321792 321787 321788 321791 Sample Reference BH04D BH10D BH10S BH01D BH04S BH02S Sample Number None Supplied None Supplied None Supplied None Supplied None Supplied None Supplied Depth (m) 0.67 0.55 0.00 1.18 1.19 1.235 Date Sampled 04/03/2014 05/03/2014 04/03/2014 04/03/2014 04/03/2014 04/03/2014 Time Taken 1115 1415 1230 1330 1340 1430 Accreditation Status Limit of detection Analytical Parameter Units (Water Analysis) Monoaromatics Benzene µg/l ISO 17025 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 < 1.0ISO 1702 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 Toluene ua/l Ethylbenzene ISO 1702 < 1.0 µg/l < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 1 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 p & m-xylene µg/l ISO 17025 µg/l ISO 17025 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 -xylene MTBE (Methyl Tertiary Butyl Ether) ua/l ISO 1702 < 1.0 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 **Petroleum Hydrocarbons** TPH-CWG - Aliphatic >C5 - C6 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C6 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C10 - C12 ua/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C12 - C16 10 < 10 < 10 < 10 µg/l NONE TPH-CWG - Aliphatic >C16 - C21 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C21 - C35 µg/l 10 < 10 < 10 < 10 < 10 < 10 NONE < 10 TPH-CWG - Aliphatic (C5 - C35) < 10 < 10 < 10 < 10 µg/l 10 NONE < 10 < 10 < 10 TPH-CWG - Aromatic >C5 - C7 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C7 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C10 - C12 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C12 - C16 10 µg/l NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C16 - C21 10 < 10 < 10 < 10 < 10 µg/l NONE < 10 < 10 < 10 TPH-CWG - Aromatic >C21 - C35 10 NONE < 10 < 10 < 10 µg/l

< 10

< 10

< 10

< 10

< 10

< 10

U/S = Unsuitable Sample I/S = Insufficient Sample

µg/l

10

NONE

TPH-CWG - Aromatic (C5 - C35)





Lab Sample Number				321793	321794	321795	321796	321797	321798
Sample Reference				BH02D	BH03D	BH09S	BH09D	BH08S	BH08D
Sample Number				None Supplied					
Depth (m)				1.31	1.94	0.665	1.56	0.605	1.37
Date Sampled				04/03/2014	04/03/2014	05/03/2014	05/03/2014	05/03/2014	05/03/2014
Time Taken				1440	1600	1045	1030	1140	1120
Analytical Parameter (Water Analysis)	Units	Limit of detection	Accreditation Status						
Conoral Inorganics						•			
General Inorganics				7.5	7.5		7.6	7.0	7.6
pH Tatal Casaida	pH Units	N/A	ISO 1/025	/.5	7.5	/.4	7.6	7.3	/.6
I otal Cyanide Sulphate as SO	µg/l	10	ISO 17025	< 10	< 10 80000	< 10	< 10 92500	< 10	< 10 41300
Chlorido	ug/i	0.15	150 17025	10000	100	250	190	750	140
	ug/l	15	ISO 17025	os د 15	190 < 15	1100	< 15	8700	< 15
	ma/l	3	ISO 17025	140	130	220	130	230	120
Airconney	ilig/i	5	130 17025	140	150	220	150	230	120
Total Phenols	-	r							
Total Phenols (monohydric)	µg/l	10	ISO 17025	< 10	< 10	< 10	< 10	< 10	< 10
Speciated PAHs									
Naphthalene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	0.69	< 0.01
Acenaphthylene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Acenaphthene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Fluorene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Phenanthrene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Anthracene	µg/l	0.01	ISO 1/025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Pluorantnene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Pyrene Ronzo(a)anthracono	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Chrycone	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(h)fluoranthene	µg/1	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(k)fluoranthene	µg/1	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(a)nyrene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Indeno(1,2,3-cd)pyrene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Dibenz(a,h)anthracene	µa/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(ghi)perylene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Total PAH									
Total EPA-16 PAHs	µg/l	0.2	ISO 17025	< 0.20	< 0.20	< 0.20	< 0.20	0.70	< 0.20
Heavy Metals / Metalloids									
Arsenic (dissolved)	µg/l	1	ISO 17025	8.1	7.7	15	6.0	21	5.7
Boron (dissolved)	µg/l	10	ISO 17025	88	150	580	140	1100	69
Cadmium (dissolved)	µg/l	0.08	ISO 17025	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08
Chromium (hexavalent)	µg/l	5	ISO 17025	< 5.0	< 5.0	< 5.0	< 5.0	< 5.0	< 5.0
Chromium (dissolved)	µg/l	0.4	ISO 17025	< 0.4	< 0.4	< 0.4	< 0.4	0.6	< 0.4
Copper (dissolved)	µg/l	0.7	ISO 17025	< 0.7	< 0.7	1.5	0.8	1.2	1.0
Lead (dissolved)	µg/l	1	ISO 17025	3.4	3.6	5.2	5.2	6.9	3.9
Manganese (dissolved)	µg/l	0.06	ISO 17025	20	22	2000	110	8400	69
Mercury (dissolved)	µg/l	0.5	ISO 17025	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5
Nickel (dissolved)	µg/l	0.3	ISO 17025	1.2	1.0	11	0.8	25	0.5
Selenium (dissolved)	µg/l	4	ISO 17025	< 4.0	< 4.0	< 4.0	< 4.0	< 4.0	< 4.0
Zinc (dissolved)	µg/l	0.4	ISO 17025	5.9	8.1	3.5	2.8	3.1	5.4
Calcium (dissolved)	mg/l	0.012	ISO 17025	120	120	270	92	410	100
Magnesium (dissolved)	mg/l	0.005	ISO 17025	8.1	11	43	29	79	10
Sodium (dissolved)	mg/l	0.01	ISO 17025	46	130	210	110	580	80





Lab Sample Number 321798 321793 321794 321795 321796 321797 Sample Reference BH02D BH03D BH09S BH09D BH08S BH08D Sample Number None Supplied None Supplied None Supplied None Supplied None Supplied None Supplied Depth (m) 1.31 1.94 0.665 1.56 0.605 1 37 Date Sampled 04/03/2014 04/03/2014 05/03/2014 05/03/2014 05/03/2014 05/03/2014 Time Taken 1440 1600 1045 1030 1140 1120 Accreditation Status Limit of detection Analytical Parameter Units (Water Analysis) Monoaromatics Benzene µg/l ISO 1702 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 < 1.0ISO 1702 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 Toluene ua/l Ethylbenzene ISO 1702 < 1.0 µg/l < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 1 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 p & m-xylene µg/l ISO 17025 µg/l ISO 17025 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 -xylene MTBE (Methyl Tertiary Butyl Ether) ua/l ISO 1702 < 1.0 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 **Petroleum Hydrocarbons** TPH-CWG - Aliphatic >C5 - C6 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C6 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C10 - C12 ua/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C12 - C16 10 < 10 < 10 < 10 µg/l NONE TPH-CWG - Aliphatic >C16 - C21 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C21 - C35 µg/l 10 < 10 < 10 < 10 < 10 < 10 NONE < 10 TPH-CWG - Aliphatic (C5 - C35) < 10 < 10 < 10 < 10 µg/l 10 NONE < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C5 - C7 µg/l 10 NONE < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C7 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C10 - C12 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C12 - C16 10 µg/l NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C16 - C21 10 < 10 < 10 < 10 < 10 µg/l NONE < 10 < 10 < 10 TPH-CWG - Aromatic >C21 - C35 10 NONE < 10 < 10 < 10 µg/l

< 10

< 10

< 10

< 10

< 10

< 10

U/S = Unsuitable Sample I/S = Insufficient Sample

µg/l

10

NONE

TPH-CWG - Aromatic (C5 - C35)





Lab Sample Number				321799	321800	321801	321802	321803	321804
Sample Reference				BH07S	BH07D	BH06S	BH06D	BH05D	BH11D
Sample Number				None Supplied	None Supplied	None Supplied	None Supplied	None Supplied	None Supplied
Denth (m)				1.56	2.99	1.095	1.245	0.43	1.30
Date Sampled				05/03/2014	05/03/2014	05/03/2014	05/03/2014	05/03/2014	05/03/2014
Time Taken				1300	1700	1540	1525	1625	1430
	1			1000	1/00	1010	1010	1020	1.00
Analytical Parameter (Water Analysis)	Units	Limit of detection	occreditation Status						
General Inorganics									
nH	nH ∐nite	N/A	ICO 17025	73	74	77	77	7.8	77
Total Ovanide	pri onics	10	ISO 17025	/.5	7. 4 < 10	/./	/./	/.0	7.7 < 10
Sulphate as SQ	ug/l	45	ISO 17025	1280000	806000	283000	42700	71000	43600
Chloride	mg/l	0.15	100 17025	220	200	580	30	120	38
Ammonium as NH	ug/l	15	ISO 17025	11000	2600	310	< 15	< 15	< 15
	mg/l	3	100 17025	260	180	130	110	230	110
Aikaininty	mg/i	5	130 17023	200	100	150	110	230	110
Total Phenols									
Total Phenols (monohydric)	ug/l	10	ICO 17025	< 10	< 10	< 10	< 10	< 10	< 10
Total Filehols (Hohonyunc)	µy/i	10	150 17025	< 10	< 10	< 10	< 10	< 10	< 10
Speciated PAHs									
Nanhthalene	ua/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Acenaphthylene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Acenaphthylene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Fluorene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Phenanthrene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Anthracene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Fluoranthene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Pyrene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(a)anthracene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Chrysene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(h)fluoranthene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(k)fluoranthene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(a)pyrene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Indeno(1,2,3-cd)pyrene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Dibenz(a, h)anthracene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(ghi)pervlene	ug/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzelginiperytene	P9/-	0.01	100 17020						10101
Total PAH									
Total EPA-16 PAHs	µg/l	0.2	ISO 17025	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20
Heavy Metals / Metalloids									
Arcenic (discolved)	ua/I	1	ISO 17025	17	10	83	3.6	10	ĘΩ
Boron (discolved)	µg/1	10	ISO 17025	720	610	320	0.C	630	5.0
Cadmium (dissolved)	µg/I	0.08	ISO 17025	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08
Chromium (desavalent)	P9/1	5.00	ISO 17025	< 5.00	< 5.00	< 5.00	< 5.00	< 5.00	< 5.00
Chromium (dissolved)	ug/l	04	ISO 17025	0.4	< 0.4	< 0.4	< 0.4	< 0.4	< 0.4
Copper (dissolved)	µg/1	0.4	150 17025	1.7	2.2	1.5	< 0.7	< 0.7	< 0.7
Lead (dissolved)	µg/I	1	ISO 17025	6.3	4.0	2.3	3.2	> 0.7	1.8
Mangapese (dissolved)	µg/1	0.06	ISO 17025	5200	1400	500	7.6	320	9.2
Marcury (discolved)	µg/I	0.00	ISO 17025	200	205	290	/.0	J20 2 0 5	0.2
Nickel (dissolved)	µg/I	0.3	ISO 17025	21	15	25	< 0.3	<u> </u>	< 0.3
Selenium (dissolved)	µg/I	0.5	ISO 17025	< 10	13	2.3	< 4.0	2.0	< 0.3
Zinc (discolved)	µg/I	04	ISO 17025	12	× ۲۰.0 وي	26	4.0	67	2.4.0
	∎ µ9/1	0.4	130 17025	13	00	2.0	ט.ד	0.7	J.Z
Calcium (dissolved)	mg/l	0.012	ISO 17025	700	280	110	110	46	110
Magnesium (dissolved)	mg/l	0.005	ISO 17025	70	56	24	6.3	19	6.4
Sodium (dissolved)	mg/l	0.01	ISO 17025	200	250	390	25	190	25





Lab Sample Number 321800 321802 321799 321801 321803 321804 Sample Reference BH07S BH07D BH06S BH06D BH05D BH11D Sample Number None Supplied None Supplied None Supplied None Supplied None Supplied None Supplied Depth (m) 1.56 2 99 1.095 1.245 0.43 1.30 Date Sampled 05/03/2014 05/03/2014 05/03/2014 05/03/2014 05/03/2014 05/03/2014 Time Taken 1300 1700 1540 1525 1625 1430 Accreditation Status Limit of detection Analytical Parameter Units (Water Analysis) Monoaromatics Benzene µg/l ISO 17025 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 < 1.0ISO 1702 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 Toluene ua/l Ethylbenzene ISO 1702 < 1.0 µg/l < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 1 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 p & m-xylene µg/l ISO 17025 µg/l ISO 17025 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 -xylene MTBE (Methyl Tertiary Butyl Ether) ua/l ISO 1702 < 1.0 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 **Petroleum Hydrocarbons** TPH-CWG - Aliphatic >C5 - C6 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C6 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C10 - C12 ua/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C12 - C16 10 < 10 < 10 < 10 µg/l NONE TPH-CWG - Aliphatic >C16 - C21 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C21 - C35 µg/l 10 < 10 < 10 < 10 < 10 < 10 NONE < 10 TPH-CWG - Aliphatic (C5 - C35) < 10 < 10 < 10 < 10 µg/l 10 NONE < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C5 - C7 µg/l 10 NONE < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C7 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C10 - C12 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C12 - C16 10 µg/l NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C16 - C21 10 < 10 < 10 < 10 < 10 µg/l NONE < 10 < 10 < 10

< 10

< 10

< 10

< 10

< 10

< 10

< 10

< 10

< 10

U/S = Unsuitable Sample I/S = Insufficient Sample

TPH-CWG - Aromatic >C21 - C35

TPH-CWG - Aromatic (C5 - C35)

10

10

µg/l

µg/l

NONE

NONE





Lab Sample Number				321805	321806	321807	321808	321809	321810
Sample Reference				SW3	SW4	SW5	SW1	SW2	SW6
Sample Number				None Supplied					
Depth (m)				0.265	0.39	0.24	0.86	0.83	0.37
Date Sampled				05/03/2014	05/03/2014	05/03/2014	06/03/2014	06/03/2014	06/03/2014
Time Taken				1217	1155	1205	1030	1058	1234
Analytical Parameter (Water Analysis)	Units	Limit of detection	Accreditation Status						
General Inorganics									
pH	nH I Inits	N/A	ISO 17025	77	77	77	77	7.6	77
Total Cvanide	ua/l	10	ISO 17025	< 10	< 10	< 10	< 10	< 10	< 10
Sulphate as SO ₄	ua/l	45	ISO 17025	88600	78700	154000	31300	37100	262000
Chloride	ma/l	0.15	ISO 17025	160	81	170	41	49	260
Ammonium as NH ₄	ua/l	15	ISO 17025	< 15	< 15	33	< 15	700	< 15
Alkalinity	mg/l	3	ISO 17025	140	140	130	120	130	160
Total Phenols									
Total Phenols (monohydric)	μα/Ι	10	ISO 17025	< 10	< 10	< 10	< 10	< 10	< 10
	P9/1	10	150 17025						× 10
Speciated PAHs		0.01	100 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Naphthalene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Acenaphthylene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Acenaphthene	µg/l	0.01	ISO 1/025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Fluorene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Phenanthrene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Anthracene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Fluoranthene	µg/l	0.01	ISO 1/025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Pyrene	µg/l	0.01	ISO 1/025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(a)anthracene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Chrysene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(b)fluoranthene	µg/l	0.01	ISO 1/025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(K)fluorantnene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Benzo(a)pyrene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Indeno(1,2,3-cd)pyrene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Dibenz(a,n)anthracene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Derizo(giii)perviene	µg/i	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01
Total PAH						•			
Total EPA-16 PAHs	µg/l	0.2	ISO 17025	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20
Heavy Metals / Metalloids									
Arsenic (dissolved)	µg/l	1	ISO 17025	6.3	7.4	7.5	5.4	6.4	7.9
Boron (dissolved)	µg/l	10	ISO 17025	110	94	150	35	52	230
Cadmium (dissolved)	µg/l	0.08	ISO 17025	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08
Chromium (hexavalent)	µg/l	5	ISO 17025	< 5.0	< 5.0	< 5.0	< 5.0	< 5.0	< 5.0
Chromium (dissolved)	µg/l	0.4	ISO 17025	< 0.4	< 0.4	0.5	< 0.4	< 0.4	< 0.4
Copper (dissolved)	µg/l	0.7	ISO 17025	1.3	< 0.7	3.2	0.9	1.6	1.8
Lead (dissolved)	µg/l	1	ISO 17025	2.0	2.4	3.0	2.6	2.3	3.3
Manganese (dissolved)	µg/l	0.06	ISO 17025	5.4	7.7	43	2.6	4.2	11
Mercury (dissolved)	µg/l	0.5	ISO 17025	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5
Nickel (dissolved)	µg/l	0.3	ISO 17025	0.4	< 0.3	1.5	< 0.3	< 0.3	0.6
Selenium (dissolved)	µg/l	4	ISO 17025	< 4.0	< 4.0	< 4.0	< 4.0	< 4.0	< 4.0
Zinc (dissolved)	µg/l	0.4	ISO 17025	3.0	5.2	5.8	4.9	7.1	6.8
Calcium (dissolved)	mg/l	0.012	ISO 17025	120	130	140	110	110	180
Magnesium (dissolved)	mg/l	0.005	ISO 17025	16	11	17	4.5	5.5	31
Sodium (dissolved)	mg/l	0.01	ISO 17025	89	53	98	23	28	160

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mg/l





Lab Sample Number 321805 321806 321808 321809 321810 321807 Sample Reference SW3 SW4 SW5 SW1 SW2 SW6 Sample Number None Supplied None Supplied None Supplied None Supplied None Supplied None Supplied Depth (m) 0.265 0.39 0.24 0.86 0.83 0.37 Date Sampled 05/03/2014 05/03/2014 05/03/2014 06/03/2014 06/03/2014 06/03/2014 Time Taken 1217 1155 1205 1030 1058 1234 Accreditation Status Limit of detection Analytical Parameter Units (Water Analysis) Monoaromatics Benzene µg/l ISO 1702 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 < 1.0ISO 1702 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 Toluene ua/l Ethylbenzene ISO 1702 < 1.0 µg/l < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 1 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 p & m-xylene µg/l ISO 17025 µg/l ISO 17025 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 -xylene MTBE (Methyl Tertiary Butyl Ether) ua/l ISO 1702 < 1.0 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 **Petroleum Hydrocarbons** TPH-CWG - Aliphatic >C5 - C6 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C6 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C10 - C12 ua/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C12 - C16 10 < 10 < 10 µg/l NONE TPH-CWG - Aliphatic >C16 - C21 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C21 - C35 µg/l 10 < 10 < 10 < 10 < 10 < 10 NONE < 10 TPH-CWG - Aliphatic (C5 - C35) < 10 < 10 < 10 < 10 µg/l 10 NONE < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C5 - C7 µg/l 10 NONE < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C7 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C10 - C12 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C12 - C16 10 µg/l NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C16 - C21 10 < 10 < 10 < 10 < 10 µg/l NONE < 10 < 10 < 10 TPH-CWG - Aromatic >C21 - C35 10 NONE < 10 < 10 < 10 µg/l

< 10

< 10

< 10

< 10

< 10

< 10

U/S = Unsuitable Sample I/S = Insufficient Sample

µg/l

10

NONE

TPH-CWG - Aromatic (C5 - C35)





Lab Sample Number				321811	321812	321813	321814	321815	
Sample Reference				SW7	SW8	SW9	SW10	SW11	
Sample Number				None Supplied					
Depth (m)				0.82	0.21	0.39	0.85	0.55	
Date Sampled				06/03/2014	06/03/2014	06/03/2014	06/03/2014	06/03/2014	
Time Taken				1250	1320	1355	1410	1451	
			Þ						
	_	응 드	6						
Analytical Parameter	Uni	te mi	edi						
(Water Analysis)	ស	ti of	us						
			ion						
General Inorganics									
pH	pH Units	N/A	ISO 17025	8.0	7.9	7.9	7.9	7.8	
Total Cyanide	µg/l	10	ISO 17025	< 10	< 10	< 10	< 10	< 10	
Sulphate as SO ₄	ug/l	45	ISO 17025	48500	35200	24800	159000	27400	
Chloride	mg/l	0.15	ISO 17025	53	52	41	110	32	
Ammonium as NH ₄	µg/l	15	ISO 17025	< 15	< 15	< 15	< 15	< 15	
Alkalinity	mg/l	3	ISO 17025	130	120	120	170	140	
Total Phenois					T	•	ā	T	T
Total Phenols (monohydric)	µg/l	10	ISO 17025	< 10	< 10	< 10	< 10	< 10	
Speciated PAHs	1		1						
Naphthalene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Acenaphthylene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Acenaphthene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Fluorene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Phenanthrene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Anthracene	µg/l	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Fluoranthene	µg/l	0.01	ISO 1/025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Pyrene	µg/l	0.01	ISO 1/025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Benzo(a)anthracene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Chrysene Banna (h)fluaranthan a	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Benze(k)flueranthene	µg/I	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Benze(a)pyrana	µg/I	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Indeno(1,2,2,cd)pyrene	µg/I	0.01	150 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Dibenz(a b)anthracene	µg/1	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Benzo(abi)pervlene	µg/I	0.01	ISO 17025	< 0.01	< 0.01	< 0.01	< 0.01	< 0.01	
Denzo(gin/per/iene	P9/1	0.01	150 17025	0.01	\$ 0.01	0.01	\$ 0.01	\$ 0.01	
Total PAH									
Total EPA-16 PAHs	µg/l	0.2	ISO 17025	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	
Heavy Metals / Metalloids									
Arsenic (dissolved)	µg/l	1	ISO 17025	5.3	6.1	6.1	7.0	5.2	
Boron (dissolved)	µg/l	10	ISO 17025	54	44	28	160	27	
Cadmium (dissolved)	µg/l	0.08	ISO 17025	< 0.08	< 0.08	< 0.08	< 0.08	< 0.08	
Chromium (hexavalent)	µg/l	5	ISO 17025	< 5.0	< 5.0	< 5.0	< 5.0	< 5.0	
Chromium (dissolved)	µg/l	0.4	ISO 17025	< 0.4	< 0.4	< 0.4	< 0.4	< 0.4	
Copper (dissolved)	µg/l	0.7	ISO 17025	1.5	1.3	1.5	3.4	12	
Lead (dissolved)	µg/l	1	ISO 17025	1.8	3.3	2.5	2.4	2.4	
Manganese (dissolved)	µg/l	0.06	ISO 17025	13	6.3	3.6	53	0.61	
Mercury (dissolved)	µg/l	0.5	ISO 17025	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	
Nickel (dissolved)	µg/l	0.3	ISO 17025	< 0.3	< 0.3	< 0.3	1.5	< 0.3	
Selenium (dissolved)	µg/l	4	ISO 17025	< 4.0	< 4.0	< 4.0	< 4.0	< 4.0	}
Zinc (dissolved)	µg/l	0.4	ISO 17025	3.9	5.4	5.2	7.2	6.2	
Calaiuma (diasaluad)		0.012	100 1700-	120	110	110	150	110	
Calcium (dissoived)	mg/l	0.012	150 1/025	120	110	110	150	110	1

Calcium (dissolved)	mg/l	0.012	ISO 17025	120	110	110	150	110	
Magnesium (dissolved)	mg/l	0.005	ISO 17025	6.2	5.4	4.0	14	3.3	
Sodium (dissolved)	mg/l	0.01	ISO 17025	31	28	22	81	18	

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Lab Sample Number 321812 321814 321811 321813 321815 Sample Reference SW7 SW8 SW9 SW10 SW11 Sample Number None Supplied None Supplied None Supplied None Supplied None Supplied Depth (m) 0.82 0.21 0.39 0.85 0.55 Date Sampled 06/03/2014 06/03/2014 06/03/2014 06/03/2014 06/03/2014 Time Taken 1250 1320 1355 1410 1451 Accreditation Status Limit of detection Analytical Parameter Units (Water Analysis) Monoaromatics Benzene µg/l ISO 17025 < 1.0< 1.0 < 1.0 < 1.0 < 1.0 ISO 1702 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 Toluene ua/l Ethylbenzene ISO 1702 < 1.0 µg/l < 1.0 < 1.0 < 1.0 < 1.0 1 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 p & m-xylene µg/l ISO 17025 o-xylene MTBE (Methyl Tertiary Butyl Ether) µg/l ISO 17025 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 ua/l ISO 1702 < 1.0 < 1.0 < 1.0 < 1.0 < 1.0 **Petroleum Hydrocarbons** TPH-CWG - Aliphatic >C5 - C6 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C6 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C10 - C12 ua/l 10 NONE < 10 < 10 < 10 < 10 < 10 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C12 - C16 < 10 µg/l NONE TPH-CWG - Aliphatic >C16 - C21 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aliphatic >C21 - C35 µg/l 10 < 10 < 10 < 10 < 10 < 10 NONE TPH-CWG - Aliphatic (C5 - C35) 10 < 10 < 10 < 10 < 10 < 10 µg/l NONE < 10 < 10 < 10 TPH-CWG - Aromatic >C5 - C7 µg/l 10 NONE < 10 < 10 TPH-CWG - Aromatic >C7 - C8 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C8 - C10 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C10 - C12 µg/l 10 NONE < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C12 - C16 10 µg/l NONE < 10 < 10 < 10 < 10 < 10 < 10 < 10 TPH-CWG - Aromatic >C16 - C21 10 < 10 < 10 < 10 µg/l NONE TPH-CWG - Aromatic >C21 - C35 < 10 < 10 10 NONE < 10 < 10 < 10 µg/l TPH-CWG - Aromatic (C5 - C35)

< 10

< 10

< 10

< 10

< 10

U/S = Unsuitable Sample I/S = Insufficient Sample

µg/l

10

NONE





Analytical Report Number : 14-51791

Project / Site name: New Monks Farm

Water matrix abbreviations: Surface Water (SW) Potable Water (PW) Ground Water (GW)

Analytical Test Name	Analytical Method Description	Analytical Method Reference	Method number	Wet / Dry Analysis	Accreditation Status
Alkalinity in Water	Determination of Alkalinity by discreet analyser (colorimetry). Accredited matrices: SW, PW, GW.	In house method based on MEWAM & USEPA Method 310.2.	L082-PL	W	ISO 17025
Ammonium as NH4 in water	Determination of Ammonium/Ammonia/Ammoniacal Nitrogen by the colorimetric salicylate/nitroprusside method. Accredited matrices SW, GW, PW.	In-house method based on Examination of Water and Wastewater 20th Edition: Clesceri, Greenberg & Eaton	L082-PL	w	ISO 17025
Boron in water	Determination of boron by acidification followed by ICP-OES. Accredited matrices: SW PW GW	In-house method based on MEWAM	L039-PL	W	ISO 17025
BTEX and MTBE in water	Determination of BTEX and MTBE in water by headspace GC-MS. Accredited matrices: SW PW GW	In-house method based on USEPA8260	L073W-PL	W	ISO 17025
Chloride in water	Determination of Chloride in water by Gallery Discrete Analyser based on reaction with mercury (II) thiocyanate and acid solution with iron (III) nitrate to form a red/brown iron (III) thiocyanate	Methods for the Examination of Water and Associated Materials Chloride in Waters, Sewage and Effluents 1981.ISBN 0117516260 Accredited matrices: SW, PW,	L082 B	W	ISO 17025
Hexavalent chromium in water	Determination of hexavalent chromium in water by acidification, addition of 1,5 diphenylcarbazide followed by colorimetry.	In-house method by continuous flow analyser. Accredited Matrices SW, GW, PW.	L080-PL	W	ISO 17025
Metals in water by ICP-OES (dissolved)	Determination of metals in water by acidification followed by ICP-OES. Accredited Matrices SW, GW, PW.	In-house method based on MEWAM 2006 Methods for the Determination of Metals in Soil.	L039-PL	W	ISO 17025
Monohydric phenols in water	Determination of phenols in water by continuous flow analyser. Accredited matrices: SW PW GW	In-house method based on Examination of Water and Wastewater 20th Edition: Clesceri, Greenberg & Eaton (skalar)	L080-PL	W	ISO 17025
pH in water	Determination of pH in water by electrometric measurement. Accredited matrices: SW PW GW	In-house method based on BS1377 Part 3, 1990, Chemical and Electrochemical Tests	L005-PL	w	ISO 17025
Speciated EPA-16 PAHs in water	Determination of PAH compounds in water by extraction in dichloromethane followed by GC-MS with the use of surrogate and internal standards. Accredited matrices: SW PW GW	In-house method based on USEPA 8270	L070-UK	W	ISO 17025
Sulphate in water	Determination of sulphate in water by acidification followed by ICP-OES. Accredited matrices: SW PW GW	In-house method based on MEWAM 2006 Methods for the Determination of Metals in Soil.	L039-PL	W	ISO 17025
Total cyanide in water	Determination of total cyanide by distillation followed by colorimetry. Accredited matrices: SW PW GW	In-house method based on Examination of Water and Wastewater 20th Edition: Clesceri, Greenberg & Eaton (Skalar)	L080-PL	w	ISO 17025
TPHCWG (Waters)	Determination of dichloromethane extractable hydrocarbons in water by GC-MS, speciation by interpretation.	In-house method	L070-UK	W	NONE

For method numbers ending in 'UK' analysis have been carried out in our laboratory in the United Kingdom.

For method numbers ending in 'PL' analysis have been carried out in our laboratory in Poland.

Soil analytical results are expressed on a dry weight basis. Where analysis is carried out on as-received the results obtained are multiplied by a moisture correction factor that is determined gravimetrically using the moisture content which is carried out at a maximum of 30oC.

	In Situ Index Testing											
Location		Time	Temperature	אוום*	Baro	ORP	Conductivity	RE	00			
Location Date	nme	°C	PL	"Hg	mV	μs/cm	mg/l	%				
SW01	06/03/2014	10:30	10.85	6.11	30.33	304	526.4	8.71	77.4			
SW02	06/03/2014	10:56	11.32	0.84	30.32	342	556.1	8.41	75.3			
\$11/02	05/03/2014	12:15	12.32	7.02	30.2	123	897.8	13.21	122.3			
30005	06/03/2014	12:14	12.57	2.06	30.32	331	886.5	12.94	119.1			
SW04	05/03/2014	11:54	10.32	0	30.18	187	696.4		81			
SW05	05/03/2014	12:03	8.93	-0.82	30.19	210	915	7.65	65.5			
SW06	06/03/2014	12:34	9.95	4.31	30.31	314	1739	19.37	172.5			
SW07	06/03/2014	13:04	10.98	2.33	30.3	332	678	13.33	118.7			
SW08	06/03/2014	13:26	12.14	3.44	30.3	326	561.8	12.92	119			
SW09	06/03/2014	13:55	12.19	9.86	30.3	276	521.4	11.22	102.6			
SW10	06/03/2014	14:08	8.29	2.01	30.29	336	839.9	8.29	68.8			

*Ph readings found to be unreliable

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